

**Source Test Report for Measurement of
Toxic Metals, Particulate Matter, Nitrogen Oxides,
Sulfur Dioxide, Carbon Monoxide and Total Hydrocarbons on
the Exhaust of a Pyrolytic Oxidation Unit at**

**Balboa Pacific Corporation
11240 Bloomfield Ave.
Santa Fe Springs, CA 90670**

**Prepared For
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PES Job Number 5102.000

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10/18/95**

FOREWORD

This report was prepared by Pacific Environmental Services, Inc. (PES) using due and ordinary care and in accordance with the scope of work identified in the Professional Services Agreement, Purchase Order, or other written/verbal request.

Any measured contaminants and their concentrations detected or identified in this study are for the sample(s) obtained or for the observations made at the time(s) and location(s) referenced in the report and may not represent other times, locations, or contaminants and their concentrations.

Except for the tests and observations conducted by PES, no attempt was made to check for compliance of present or past owners or operators of the equipment, plant, or site with federal, state, or local laws and regulations.

The information provided in this report, including any drawings and specifications, was prepared solely for the use of the identified client and any use by any other party shall be at their own risk.

The project work was conducted by Neil Norcross, Siya Mokh, Steven Hernandez and Rachael Newman under the direction of S. Hugh Brown.

Approved: S. Hugh Brown
S. Hugh Brown, Director
Air Quality Testing

INTRODUCTION

Balboa Pacific Corporation operates a pyrolytic oxidation unit (BAL PAC 2000) at its Santa Fe Springs, CA facility. This unit is utilized for research and development purposes. Balboa Pacific Corporation was contracted to conduct a pilot test of a petroleum byproduct material generated by Texaco Corporation.

The purpose of the test program was to evaluate the exhaust emissions resulting from a waste reduction process to be established in Canada. The source tests determined the particulate matter, total chromium, lead, manganese, copper, nickel, cadmium, beryllium, arsenic, selenium, molybdenum, silver, antimony, barium, thallium, zinc, nitrogen oxides, carbon monoxide, sulfur dioxide and total hydrocarbon (as C_3H_8) mass emission rates from the unit to atmosphere.

Pacific Environmental Services (PES), a participant in the California Air Resources Board (CARB) Independent Contractor Program and certified by the South Coast Air Quality Management District (SCAQMD) for various source testing, was hired by ATC Environmental Group, Inc. to perform the requested source testing and data reduction. PES qualifies as an independent testing laboratory - no conflict of interest.

EQUIPMENT AND PROCESS DESCRIPTION

The pyrolytic oxidation unit utilized for this pilot study consisted of the equipment described below. The unit was tested while running on three separate batches of a petroleum byproduct material over three days of operation. Since there may have been differences in the composition of each batch of byproduct, one run for each parameter was conducted on each individual batch. A second test set consisting of triplicate test runs for each parameter was conducted on the pyrolysis of the char produced during the initial test set.

The material is pumped into the pyrolytic chamber which maintains a low oxygen atmosphere and a temperature of at least 1200 degrees Fahrenheit. The waste is conveyed through the chamber by a ram transport system. Air locks are utilized at each end of the chamber to reduce fugitive emissions (see Figure 1). The temperature of the chamber is maintained by two low NOx natural gas burners that vent directly to the atmosphere. The waste exits the chamber either as non-hazardous dry char, or as gas that is ducted to a thermal oxidizer via a particulate removal cyclone. The natural gas fired thermal oxidizer maintains a temperature of approximately 1400 degrees Fahrenheit to destroy any hazardous gases. The thermal oxidizer exhaust is then vented to the atmosphere via a waste heat recovery boiler, exhaust fan and rectangular exhaust duct. The source tests were conducted on the waste heat boiler exhaust.

1
WASTE HEAT IS
RELEASED TO ATMOSPHERE

2
GAS GENERATED FROM
WASTE MATERIAL IS
PULLED INTO
THERMAL OXIDIZER

3
THERMAL OXIDIZER
DESTROYS OFF GASES

4
WASTE MATERIAL IS
FEED INTO HOPPER

5
CONVERTER DRAWS
MATERIAL INTO A
CORNER'S IT TO A
HARMLESS ASH

6
MATERIAL IS FED
INTO FEED BOXES
AND THEN UP
THE HOPPER

BAL PAC 2000
THERMAL CONVERTER

GAS RELEASE

THE 1975 CONVENTION PRESENTS A BASIC ANALYSIS OF THE CAUSE, THE ACTUAL UTILIZATION OF COMPONENTS AND THE PLANNING OF OPERATIONS SUBJECT TO CHANGE.

Figure 1

Figure 1

TESTING METHODOLOGY

The approximate sampling port locations are shown in Figure 2. The number of traverse points required (6 on each of three sample ports on the long dimension of the rectangular stack) and their locations are specified in EPA Method 1. Triplicate test runs were conducted for all parameters. In addition, EPA Methods 1, 2, 3 and 4 were utilized during each test run to determine moisture, molecular weight, temperature, velocity and flow rate.

Total Particulates

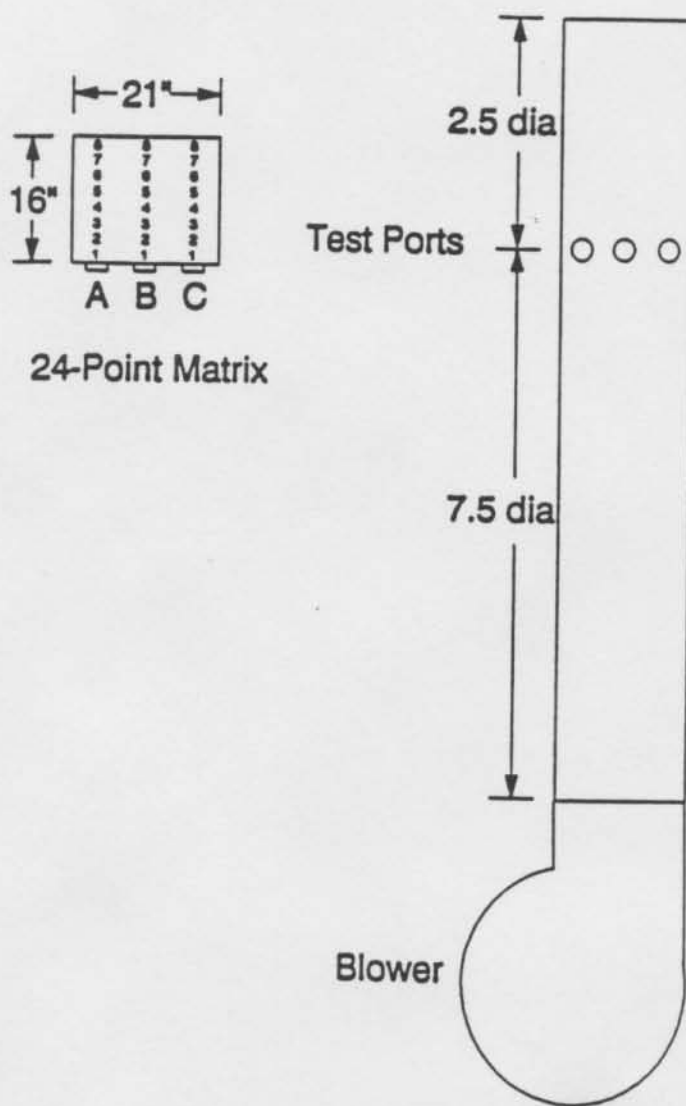
The particulate matter emissions of the waste heat boiler exhaust were determined by EPA Method 5. The sampling train is shown in Figure 3 and consisted of a glass nozzle, a Teflon union, an 36-inch glass probe, a tared Gelman type A/E glass fiber filter in a glass filter holder, a set of Greenburg-Smith impingers, a 30-foot umbilical line, a vacuum pump, a dry gas meter and a calibrated orifice connected to an inclined oil manometer. The heated probe and filter were maintained at about 250 degrees Fahrenheit. The impinger set consisted of 1 modified Greenberg-Smith impinger and 1 Greenberg-Smith impinger each containing 100 milliliters of distilled water, an empty modified Greenberg-Smith impinger, and an impinger filled with 250 grams of silica gel.

The sample was collected isokinetically for 72 minutes (4 minutes/point) generating a sample size of about 45 cubic feet through the train. The velocity and temperature were measured at each point as it was sampled. Field data and calculation sheets are shown in Appendix A.

The volume of the impinger solution and the weight of the silica gel were recorded before and after the tests in order to obtain the moisture content of the stack gas stream. The weight of the filter was also recorded before and after the tests as part of the analysis to determine the amount of particulate collected. All sample volumes and silica gel weights were recorded immediately on sample recovery sheets (Appendix A) during charging and sample recovery. Leak checks were performed before and after each test.

After the test, the nozzle, probe, and front filter bell were rinsed and brushed three times with acetone and the rinses placed in a 250-milliliter polyethylene container. The filter was recovered and placed in a plastic cassette. The sample train from the back half of the filter housing through the third impinger was rinsed three times with distilled water and these rinses were placed along with the impinger contents in a 1000-milliliter polyethylene container. Disposable vinyl gloves were worn during sample retrieval to help prevent contamination.

Balboa Pacific - ATC

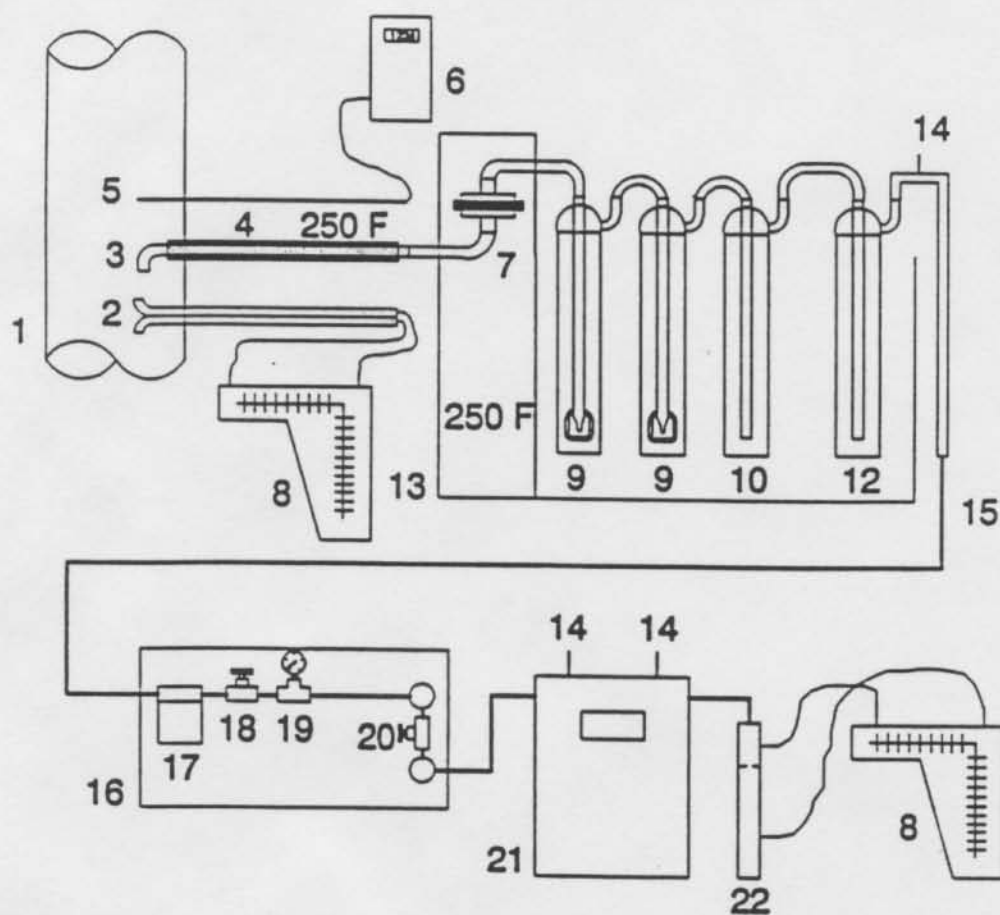


Pyrolyzer/Oxidizer/Waste Heat Boiler Exhaust

Figure 2

EPA METHOD 5

Particulate Matter



- | | |
|--|--|
| 1. Stack | 12. Modified G/S impinger charged w/silica gel |
| 2. Pitot tube | 13. Ice bath |
| 3. Glass or quartz nozzle | 14. Thermocouple |
| 4. SS probe w/glass liner | 15. Umbilical line |
| 5. Thermocouple | 16. Sealed vacuum pump |
| 6. Digital Potentiometer | 17. Pump filter |
| 7. Heated glass fiber filter | 18. Shut-off valve |
| 8. Inclined oil manometer | 19. Vacuum gage |
| 9. Greenberg/Smith impinger charged w/D.I. Water | 20. Bypass metering valve |
| 10. Modified G/S impinger empty | 21. Dry gas meter |
| 11. (Reserved) | 22. Orifice flow indicator |

Figure 3

The acetone and aqueous particulate collections were evaporated to dryness at 100 degrees Centigrade and desiccated to a constant weight along with the sample filters. The particulate matter was reported with and without the condensibles (back half impinger collection).

Metals Sampling

The metals emissions of the oxidizer exhaust were determined by EPA Method 12 modified to incorporate the analyses for total chromium, lead, manganese, copper, nickel, cadmium, beryllium, arsenic, selenium, molybdenum, silver, antimony, barium, thallium and zinc. The sampling train is shown in Figure 4 and consisted of a borosilicate glass nozzle and probe, connected by a Teflon union, a glass filter holder connected to the first two impingers, two Greenburg-Smith impingers each charged with 100 mls of 0.1N nitric acid solution, an empty impinger, an impinger filled with silica gel, a 30-foot umbilical line, a vacuum pump, a dry gas meter and a calibrated orifice connected to an inclined oil manometer. Gelman A/E glass fiber filters were used in the filter holders.

Triplicate test runs were conducted and the samples were collected isokinetically for 120 minutes (5 minutes per point) generating a sample size of about 75 cubic feet. Field data was recorded on the data sheets presented in Appendix A, which also contains the calculation sheets. The velocity and temperature were measured at each traverse point as described previously for particulates.

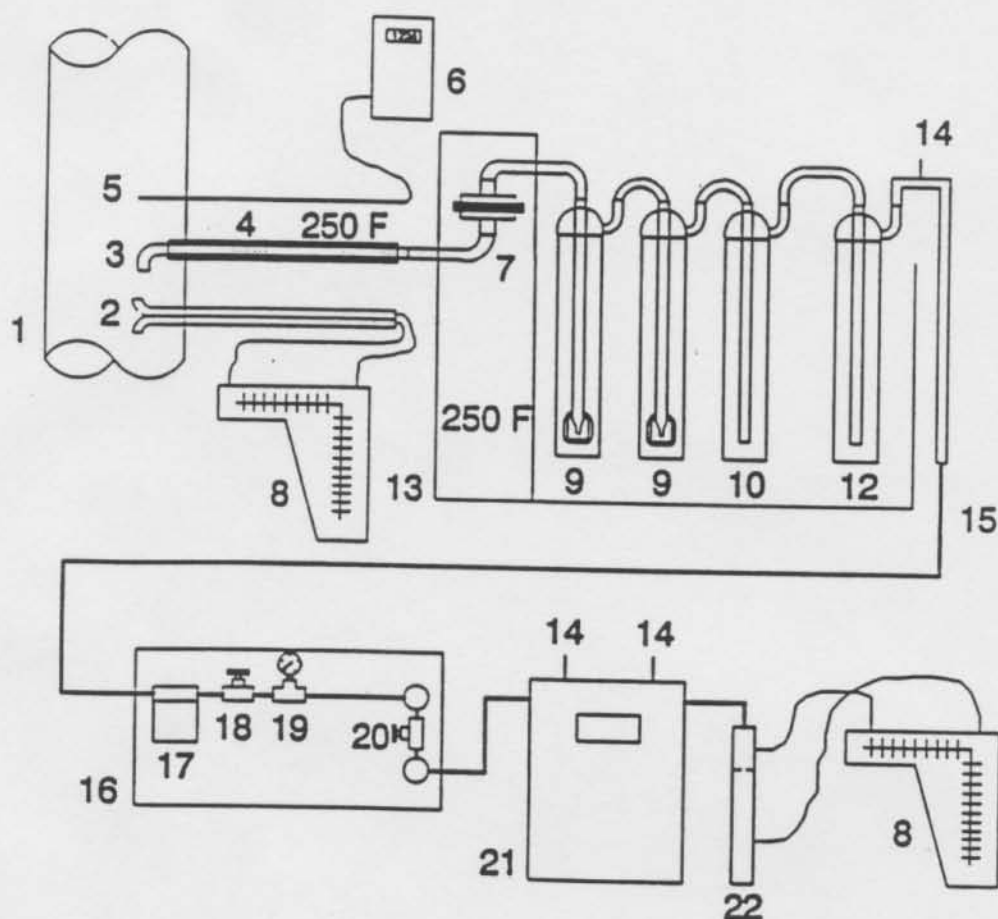
The weight of the impinger solution and the silica gel was recorded before and after the tests in order to obtain the moisture content of the stack gas stream. All sample weights were recorded immediately on sample recovery sheets (Appendix A) during charging and sample recovery. Leak checks were performed before and after the test.

After the test, the contents of each impinger set was placed in a 1000 ml. borosilicate glass container. The sampling train was then rinsed from the 3rd impinger to the nozzle with the 0.1N nitric acid solution and the rinse were added to the sample. The filter was recovered and placed in a separate container. The impinger solution and filter were kept refrigerated prior to the analyses in order to prevent degradation of the sample. Disposable vinyl gloves were worn during sample retrieval to help prevent contamination.

Laboratory analyses were conducted by West Coast Analytical Service, Inc., in Sante Fe Springs, California. Total chromium, lead, manganese, copper, nickel, cadmium, beryllium, arsenic, selenium, molybdenum, silver, antimony, barium, thallium and zinc determinations were made by ICP/MS. The laboratory report is included in Appendix B.

EPA METHOD 12

Metals



- | | |
|---|--|
| 1. Stack | 12. Modified G/S impinger charged w/silica gel |
| 2. Pitot tube | 13. Ice bath |
| 3. Glass or quartz nozzle | 14. Thermocouple |
| 4. SS probe w/glass liner | 15. Umbilical line |
| 5. Thermocouple | 16. Sealed vacuum pump |
| 6. Digital Potentiometer | 17. Pump filter |
| 7. Heated glass fiber filter | 18. Shut-off valve |
| 8. Inclined oil manometer | 19. Vacuum gage |
| 9. Greenberg/Smith impinger charged w/0.1N HNO ₃ | 20. Bypass metering valve |
| 10. Modified G/S impinger empty | 21. Dry gas meter |
| 11. (Reserved) | 22. Orifice flow indicator |

Figure 4

Continuous Monitoring

The pyrolytic chamber waste heat boiler exhaust was monitored for total hydrocarbons, CO, CO₂, O₂, SO₂ and NO_x by EPA Methods 25A, 10, 3A, 6C and 7E, respectively. A JUM Model VE-7 heated total hydrocarbon analyzer was used to determine the total hydrocarbons, two Rosemount Analytical Model 880 Infrared Analyzers were used to determine the CO and CO₂ concentrations, a Rosemount Analytical Model 755R Paramagnetic Analyzer was used to determine the oxygen concentration, a Bovar Engineering Model 721M was used to determine the SO₂ concentration, and a Thermo Electron Model 10 Chemiluminescent Analyzer was used to determine the NO_x concentration. The output of the analyzers was linearized by the manufacturers. Table 1 lists the instrument specifications.

The continuous monitoring train for the NO_x, SO₂, CO, CO₂ and O₂ is shown in Figure 5 and consisted of a 3/8-inch stainless steel sampling probe, a 3/8-inch heated Teflon sampling line, a sample refrigeration/pump system, a glass fiber filter in a 47-millimeter stainless steel holder, and a sample distribution manifold. The distribution manifold was equipped with a series of 3-way valves with flow meters (rotometer style). One flow meter acted as a bypass, and the others were connected to the individual analyzers. The output of the analyzers was logged by a Yokogawa Model HR2400 multi-channel recorder and a Rustrak Ranger II data logger. The data logger information was used to determine the arithmetic means for each analyzer run and to generate graphs of the concentration versus time (see Appendix A).

The NO_x and CO analyzers were operated in the respective ranges of 0-50 ppmv and 0-100 ppmv with span gases at about 50 and 90 percent of span. The SO₂ analyzer was operated in the 0-100 ppmv range with span gases of about 50 and 90 percent of span. The O₂ analyzer was operated on a range of 0-25 percent with span gases at about 10 and 18 percent. The CO₂ analyzer was operated on a range of 0-20 percent with span gases at about 10 and 18 percent. Prior to the source tests, the suction side of the monitoring system was leak-checked at a full vacuum (greater than 20 inches mercury). All instruments were calibrated with a zero and two upscale span gases prior to the start of testing. A zero and mid-span bias check were conducted before and after each test run. Calibration correction calculations were performed in accordance with EPA Method 6C for each instrument.

The total hydrocarbons (THC) were determined by EPA Method 25A. The THC concentrations were monitored with a JUM Model VE-7 total hydrocarbon analyzer that utilized a heated Teflon sample line and a flame ionization detector (FID) mounted in a heated oven. The sample line was maintained at 250°F, and the oven was maintained at 190°C (see Figure 6). The instrument was used on the 0-100 ppmv range and calibrated with zero, high, mid, and low span gases. The output of the analyzer was connected to a Rustrak Ranger II data logger for continuous monitoring of the total hydrocarbons. The data logger

Table 1
Continuous Monitor Specifications

NOx Chemiluminescent Analyzer - Thermo-Electron Model 10A

Response Time	1.5 sec - NO, 1.7 sec - NOx
Zero Drift	+/- 0.5% after warm up (30 min)
Span Drift	+/- 1% of full scale
Linearity	+/- 1% of full scale
Accuracy	Derived from the +/- 1% calibration gas
Output	NO 0-5.0 Vdc NOx 0-0.5 Vdc

SO2 Photometric Analyzer - Bovar Engineering Model 721M

Response Time	1.5 sec
Zero Drift	+/- 0.5% after warm up (30 min)
Span Drift	+/- 0.5% of full scale
Linearity	+/- 0.5% up to 1000 ppm
Accuracy	+/- 1% of full scale
Output	0-10.0 Vdc

O2 Paramagnetic Analyzer - Beckman Model 755R

Response Time	2 Sec
Zero Drift	+/- 1% of full scale
Span Drift	+/- 1% of full scale
Linearity	+/- 1% of full scale
Accuracy	Derived from the +/- 1% calibration gas
Output	0-1.0 Vdc

CO/CO2 Infrared Analyzers - Beckman Model 880

Response Time	2 sec.
Zero Drift	+/- 1% of full scale
Span Drift	+/- 1% of full scale
Linearity	+/- 1% of full scale
Accuracy	Derived from the +/- 1% calibration gas
Output	0-1.0 Vdc

Table 1 (cont'd)

Continuous Monitor Specifications

VOC Heated Hydrocarbon Analyzer - J.U.M. Engineering Model VE-7 FID Analyzer

Response Time	0-95% in less than 1.2 Seconds
Zero Drift	+/- 1% of Full Scale in 24 Hrs
Span Drift	+/- 1% of Full scale in 24 Hrs
Linearity	+/- 1% of Full Scale
Accuracy	Derived from the +/- 1% calibration gas
Sensitivity	1 ppb
Range Change Consistency	Less than 1% Full Scale
Oxygen Synergism	Less than 2%
Output	0-10.0 Vdc Scaled:
	R ₁ 0-10 ppm as C ₃
	R ₂ 0-100 ppm as C ₃
	R ₃ 0-1,000 ppm as C ₃
	R ₄ 0-10,000 ppm as C ₃
	R ₅ 0-100,000 ppm as C ₃
Sample Flow Rate	3 Liters/Minute

CONTINUOUS MONITORING SYSTEM

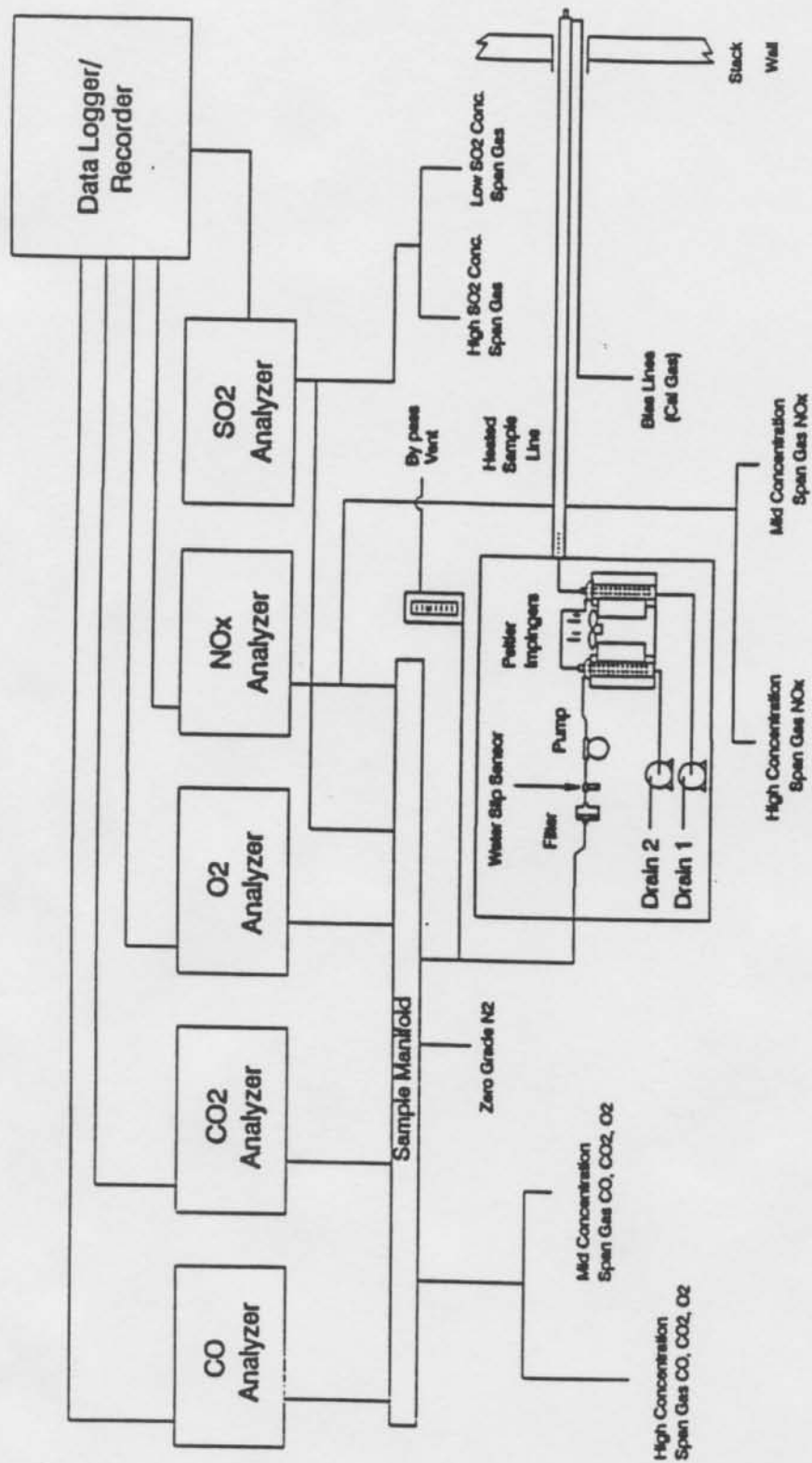


Figure 5

TOTAL HYDROCARBON SAMPLING TRAIN EPA Method 25A

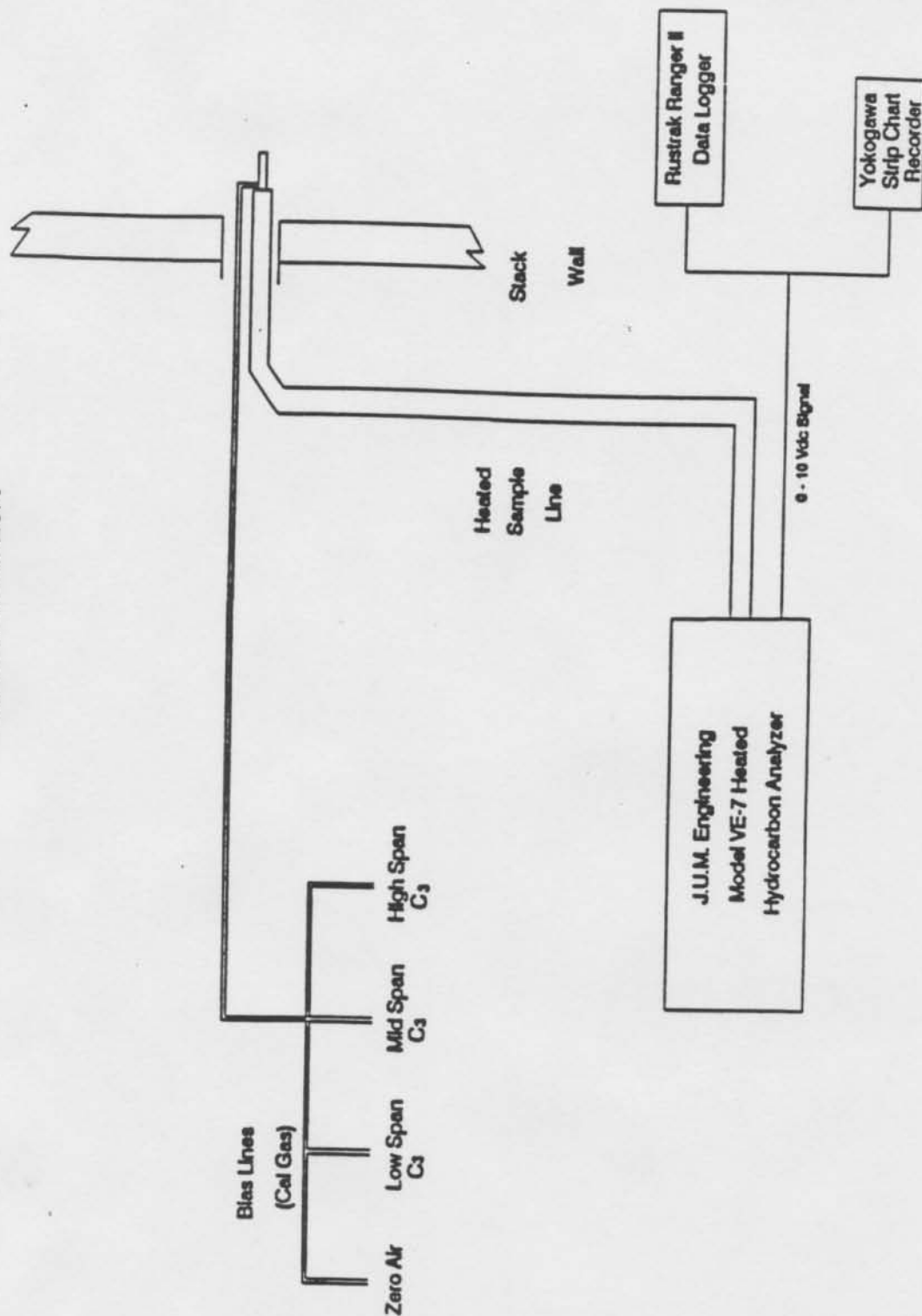


Figure 6

information was used to determine the arithmetic means for each analyzer run and to generate graphs of the concentration versus time (see Appendix A). The hydrocarbon concentrations were monitored for about a 60-minute period.

Each THC measurement was taken at a single point near the center of the duct. The analyzer was spanned before and after the test run and a bias check was performed with one span gas to check the sample line for leakage.

RESULTS

Calculations were made from the field data sheets to determine sample volume, dry gas average molecular weight, velocities, flow rate, component concentrations, and isokinetic variation for each test. The calculations are shown on the emission test calculation sheets in Appendix A.

Tables 2 and 3 summarize the results of the source tests for particulates on the initial material and the char, respectively. The results of the testing are presented along with the stack conditions present during sampling. The particulate emissions are presented in grains per dry standard cubic foot (grains/DSCF) and pounds per hour (lbs/hr).

Tables 4 and 5 summarize the results of the source tests for the gaseous components on the initial material and the char, respectively. The results of the testing for nitrogen oxides, carbon monoxide, sulfur dioxide, carbon dioxide, oxygen and total hydrocarbons are presented in parts per million by volume (ppmv) and pounds per hour (lbs/hr).

Tables 6 and 7 summarize the results of the source tests for multiple metals on the initial material and the char, respectively. The results of the testing are presented along with the stack conditions present during the sampling period. The metals emissions are presented in milligrams per dry standard cubic meter (mg/DSCM) and milligrams per hour (mg/hr).

TABLE 2

Balboa Pacific/ATC Pyrolysis Unit
Oxidizer Exhaust
Particulate Emissions
Initial Pyrolysis

Date:	9/12/95	9/13/95	9/14/95
Test Number:	Batch 1	Batch 2	Batch 3
Sample Number:	ATC-2	ATC-4	ATC-6
<u>Flue Gas</u>			
Temperature, °F	374	378	382
Velocity, ft/sec	10.2	10.5	10.5
Static Pressure, in. H ₂ O	-0.02	-0.02	-0.02
Duct Area, sq. ft.	2.33	2.33	2.33
Flow Rate, ACFM	1,430	1,470	1,470
Flow Rate, DSCFM	844	874	872
Moisture, % v/v	6.4	5.4	5.4
CO ₂ , %	2.8	2.7	2.9
O ₂ , %	16.1	16.4	16.3
<u>Particulate Matter</u>			
Sample Start	1635	1430	1120
Sample Stop	1750	1554	1330
Sampling Time, min.	72	72	72
Sample Volume, DSCF	35.6	36.9	36.9
Isokinetic Rate, %	101	101	101
Concentration, grains/DSCF			
w/condensibles	0.0026	0.0112	0.0015
w/o condensibles	0.0008	0.0097	0.0008
Emission Rate, lbs/hr			
w/condensibles	0.019	0.084	0.012
w/o condensibles	0.006	0.073	0.006

TABLE 3

Balboa Pacific/ATC Pyrolysis Unit
Oxidizer Exhaust
Particulate Emissions
Char Pyrolysis

Date:	10/3/95	10/4/95	10/4/95
Test Number:	1	2	3
Sample Number:	PM-1	PM-2	PM-3
<u>Flue Gas</u>			
Temperature, °F	437	378	379
Velocity, ft/sec	7.8	9.8	11.7
Static Pressure, in. H ₂ O	-0.005	-0.01	-0.03
Duct Area, sq. ft.	2.33	2.33	2.33
Flow Rate, ACFM	1,080	1,360	1,630
Flow Rate, DSCFM	597	796	953
Moisture, % v/v	6.0	6.7	6.6
CO ₂ , %	2.7	2.7	2.7
O ₂ , %	16.0	16.1	16.0
<u>Particulate Matter</u>			
Sample Start	0942	1015	1456
Sample Stop	1100	1133	1614
Sampling Time, min.	72	72	72
Sample Volume, DSCF	27.0	36.1	40.4
Isokinetic Rate, %	110	110	103
Concentration, grains/DSCF			
w/condensibles	0.0038	0.0039	0.0021
w/o condensibles	0.0031	0.0025	0.0018
Emission Rate, lbs/hr			
w/condensibles	0.019	0.026	0.017
w/o condensibles	0.016	0.017	0.015

TABLE 4

Balboa Pacific/ATC Pyrolysis Unit
Oxidizer Exhaust
Continuous Monitoring of Gases
Initial Pyrolysis

Date:	9/12/95	9/13/95	9/14/95
Test Number:	Batch 1	Batch 2	Batch 3
Sample Start	2111	1520	1215
Sample Stop	2211	1620	1315
Sampling Time, min.	60	60	60
Concentration, %			
Carbon Dioxide	2.8	2.7	2.9
Oxygen	16.1	16.4	16.3
Concentration, ppmv			
Carbon Monoxide	62.8	38.2	37.8
Total HC (as C ₃)	8.1	0.2	0.3
Sulfur Dioxide	0.0	0.7	0.0
Nitrogen Oxides	28.3	26.2	30.9
Emission Rate, lbs/hr			
Carbon Monoxide	0.23	0.15	0.17
Total HC (as C ₃)	0.05	0.01	0.01
Sulfur Dioxide	0.00	0.01	0.00
Nitrogen Oxides	0.17	0.17	0.23

TABLE 5
Balboa Pacific/ATC Pyrolysis Unit
Oxidizer Exhaust
Continuous Monitoring of Gases
Char Pyrolysis

Date:	10/3/95	10/3/95	10/3/95
Test Number:	1	2	3
Sample Start	1148	1346	1540
Sample Stop	1248	1446	1640
Sampling Time, min.	60	60	60
Concentration, %			
Carbon Dioxide	2.7	2.7	2.7
Oxygen	16.0	16.1	16.0
Concentration, ppmv			
Carbon Monoxide	32.0	28.1	28.6
Total HC (as C ₃)	3.8	3.0	3.3
Sulfur Dioxide	0.5	0.1	0.3
Nitrogen Oxides	27.6	23.5	23.3
Emission Rate, lbs/hr			
Carbon Monoxide	0.08	0.10	0.12
Total HC (as C ₃)	0.02	0.02	0.02
Sulfur Dioxide	0.02	0.02	0.03
Nitrogen Oxides	0.12	0.14	0.16

TABLE 6

**Balboa Pacific/ATC Pyrolysis Unit
Oxidizer Exhaust
Toxic Metals Emissions
Initial Pyrolysis**

Date:	9/13/95	9/14/95	9/15/95
Test Number:	Batch 1	Batch 2	Batch 3
Sample Number:	ATC-3	ATC-6	ATC-7
Flue Gas			
Temperature, °F	388	393	384
Velocity, ft/sec	9.4	12.5	11.1
Static Pressure, in. H ₂ O	-0.02	-0.02	-0.02
Duct Area, sq. ft.	2.33	2.33	2.33
Flow Rate, ACFM	1,320	1,750	1,550
Flow Rate, DSCFM	766	1,010	909
Moisture, % v/v	6.4	6.2	6.1
CO ₂ , %	2.8	2.7	2.9
O ₂ , %	16.1	16.4	16.3
Metals			
Sample Start	1125	1120	1047
Sample Stop	1335	1330	1253
Sampling Time, min.	120	120	120
Sample Volume, DSCF	54.3	70.8	62.7
Isokinetic Rate, %	103	101	100
Concentration, mg/DSCM			
Copper	8.30E-4	4.52E-4	2.72E-4
Chromium	4.61E-4	3.83E-4	4.66E-4
Lead	4.01E-4	2.43E-4	2.41E-4
Zinc	3.18E-3	1.67E-3	2.25E-3
Manganese	1.84E-4	1.39E-4	1.94E-4
Nickel	3.83E-4	1.63E-4	2.02E-4
Cadmium	< 9.22E-5	1.74E-4	1.94E-4
Beryllium	< 4.61E-5	< 3.48E-5	< 3.88E-5
Arsenic	1.06E-4	1.01E-4	9.32E-5
Selenium	< 3.23E-4	< 2.43E-4	< 2.72E-4
Molybdenum	3.88E-2	8.69E-2	9.59E-2
Silver	< 4.61E-6	< 3.48E-6	< 3.88E-6
Antimony	< 1.38E-4	< 1.04E-4	< 1.17E-4
Barium	1.50E-3	1.15E-3	1.33E-3
Thallium	< 4.61E-06	< 3.48E-06	< 3.88E-6

TABLE 6 (cont'd)

Balboa Pacific/ATC Pyrolysis Unit
Oxidizer Exhaust
Toxic Metals Emissions
Initial Pyrolysis

Date:	9/13/95	9/14/95	9/15/95
Test Number:	Batch 1	Batch 2	Batch 3
Sample Number:	ATC-3	ATC-6	ATC-7
Emission Rate, mg/hr			
Copper	1.1	0.8	0.4
Chromium	0.6	0.7	0.7
Lead		0.5	0.40.4
Zinc	4.1	2.9	3.5
Manganese	0.2	0.2	0.3
Nickel	0.5	0.3	0.3
Cadmium	< 0.1	0.3	0.3
Beryllium	< 0.1	< 0.1	< 0.1
Arsenic	0.1	0.2	0.1
Selenium	< 0.4	< 0.4	< 0.4
Molybdenum	51	150	150
Silver	< 0.1	< 0.1	< 0.1
Antimony	< 0.2	< 0.2	< 0.2
Barium	2.0	2.0	2.1
Thallium	< 0.1	< 0.1	< 0.1

TABLE 7

Balboa Pacific/ATC Pyrolysis Unit
Oxidizer Exhaust
Toxic Metals Emissions
Char Pyrolysis

Date:	10/3/95	9/14/95	9/15/95
Test Number:	Set 2	Set 2	Set 2
Sample Number:	MM1/ATC2	MM2/ATC2	MM3/ATC3
<u>Flue Gas</u>			
Temperature, °F	381	383	380
Velocity, ft/sec	9.4	12.1	9.8
Static Pressure, in. H ₂ O	0.01	0.04	-0.02
Duct Area, sq. ft.	2.33	2.33	2.33
Flow Rate, ACFM	1,320	1,690	1,380
Flow Rate, DSCFM	776	990	801
Moisture, % v/v	5.9	6.3	6.7
CO ₂ , %	2.7	2.7	2.7
O ₂ , %	16.0	16.1	16.0
<u>Metals</u>			
Sample Start	1100	1415	1220
Sample Stop	1336	1618	1425
Sampling Time, min.	120	120	120
Sample Volume, DSCF	58.4	70.3	57.4
Isokinetic Rate, %	105	99.6	100
Concentration, mg/DSCM			
Copper	5.46E-4	3.21E-4	4.41E-4
Chromium	2.73E-4	< 2.14E-4	3.09E-4
Lead	5.77E-4	2.67E-4	< 1.76E-4
Zinc	4.96E-3	2.32E-3	2.16E-2
Manganese	1.82E-4	1.43E-4	1.32E-4
Nickel	4.09E-4	< 3.21E-4	8.37E-4
Cadmium	1.36E-5	1.07E-4	< 3.09E-4
Beryllium	< 4.55E-5	< 3.57E-5	< 1.32E-4
Arsenic	< 4.55E-6	< 3.57E-6	2.20E-5
Selenium	< 4.55E-4	< 3.57E-4	< 8.81E-4
Molybdenum	3.64E-2	2.11E-2	1.32E-1
Silver	< 4.55E-6	< 3.57E-6	< 4.41E-6
Antimony	< 9.09E-5	< 7.13E-5	< 1.32E-4
Barium	1.82E-4	1.07E-4	6.17E-4
Thallium	< 9.09E-06	< 7.13E-06	< 4.41E-6

TABLE 7 (cont'd)

Balboa Pacific/ATC Pyrolysis Unit
Oxidizer Exhaust
Toxic Metals Emissions
Char Pyrolysis

Date:	10/3/95	9/14/95	9/15/95
Test Number:	Set 2	Set 2	Set 2
Sample Number:	MM1/ATC2	MM2/ATC2	MM3/ATC3
Emission Rate, mg/hr			
Copper	0.72	0.54	0.60
Chromium	0.36	< 0.36	0.42
Lead	0.76	0.45	< 0.24
Zinc	6.5	3.9	29
Manganese	0.24	0.24	0.18
Nickel	0.54	< 0.54	1.1
Cadmium	0.18	0.18	< 0.42
Beryllium	< 0.06	< 0.06	< 0.18
Arsenic	< 0.01	< 0.01	0.03
Selenium	< 0.60	< 0.60	< 1.2
Molybdenum	48	36	180
Silver	< 0.01	< 0.01	< 0.01
Antimony	< 0.12	< 0.12	< 0.18
Barium	0.24	0.18	0.84
Thallium	< 0.01	< 0.01	< 0.01

QUALITY ASSURANCE/QUALITY CONTROL

Source tests are performed to determine the types and amounts of pollutants emitted by a source. Information from this source test program may be used for obtaining permits, evaluating control equipment performance, updating emission inventories, and determining compliance with present and future emission regulations. For these purposes, reliable data are required. PES provides this reliability by using the following work practices:

Use Of Standard Test Procedures

EPA Methods 1 and 2 were utilized to measure flow rates. EPA Method 5 was used to determine the total particulate emission rates, EPA Method 12 was used to determine the metals emissions, and EPA Methods 3A, 6C, 7E, 10 and 25A were used to determine the continuous emission rates for the gases. A procedure must be thoroughly studied under various conditions in order to be designated as a state or federal Method. Results of many executions of the procedure are compared to demonstrate accuracy and repeatability before adoption of the procedure as a source testing method.

Use Of Trained Test Personnel

Because of the complexity of typical source testing methods, testers should be trained and experienced with the test procedures in order to assure reliable results. PES personnel have had professional training and routinely conduct source tests.

Knowledge Of Source's Operation

The source testing team should have sufficient knowledge of the process to be tested in order to properly document the process parameters during the tests. Without documentation of the process parameters used, results are much less meaningful. PES has previously tested boilers and combustion sources and is familiar with the processes and equipment.

Equipment Maintenance and Calibration

Use of properly maintained and calibrated test equipment is essential for minimizing systematic errors in results. All sampling devices were constructed, maintained, and calibrated as suggested in EPA documents APTD-0576, and APTD-0581 (These are commonly accepted construction and maintenance manuals for source testing equipment).

The dry gas meters were calibrated with a transfer gas meter with NBS traceability. These calibrations are included in Appendix C along with those for the nozzles, thermocouples, digital potentiometers, and Pitot tubes.

Quality control procedures used for continuous monitoring included the use of non-reactive 316 stainless steel or Teflon tubing and fittings throughout the system. A 2-pass refrigeration unit was used with the pump downstream of the sample gas conditioner. All instrumentation was continuously monitored and checked between load conditions to insure data reliability during all sample runs. Bias checks were made with a calibration gas blend to confirm they met the tolerances specified in the EPA Methods.

All calibration gases were ± 1 per cent accuracy and provided by Scott Specialty Gases in San Bernardino, California.

Thorough Record Keeping

All data relating to the operation of the sampling train must be immediately recorded to ensure that it is not lost or misinterpreted. PES accomplishes this thorough record keeping by use of the field data sheets shown in Appendix A. The PES test team is familiar with these sheets and the information required to complete them. Any unusual occurrences in the process operation, unusual test instrument readings, or any other items that could affect the test results were also noted.

Use Of Thoroughly Cleaned Glassware

All glassware and probe lines were cleaned prior to the tests with hot tap water and detergent. The trains were then rinsed with laboratory grade distilled water, air dried, and sealed until the tests.

Use Of Standardized Data Reduction Techniques

Data reduction was accomplished by the use of step by step calculation sheets. The calculations were systematic and easy to follow. All calculations for the source test are included in Appendix A.

Submission Of Blank Samples

Filter and reagent samples were analyzed with the particulate samples to detect any possible contamination of sampling media or problems with lab analyses. No corrections were made to the measured concentrations of the collected samples, but the blank results were reported on the calculation sheets.

APPENDIX A
FIELD DATA AND CALCULATION SHEETS

Plant ATC-Bal. Pac.
 Date 1-17-74
 Sampling Location W113 Exhaust
 Sample Type EPA 5
 Run Number ATC-2
 Operator NJ
 Ambient Temperature 90
 Barometric Pressure 29.87
 Static Pressure -0.02
 Filter Number(s) _____
 Pretest Leak Rate 0.005 CFM @ 5 in. Hg
 Read And Record All Data Every 3 Minutes

Probe Length and Type 2' 6/1003
 Pilot Tube I.D. No. 5-3B
 Nozzle I.D. No. And Diameter 16 0.4775
 Assumed Moisture, % 6
 Meter Box Number 1A
 Meter Delta H @ 1.861
 C Factor ~
 Meter Gamma 1.021
 Heater Box Setting 250
 Reference Delta P ~
 Post test Leak Rate 0.005 CFM @ 7 in. Hg
 Impinger Box No. 9523 Blank Box No. _____

Schematic of
 Traverse Point Layout

Traverse Point Number	Sampling Time (minutes)	Clock Time (24 hr clock)	Gas Meter Reading Vm (cubic feet)	Velocity Head P _h (in. H ₂ O)	Orifice Pressure Differential (in. H ₂ O) ΔH		Stack Temp. T _s (F)	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
					Desired	Actual		Inlet T _m in (F)	Outlet T _m out (F)				
1	0	1635	915.723	0.022	0.86	0.86	324	106	105	2.0	236	217	60
2	3		917.332	0.015	0.64	0.64	323	106	105	2.0	234	215	57
3	6		917.692	0.010	0.43	0.43	340	106	105	2.0	234	215	56
4	9		918.835	0.020	0.86	0.86	342	106	105	2.0	240	249	55
5	12		910.544	0.015	0.64	0.64	388	103	105	2.0	235	237	53
6	15		911.935	0.015	0.64	0.64	394	105	106	2.0	241	252	56
7	18		913.392	0.020	0.86	0.86	354	105	106	2.0	247	252	55
8	21		914.711	0.010	0.43	0.43	323	105	105	2.0	243	252	53
1	24	1657/1700	916.265	0.010	0.43	0.43	327	105	105	2.0	242	251	53
2	27		917.426	0.010	0.43	0.43	356	105	105	2.0	240	251	53
3	30		918.563	0.015	0.64	0.64	353	105	105	2.0	242	250	53
4	33		921.018	0.015	0.64	0.64	377	105	106	2.0	243	251	53
5	36		921.320	0.020	0.86	0.86	384	105	105	2.0	242	251	53
6	39		922.523	0.015	0.64	0.64	384	105	105	2.0	240	252	56
7	42		924.325	0.020	0.86	0.86	355	110	106	2.0	243	253	60
8	45		925.893	0.020	0.86	0.86	376	105	105	2.0	244	252	57
1	48	1724/1726	927.423	0.020	0.86	0.86	341	105	105	2.0	240	253	60
2	51		927.155	0.020	0.86	0.86	371	105	105	2.0	243	252	57
3	54		930.634	0.030	1.25	1.25	372	105	105	2.0	241	252	55
4	57		932.426	0.035	1.50	1.50	386	105	105	2.0	241	252	56
5	60		934.419	0.040	1.71	1.71	342	105	105	2.0	241	252	57
6	63		936.442	0.050	2.14	2.14	395	105	105	2.0	244	252	57
7	66		938.725	0.050	2.14	2.14	356	110	105	2.0	243	252	57
8	69		941.170	0.040	1.71	1.71	391	110	104	2.0	241	252	56
9	72	1750	943.354							4.0	241	252	56

PACIFIC ENVIRONMENTAL SERVICES, INC.

$$\theta = 72^\circ \quad V_m = 37.431 \quad \bar{V}_p = 0.145 \quad \Delta P = 0.955 \quad T_{s,314} + 460 \quad T_m = 107 + 460 = 567$$

SAMPLE RETRIEVAL DATA

Plant: Balboa Pacific Corporation
 Date: 9.12.75
 Sampling Location: _____
 Sampling Type (Method): EDN 5
 Run Number: WTC-201 ATC-2
 Sample Box Number: 5B
 Clean-up Man: NN
 Job Number: _____
 Comments: _____ scale 255
cal 294.9

Filter

Filter Number: 0.4574
 Description of Filter: _____

Moisture

	# 1	# 2	# 3
Impingers:			
Final Volume:	<u>614.5</u> mL	<u>545.1</u> mL	<u>577.1</u> mL
Initial Volume:	<u>584.9 (100)</u> mL	<u>577.9 (100)</u> mL	<u>574.2 (0)</u> mL
Net Volume:	<u>29.6</u> mL	<u>7.2</u> mL	<u>2.9</u> mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	<u>283.3</u> g	_____ g	_____ g
Initial Volume:	<u>771.5</u> g	_____ g	_____ g
Net Volume:	<u>11.8</u> g	_____ g	_____ g
Total Moisture:	_____ g	_____ g	_____ g

51.5

Description of Impinger catch: _____

PES Inc.

EPA Methods 5 Calculations

Plant ATC - Balboa Pacific
 Project # 5102
 Operation Pyrolytic Waste Incinerator
 Run 1 - Particulate
 Location Santa Fe Springs, CA
 Date 9/12/95

Emission Data

Vlc =	51.5 cc	Vol. of H2O collected (impingers)
Vm =	37.431 cf	Dry gas meter reading
Pb =	29.87 in. Hg	Barometric pressure
Ps =	29.87 in. Hg	Stack pressure
dP =	0.145	Average sq.rt delta P
dH =	0.955 in. H2O	Average draft gauge reading
Tm =	566.6 R	Average meter temperature
Ts =	833.60 R	Average stack temperature
Dn =	0.499 in.	Nozzle diameter
Y =	1.021	Meter calibration factor
t =	72 min.	Duration of sampling time
A =	2.3300 sq.ft.	Cross sectional area of stack
Cp =	0.84	Pitot tube coefficient
Kp =	85.49	Pitot tube constant
K1 =	17.64 R/in.Hg	constant
K2 =	0.04707 cu.ft/ml	constant
K3 =	0.002669 in.Hg-cf/ml-R	constant

1) Volume of gas sampled at standard conditions, Vmstd
 $Vmstd = K1 * Y * Vm * (Pb + dH/13.6) / Tm$

Vmstd = 35.62 cu.ft
 1.01 cu.m

2) Volume of water vapor collected at standard conditions.

$Vw(std) = K2 * Vlc$

Vw(std) = 2.42 scf

3) Decimal fraction of moisture by volume in stack gas

$$Bws = Vwstd / (Vmstd + Vwstd)$$

$$Bws = 0.064$$

4) Molecular weight of the stack gas on a dry basis M_d .

$$Ms = ((44 * \%CO_2) + (28 * \%CO) + (32 * \%O_2) + (28 * \%N_2))$$

$$Ms = 29.10$$

Instrumental gas analysis

% CO ₂	2.83
% CO	0
% O ₂	16.06
% N ₂	81.11

5) Average stack gas velocity.

$$vs = Kp * Cp * (dP^{0.5}) * (Ts / Ps * Md)^{.5}$$

$$vs = 10.20 \text{ ft/sec}$$

6) Average actual stack gas volumetric flowrate.

$$Q = 60 * vs * As$$

$$Q = 1425.71 \text{ cfm}$$

$$40.38 \text{ cmm}$$

7) Average stack gas dry volumetric flowrate.

$$Qstd = Q * (Tstd / Ts) * (Ps / Pstd)$$

$$Qstd = 844.05 \text{ dscfm}$$

$$23.90 \text{ dscmm}$$

8) Analytical data

a) Front half acetone wash

0.0013 g wash net wt
0 g acetone blank net wt
100 ml blank vol.
152 ml Final wash volume
152 ml aliquot

0.0013 g soluble particulate*

b) Front half glass microfibre filter

0.0006 g filter net wt

c) Back half water wash - soluble

0.0041 g net wt
0 g water blank net wt
220 ml blank vol
550 ml Final wash volume
550 ml aliquot

0.0041 g soluble net wt*

* Weights are not blank corrected

9) Particulate concentrations

0.0008 grains/dscf Front 1/2
0.0026 grains/dscf Total

11) Particulate emission rate

Conc. * (1 lb/7000 gr) * Qstd * 60 min/hr

W = 0.006 lbs/hr Front 1/2
W = 0.019 lbs/hr Total Particulate

12) Isokinecity

An = 0.001 ft² Area of nozzle orifice

$\% I = 100 * Ts * ((K3 * Vlc + (Vm * Y / Tm) (Pb + dH / 13.6)) / (60 * t * Ps * vs * An))$

$\% I = 100.61$



Plant ATC - Beal Pass
 Date 9-15-93
 Sampling Location 101 H.D. E' x 100 W' S
 Sample Type EPA 17
 Run Number ATC-7
 Operator UN
 Ambient Temperature 80
 Barometric Pressure 29.85
 Static Pressure -0.02
 Filter Number(s) _____
 Pretest Leak Rate 0.018 CFM @ 5 in. Hg
 Read And Record All Data Every 5 Minutes

Probe Length and Type 3' Glass
 Pitot Tube I.D. No. S-2A
 Nozzle I.D. No. And Diameter N-6 0.495
 Assumed Moisture, % 6
 Meter Box Number 1A
 Meter Delta H @ 1.861
 C Factor _____
 Meter Gamma 1.021
 Heater Box Setting 250
 Reference Delta P _____
 Post test Leak Rate 0.015 CFM @ 5.5 in. Hg
 Impinger Box No. 323 Blank Box No. _____

Schematic of
Traverse Point Layout

Traverse Point Number	Sampling Time (minutes)	Clock Time (24 hr clock)	Gas Meter Reading Vm (cubic feet)	Velocity Head Ps (in. H2O)	Orifice Pressure Differential (in. H2O) ΔH		Stack Temp. Ts (F)	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
					Desired	Actual		Inlet Tm in (F)	Outlet Tm out (F)				
1	0	1643	167.721	0.000	0.41	0.41	230	97	97	2.0	226	250	60
2	5	1042	164.633	0.02	0.83	0.83	236	97	97	2.0	254	255	57
3	10	1037	167.092	0.03	1.24	1.24	350	99	97	3.0	255	253	60
4	15	1102	160.015	0.025	1.04	1.04	359	100	97	2.0	255	263	57
5	20	1107	173.223	0.02	0.83	0.83	405	103	97	2.0	255	255	56
6	25	1113	174.633	0.02	0.83	0.83	406	104	97	2.0	252	282	53
7	30	1117	180.325	0.02	0.83	0.83	406	105	100	2.0	253	297	58
8	35	1122	180.325	0.01	0.41	0.41	356	103	103	2.0	252	258	53
9	40	1127	183.095	0.01	0.41	0.41	366	106	103	2.0	247	262	60
10	45	1135	183.095	0.01	0.41	0.41	389	107	103	2.0	248	257	57
11	50	1140	186.865	0.01	0.41	0.41	406	107	105	2.0	254	264	57
12	55	1141	188.554	0.015	0.62	0.62	406	107	105	2.0	251	225	54
13	60	1150	190.462	0.015	1.04	1.04	410	108	105	2.0	257	266	53
14	65	1155	193.675	0.03	1.24	1.24	409	111	105	2.0	254	264	57
15	70	1200	196.451	0.03	1.24	1.24	410	112	108	2.0	251	263	54
16	75	1205	199.507	0.03	1.24	1.24	411	113	107	3.0	253	265	56
17	80	1210/1213	202.543	0.015	0.62	0.62	309	112	108	2.0	247	257	60
18	85	1214	204.735	0.02	0.83	0.83	335	111	108	2.0	247	257	66
19	90	1223	208.265	0.025	1.04	1.04	372	112	108	3.0	247	256	54
20	95	1228	210.222	0.035	1.45	1.45	398	112	108	3.0	251	257	64
21	100	1233	213.465	0.040	1.66	1.66	405	113	107	4.0	247	256	56
22	105	1238	216.917	0.045	1.87	1.87	407	113	107	4.5	247	256	57
23	110	1243	220.622	0.05	2.07	2.07	408	112	107	5.0	247	223	57
24	115	1248	224.471	0.056	2.28	2.28	405	113	107	5.0	248	268	60
25	120	1253	228.546	0.056									

SAMPLE RETRIEVAL DATA

Plant: ATC
Date: 9.15.95
Sampling Location: _____
Sampling Type (Method): CPR 12
Run Number: ATC-7
Sample Box Number: 3R
Clean-up Man: NN
Job Number: _____
Comments: Sample P 997.4
T 320.0

Filter

Filter Number: _____
Description of Filter: _____

Moisture

Impingers:			
Final Volume:	<u>702.3</u> mL	<u>620.9</u> mL	<u>480.3</u> mL
Initial Volume:	<u>640.6</u> mL	<u>614.3</u> mL	<u>474.5</u> mL
Net Volume:	<u>61.7</u> mL	<u>6.6</u> mL	<u>1.8</u> mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	<u>700.1</u> g	_____ g	_____ g
Initial Volume:	<u>684.0</u> g	_____ g	_____ g
Net Volume:	<u>16.1</u> g	_____ g	_____ g
Total Moisture:	_____ g	_____ g	_____ g

16.1

Description of Impinger catch: _____

PES, Inc.
Multi-Metals Method Calculations (EPA 12)

Plant ATC-Balboa Pacific
Project # 5102
Operation Pyrolytic Oxidation Unit
Run Batch 1
Location Outlet
Date 9/13/95

Test Data

Vlc =	79.4 cc	Vol. of H2O collected (impingers)
Vm =	57.373 cf	Dry gas meter reading
Pb =	29.85 in. Hg	Barometric pressure
Ps =	29.85 in. Hg	Stack pressure
dP =	0.131	Average sq.rt delta P
dH =	0.794 in. H2O	Average draft gauge reading
Tm =	569.1 R	Average meter temperature
ts =	848.25 R	Average stack temperature
Dn =	0.495 in.	Nozzle diameter
Y =	1.021	Meter calibration factor
t =	120 min.	Duration of sampling time
A =	2.3300 sq.ft.	Cross sectional area of stack
Cp =	0.84	Pitot tube coefficient
Kp =	85.49	Pitot tube constant
K1 =	17.64 R/in.Hg	constant
K2 =	0.04707 cu.ft/ml	constant
K3 =	0.002669 in.Hg-cf/ml-R	constant

Instrumentation Data

[O2] = 16.1 %
[CO2] = 2.8 %

CALCULATIONS

1) Volume of gas sampled at standard conditions, Vmstd
Vmstd = $K1 \cdot Y \cdot Vm \cdot (Pb + dH/13.6)/Tm$

Vmstd = 54.31 cu.ft
 1.54 cu.m

2) Volume of water vapor collected at standard conditions.
 $V_w(\text{std}) = K_2 \cdot V_{lc}$

$$V_w(\text{std}) = 3.74 \text{ scf}$$

3) Decimal fraction of moisture by volume in stack gas
 $B_{ws} = V_{wstd}/(V_{mstd} + V_{wstd})$

$$B_{ws} = 0.064$$

4) Molecular weight of the stack gas on a dry basis M_d .

$$M_d = (1 - B_{ws}) \cdot ((44\% \text{CO}_2) + (28\% \text{CO}) + (32\% \text{O}_2) + (28\% \text{N}_2)) + (18 \cdot B_{ws})$$

$$M_d = 28.38$$

5) Average stack gas velocity.

$$v_s = K_p \cdot C_p \cdot (dP^{0.5}) \cdot (T_s/P_s \cdot M_d)^{.5}$$

$$v_s = 9.43 \text{ ft/sec}$$

6) Average actual stack gas volumetric flowrate.

$$Q = 60 \cdot v_s \cdot A_s$$

$$Q = 1317.85 \text{ cfm}$$
$$37.32 \text{ cmm}$$

7) Average stack gas dry volumetric flowrate.

$$Q_{std} = Q \cdot (T_{std}/T_s) \cdot (P_s/P_{std})$$

$$Q_{std} = 765.66 \text{ dscfm}$$
$$21.68 \text{ dscmm}$$

8) Toxic metal concentrations and emission rates

Element	Sample Mass (ug)	Blank Mass (ug) DL	Conc. (mg/dscm)	Emission Rate (mg/hr)
Copper	18.00	1.00	8.30E-04	1.1E+00
Chromium	10.00	2.00	4.61E-04	6.0E-01
Lead	8.70	0.20	4.01E-04	5.2E-01
Zinc	69.00	8.00	3.18E-03	4.1E+00
Manganese	4.00	1.00	1.84E-04	2.4E-01
Nickel	8.30	0.40	3.83E-04	5.0E-01
Cadmium	2.00	2.00	9.22E-05	1.2E-01
Beryllium	1.00	1.00	4.61E-05	6.0E-02
Arsenic	2.30	0.20	1.06E-04	1.4E-01
Selenium	7.00	7.00	3.23E-04	4.2E-01
Molybdenum	842.00	3.00	3.88E-02	5.1E+01
Silver	0.10	0.10	4.61E-06	6.0E-03
Antimony	3.00	3.00	1.38E-04	1.8E-01
Barium	32.60	0.40	1.50E-03	2.0E+00
Thallium	0.10	0.10	4.61E-06	6.0E-03

9) Isokineticity

An = 0.001 ft² Area of nozzle orifice

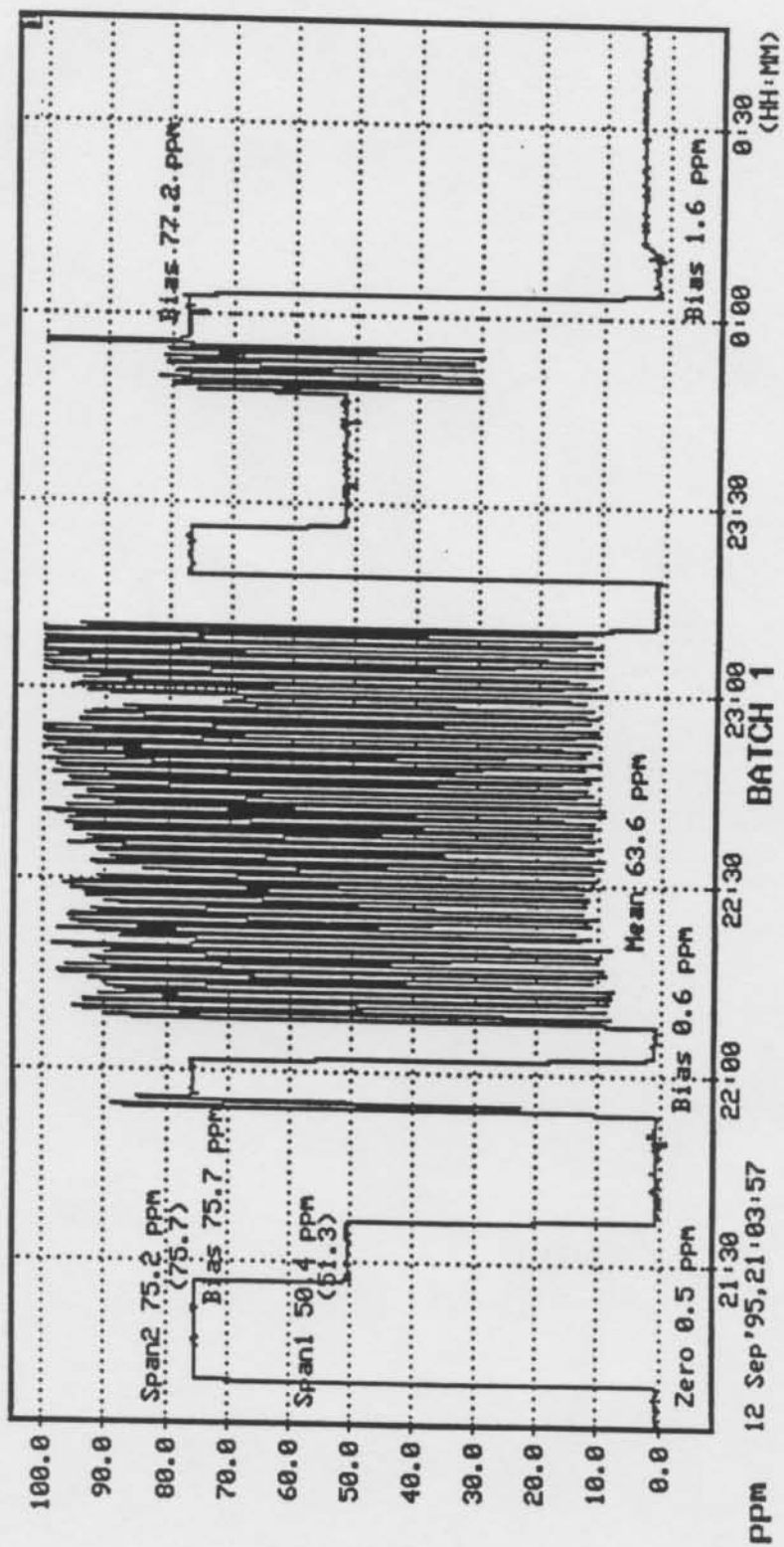
$$\% I = 100 \cdot T_s \cdot ((K_3 \cdot V_{lc} + (V_m \cdot Y / T_m) \cdot (P_b + dH / 13.6)) / (60 \cdot t \cdot P_s \cdot v_s \cdot A_n))$$

% I = 103.10

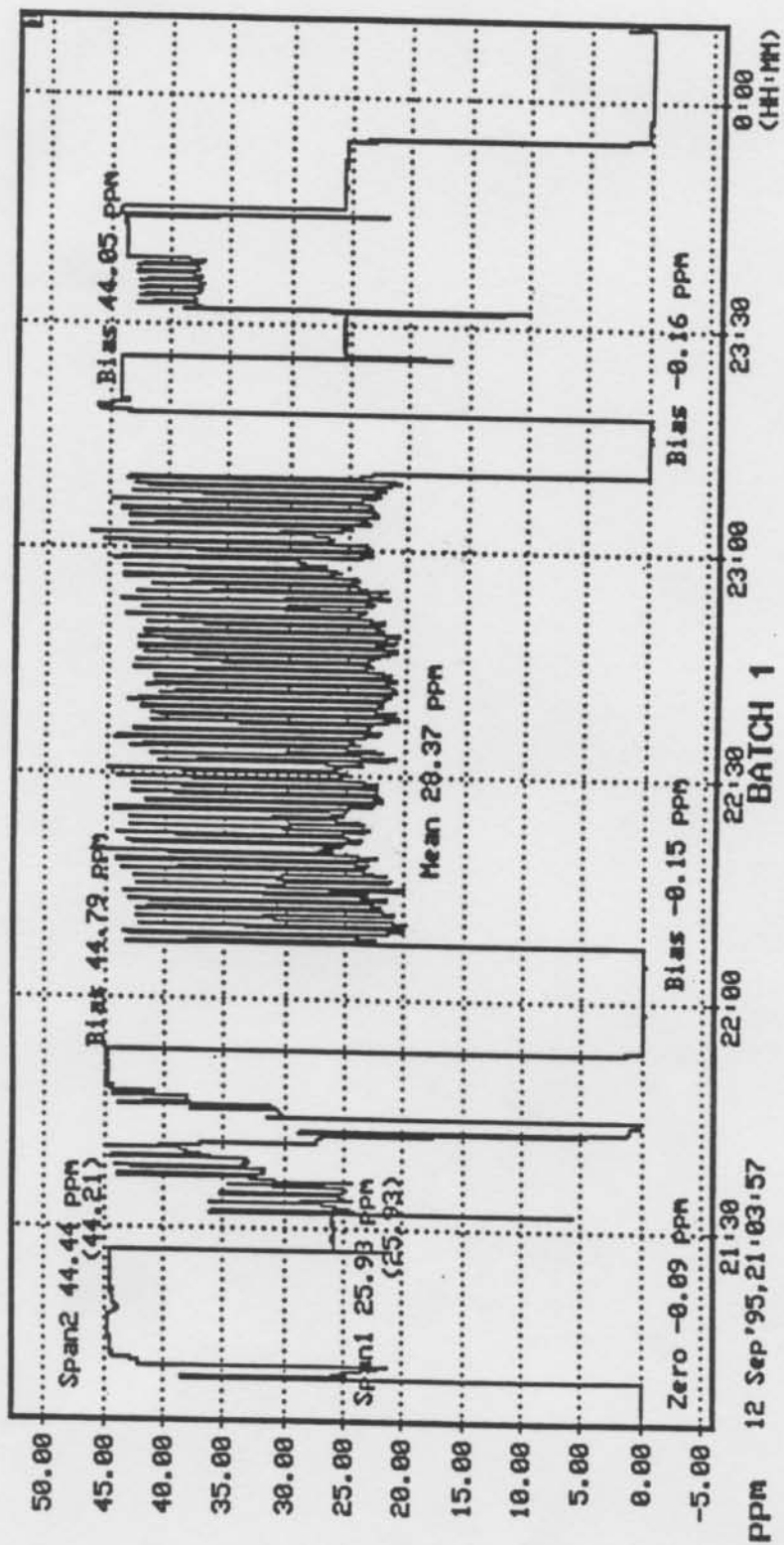
Sample Train Operation Data

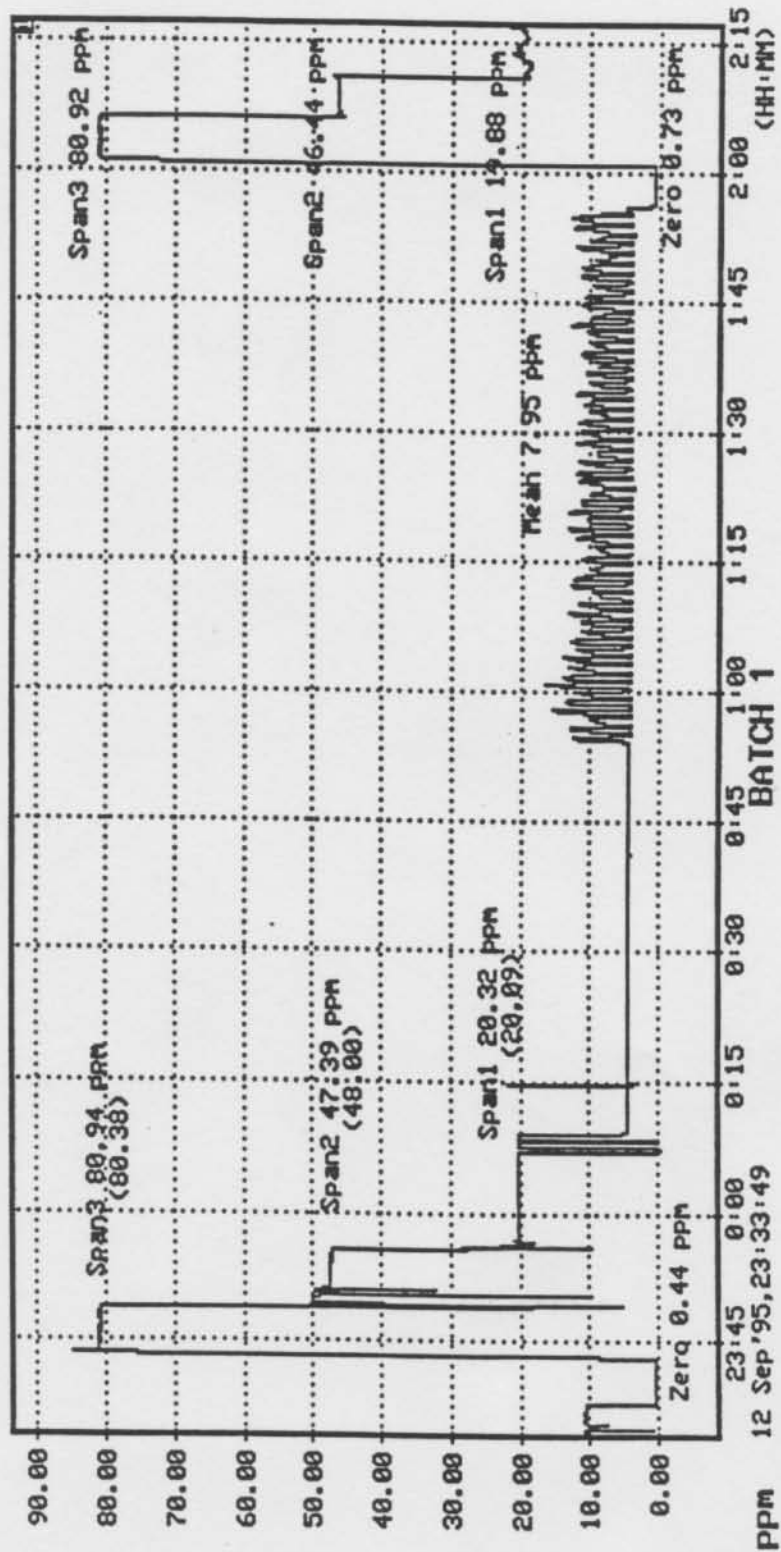
Test Date 9/13/95
 Barometer 29.85 in.Hg
 Run # 1
 Static P -0.02 in.H2O
 Pitot Cp 0.84
 Nozzle 0.495

Traverse Point	Delta-P (in. H2O)	Temp. (Deg.F)	delta H	Dry Gas Meter Temp IN	Meter Temp OUT	(dP) ^{.5}
A-1	0.01	279	0.42	105	103	0.1
A-2	0.01	379	0.42	105	103	0.1
A-3	0.01	395	0.42	106	104	0.1
A-4	0.01	403	0.42	108	105	0.1
A-5	0.01	403	0.42	109	105	0.1
A-6	0.01	401	0.42	109	105	0.1
A-7	0.01	401	0.42	109	106	0.1
A-8	0.01	392	0.42	110	106	0.1
B-1	0.01	345	0.42	108	106	0.1
B-2	0.01	360	0.42	109	107	0.1
B-3	0.01	395	0.42	111	108	0.1
B-4	0.01	405	0.42	111	108	0.1
B-5	0.01	405	0.42	112	107	0.1
B-6	0.015	407	0.64	112	109	0.122474
B-7	0.02	405	0.85	113	109	0.141421
B-8	0.025	399	1.06	113	109	0.158114
C-1	0.015	364	0.64	111	109	0.122474
C-2	0.025	388	1.06	113	110	0.158114
C-3	0.03	400	1.27	115	110	0.173205
C-4	0.03	405	1.27	115	110	0.173205
C-5	0.035	404	1.49	114	110	0.187083
C-6	0.04	402	1.7	114	109	0.2
C-7	0.045	397	1.91	114	109	0.212132
C-8	0.04	384	1.7	114	109	0.2
Average		388.25	0.79375	110.833333	107.3333 109.0833	0.131176



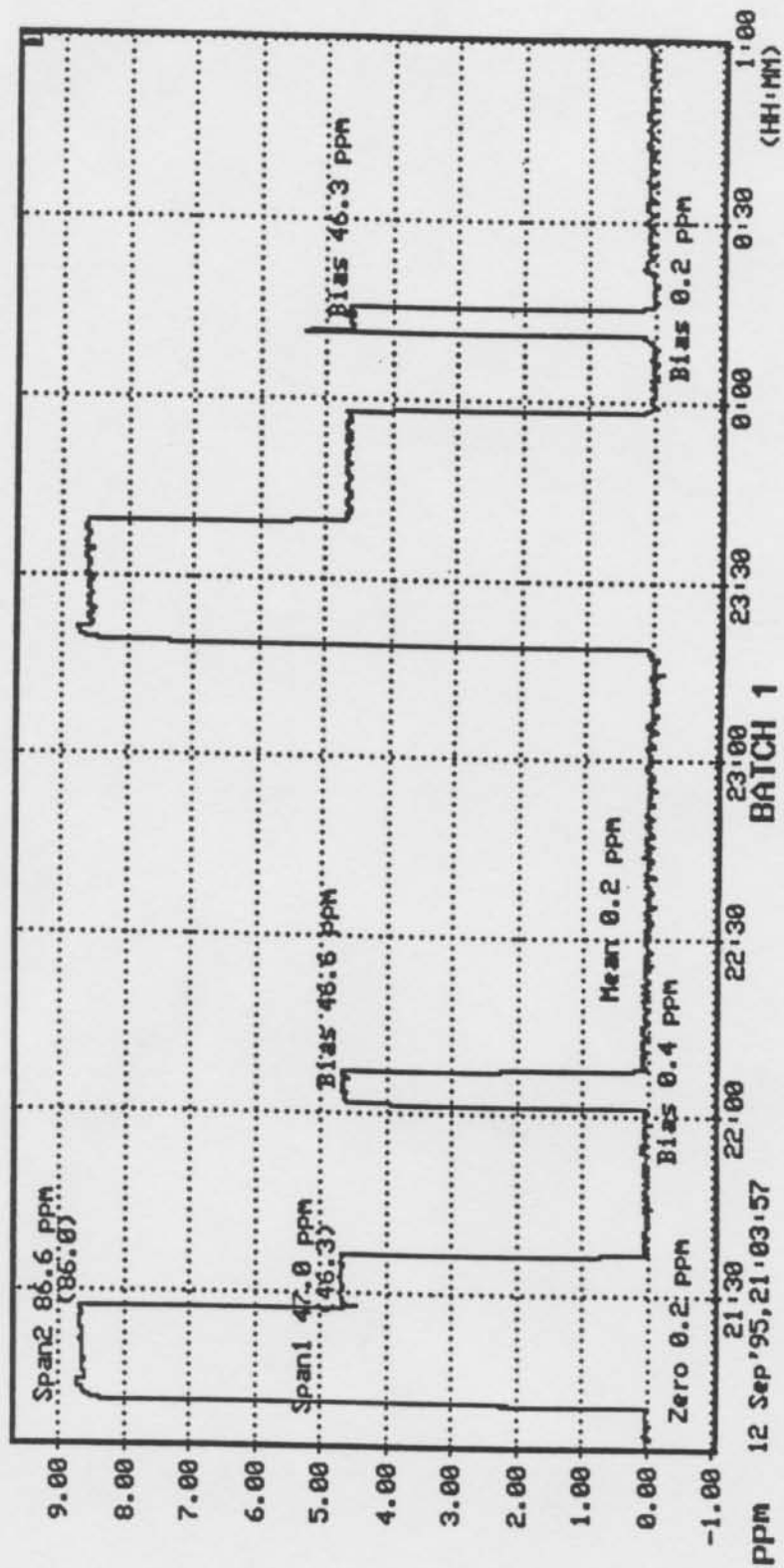
N O X



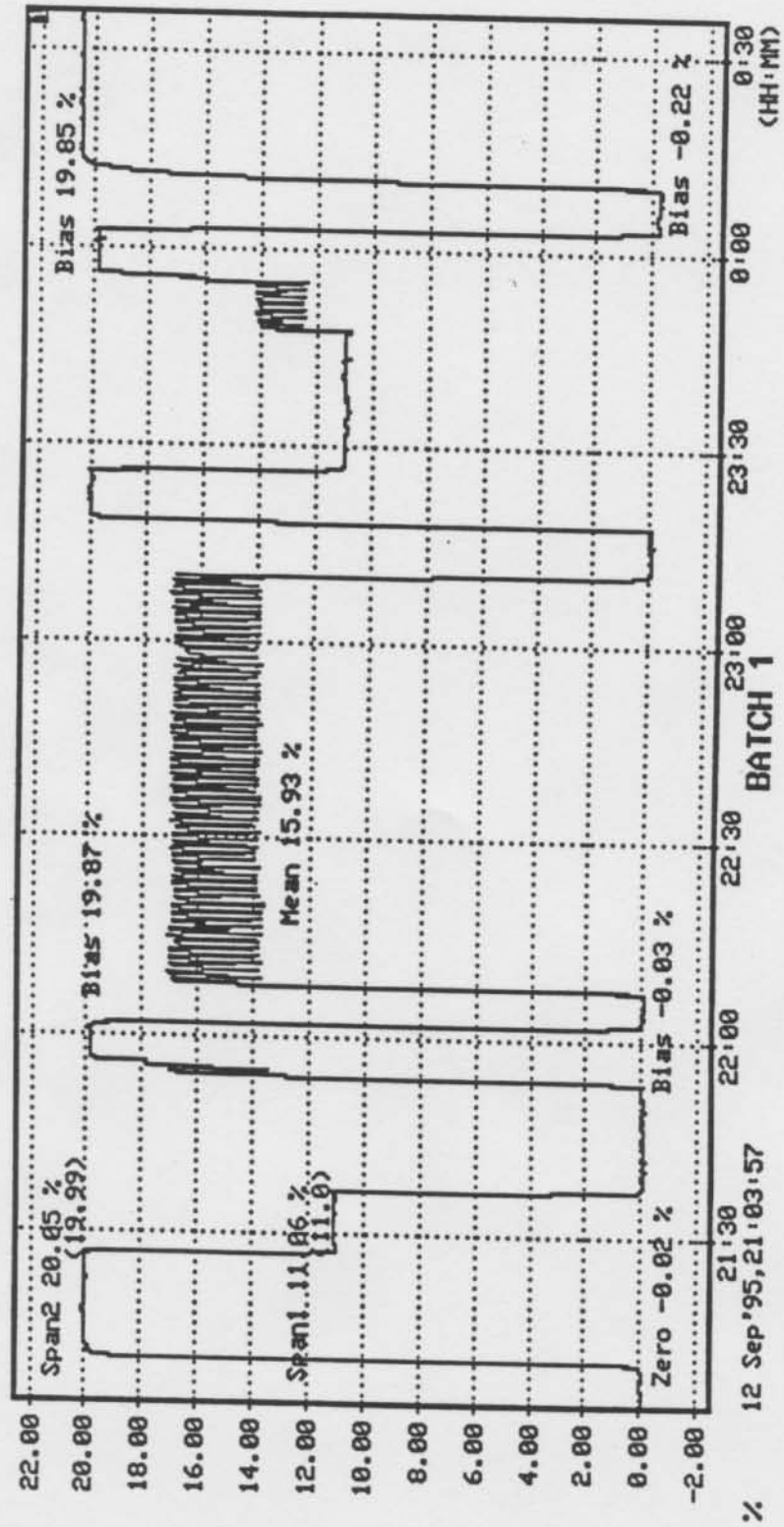


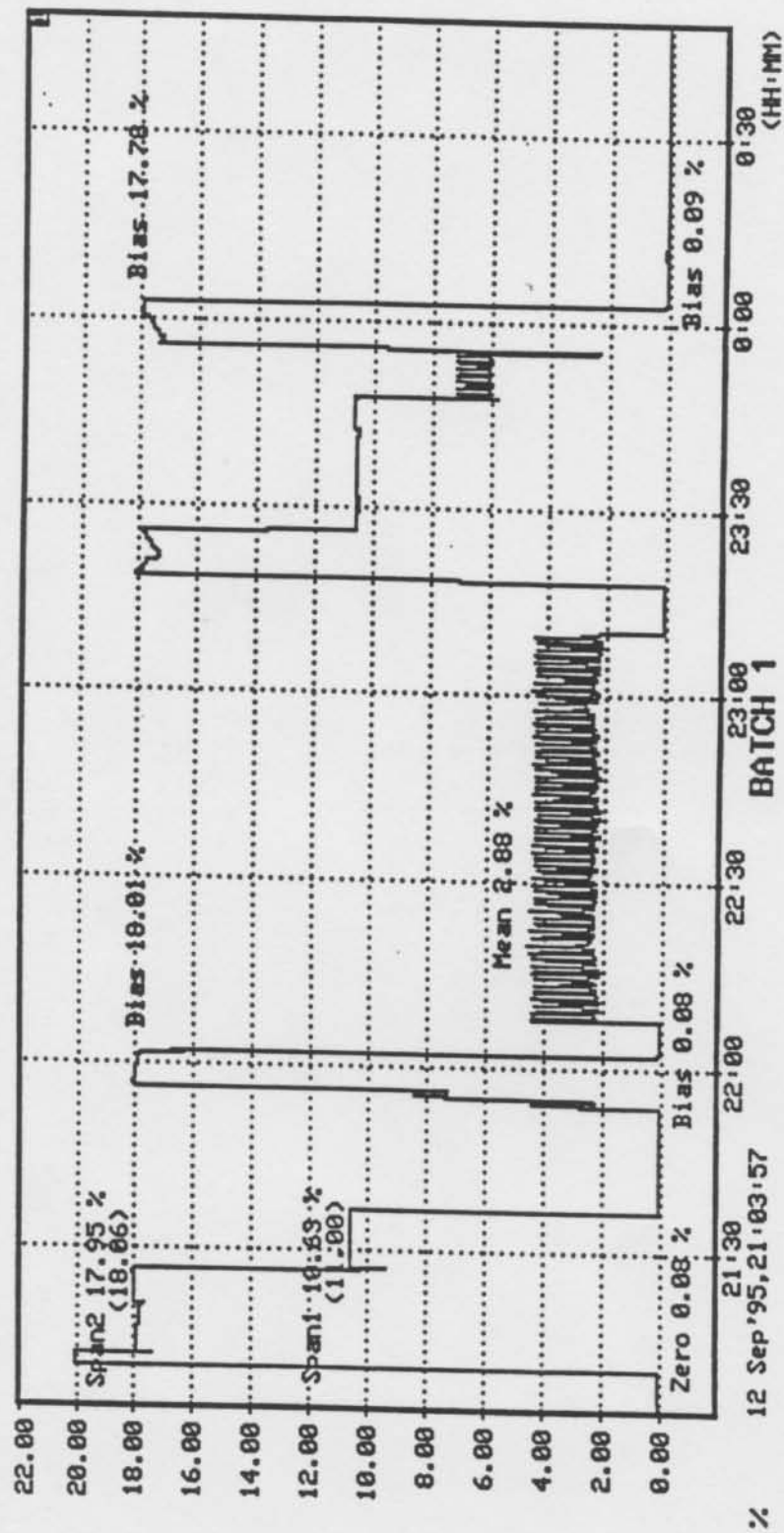
T H C

S O 2



OXYGEN





C 0 2

PES Inc.

Calculations for :

EPA Method 2,3a,4,6c,7E,10
and 25a

Plant ATC Consultants - Balboa Pacific

Project # 5102

Operation Pyrolytic Unit

Run 1

Load Batch 1

Location Santa Fe Springs, CA

Date 9/12/95

D A T A I N P U T

INPUT	Vlc =	51.5	cc	Vol. of H2O collected
INPUT	Vm =	37.431	cf	Dry gas meter reading
INPUT	Pb =	29.87	in. Hg	Barometric pressure
INPUT	Pg =	-0.02	in. H2O	Static pressure
INPUT	dP =	0.145		Avg. sq.rt delta P
INPUT	dH =	0.955	in. H2O	Avg. delta H
INPUT	Tm =	566.6	R	Avg. meter temp.
INPUT	Ts =	833.6	R	Avg. stack temp.
INPUT	Y =	1.021		Meter calibration factor
INPUT	t =	72	min.	Duration of sampling time
INPUT	A =	2.3300	sq.ft.	Stack Area
INPUT	Cp =	0.84		Pitot tube coefficient
	Kp =	85.49		Pitot tube constant
	K1 =	17.64	R/in.Hg	constant
	K2 =	0.04707	cu.ft/ml	constant
	K3 =	0.002669	in.Hg-cf/	constant

Gas Analysis			
INPUT	[O2] =	15.93	% (dry)
INPUT	[O2] =	-0.03	initial zero bias
INPUT	[O2] =	-0.22	final zero bias
	[O2] =	-0.13	average zero bias
INPUT	[O2] =	19.99	midspan concentration
INPUT	[O2] =	19.87	initial midspan bias
INPUT	[O2] =	19.85	final midspan bias
	[O2] =	19.86	average midspan bias
INPUT	[CO2] =	2.88	% (dry)
INPUT	[CO2] =	0.08	initial zero bias
INPUT	[CO2] =	0.09	final zero bias
	[CO2] =	0.09	average zero bias
INPUT	[CO2] =	18.06	midspan concentration
INPUT	[CO2] =	18.01	initial midspan bias
INPUT	[CO2] =	17.78	final midspan bias
	[CO2] =	17.90	average midspan bias
	[O2] =	16.06	adjusted concentration
	[CO2] =	2.83	adjusted concentration
	[N2] =	81.1	%
INPUT	[CO] =	63.60	ppmV (dry)
INPUT	[CO] =	0.6	initial zero bias
INPUT	[CO] =	1.6	final zero bias
	[CO] =	1.10	average zero bias
INPUT	[CO] =	75.7	midspan concentration
INPUT	[CO] =	75.7	initial midspan bias
INPUT	[CO] =	77.2	final midspan bias
	[CO] =	76.45	average midspan bias
INPUT	[NOx] =	28.4	ppmV (dry)
INPUT	[NOx] =	-0.15	initial zero bias
INPUT	[NOx] =	-0.16	final zero bias
	[NOx] =	-0.16	average zero bias
INPUT	[NOx] =	44.21	midspan concentration
INPUT	[NOx] =	44.79	initial midspan bias
INPUT	[NOx] =	44.05	final midspan bias
	[NOx] =	44.42	average midspan bias
INPUT	[THC] =	8.0	ppmV (wet)
INPUT	[THC] =	0.44	initial zero bias
INPUT	[THC] =	0.73	final zero bias
	[THC] =	0.59	average zero bias
INPUT	[THC] =	48	midspan concentration
INPUT	[THC] =	47.39	initial midspan bias
INPUT	[THC] =	46.44	final midspan bias
	[THC] =	46.915	average midspan bias
INPUT	[SO2] =	0.2	ppmV (dry)
INPUT	[SO2] =	0.4	initial zero bias
INPUT	[SO2] =	0.2	final zero bias
	[SO2] =	0.30	average zero bias
INPUT	[SO2] =	46.3	midspan concentration
INPUT	[SO2] =	46.6	initial midspan bias
INPUT	[SO2] =	46.3	final midspan bias
	[SO2] =	46.45	average midspan bias
	[CO] =	62.79	ppmV (dry) adj concentration
	[NOx] =	28.29	ppmV (dry) adj concentration
	[THC] =	7.63	ppmV (wet) adj concentration
	[SO2] =	-0.10	ppmV (dry) adj concentration

CALCULATIONS

01) Volume of gas sampled at standard conditions, Vmstd

$$Vmstd = K1 * Y * Vm * (Pb + dH/13.6) / Tm$$

$$Vmstd = \begin{array}{ll} 35.62 & \text{cu.ft} \\ 1.01 & \text{cu.m} \end{array}$$

02) Volume of water vapor collected at standard conditions.

$$Vw(std) = K2 * Vlc$$

$$Vw(std) = 2.42 \text{ scf}$$

03) Decimal fraction of moisture by volume in stack gas

$$Bws = Vwstd / (Vmstd + Vwstd)$$

$$Bws = 0.064$$

04) Molecular weight of the stack gas on a wet basis

$$Ms = (1-Q) * ((44 * \%CO2) + (28 * \%CO) + (32 * \%O2) + (28 * \%N2)) + (18 * Q)$$

$$Ms = 28.37$$

05) Average stack gas velocity.

$$Ps = 29.87 \text{ in. Hg}$$

$$vs = Kp * Cp * (dP^{0.5}) * (Ts / (Ps * Md))^{.5}$$

$$vs = 10.31 \text{ ft/sec}$$

06) Average actual stack gas volumetric flowrate.

$$Q = 60 * vs * As$$

$$Q = \begin{array}{ll} 1441.26 & \text{cfm} \\ 40.82 & \text{cmm} \end{array}$$

07) Average stack gas dry volumetric flowrate.

$$Qstd = Q * (Tstd / Ts) * (Ps / Pstd) * (1 - Bws)$$

$$Qstd = \begin{array}{ll} 853.23 & \text{dscfm} \\ 24.16 & \text{dscmm} \\ 51193.61 & \text{dscfh} \end{array}$$

08) Emission Calculation - Carbon Monoxide

$$\text{lbs CO/hr} = ([\text{CO}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[CO] =	62.79	ppmv (dry)	Actual conc.
[CO] =	0.23	Lbs/hr	

09) Emission Calculation - Nitrogen Oxides

$$\text{lbs NOx/hr} = ([\text{NOx}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[NOx] =	28.3	ppmv (dry)	Actual Conc.
[NOx] =	0.17	Lbs/hr	

10) Emission Calculation - Total Hydrocarbons

$$\text{lbs THC/hr} = ([\text{THC}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[THC] =	8.1	ppmv (dry)	Actual Conc.
[THC] =	0.05	Lbs/hr	

11) Emission Calculation - Sulfur Dioxide

$$\text{lbs NMHC/hr} = ([\text{NMHC}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[SO2] =	-0.1	ppmv (dry)	Actual Conc.
[SO2] =	0.07	Lbs/hr	

FIELD DATA

Plant Bortz ATC - Bed. Pce.
 Date 7-13-85
 Sampling Location Stack 2 WHB Exhaust
 Sample Type Stack Gas - SCA - S
 Run Number ATC-4
 Operator S-LAPIN
 Ambient Temperature 90
 Barometric Pressure 29.85
 Static Pressure -0.02
 Filter Number(s) _____
 Pretest Leak Rate 0.005 CFM @ 5 in. Hg
 Read And Record All Data Every 3 Minutes

Schematic of
Traverse Point Layout

6

Post test Leak Rate 0.005 CFM @ 5 in. Hg
 Impinger Box No. 5B Blank Box No. _____

7

4

Traverse Point Number	Sampling Time (minutes)	Clock Time (24 hr clock)	Gas Meter Reading Vm (cubic feet)	Velocity Head Ps (in. H2O)	Orifice Pressure Differential (in. H2O) ΔH		Stack Temp. Ts (F)	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
					Desired	Actual		Inlet Tm in (F)	Outlet Tm out (F)				
1	0	14:30	003.160	0.02	0.56	✓	343	107	105	2.0	240	260	48
2	3	14:33	004.7	0.02	0.56	✓	375	108	105	2.0	242	254	50
3	6	14:36	006.4	0.025	1.07	✓	391	109	106	2.5	243	256	50
4	9	14:39	007.4	0.02	0.56	✓	397	110	106	2.5	244	251	50
5	12	14:42	009.6	0.02	0.56	✓	402	111	106	2.5	245	250	51
6	15	14:45	011.1	0.02	0.56	✓	400	111	107	2.5	245	251	51
7	18	14:48	012.5	0.015	0.54	✓	393	112	107	2.0	245	255	52
8	21	14:51	014.0	0.01	0.43	✓	384	112	107	1.5	247	256	52
9	24	14:54	015.3	0.01	0.43	✓	385	111	107	1.5	242	239	49
10	27	15:03	016.1	0.01	0.43	✓	369	111	107	1.5	244	240	50
11	30	15:06	017.6	0.015	0.64	✓	381	111	107	2.0	244	250	50
12	33	15:09	018.9	0.015	0.64	✓	391	112	108	2.0	245	252	51
13	36	15:12	020.2	0.02	0.86	✓	395	112	108	2.5	245	255	52
14	39	15:15	021.7	0.025	0.86	✓	397	113	109	3.0	243	260	52
15	42	15:18	022.4	0.025	1.07	✓	397	113	109	3.0	245	257	52
16	45	15:21	025.1	0.015	0.64	✓	395	113	108	3.0	245	257	52
17	48	15:24	026.7	0.015	0.86	✓	397	109	107	2.0	240	242	50
18	51	15:27	028.1	0.020	0.86	✓	389	110	107	2.5	241	249	51
19	54	15:30	029.1	0.025	1.07	✓	390	111	107	3.0	240	254	52
20	57	15:33	031.6	0.030	1.28	✓	395	112	108	3.0	245	249	52
21	60	15:36	033.2	0.045	1.93	✓	395	113	108	4.0	243	247	53
22	63	15:39	035.1	0.050	2.14	✓	395	113	108	4.5	243	255	53
23	66	15:42	038.0	0.050	2.14	✓	395	114	108	4.5	243	255	53
24	69	15:45	040.0	0.040	1.71	✓	389	114	109	4.0	245	260	54
25	72	15:48	042.132	—	—	—	—	—	—	—	—	—	—

0.72 $V_m = 38.972 \sqrt{\Delta P} = 0.419$ $\Delta H = 1.01$ $T_s = 392.460$ $T_m = 109 + 460 = 551.4$

SAMPLE RETRIEVAL DATA

Plant: ATC
 Date: 9.13.95
 Sampling Location: _____
 Sampling Type (Method): EPN 5
 Run Number: ATC-4
 Sample Box Number: 583
 Clean-up Man: NN
 Job Number: _____
 Comments: sample 1- 6674
T 128.5

Filter

Filter Number: _____
 Description of Filter: _____

Moisture

Impingers:			
Final Volume:	<u>663.4</u> mL	<u>595.1</u> mL	<u>494.5</u> mL
Initial Volume:	<u>648.9</u> mL	<u>589.7</u> mL	<u>491.4</u> mL
Net Volume:	<u>14.5</u> mL	<u>5.4</u> mL	<u>3.1</u> mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	<u>777.7 681.5</u> g	_____ g	_____ g
Initial Volume:	<u>660.2</u> g	_____ g	_____ g
Net Volume:	<u>21.6</u> g	_____ g	_____ g
Total Moisture:	_____ g	_____ g	_____ g

44.6

Description of Impinger catch: _____

PES Inc.

EPA Methods 5 Calculations

Plant ATC - Balboa Pacific

Project # 5102

Operation Pyrolytic Waste Incinerator

Run 2 - Particulate

Location Santa Fe Springs, CA

Date 9/13/95

Emission Data

Vlc =	44.6	cc	Vol. of H2O collected (impingers)
Vm =	38.972	cf	Dry gas meter reading
Pb =	29.85	in. Hg	Barometric pressure
Ps =	29.85	in. Hg	Stack pressure
dP =	0.149		Average sq.rt delta P
dH =	1.010	in. H2O	Average draft gauge reading
Tm =	569.3	R	Average meter temperature
Ts =	837.90	R	Average stack temperature
Dn =	0.499	in.	Nozzle diameter
Y =	1.021		Meter calibration factor
t =	72	min.	Duration of sampling time
A =	2.3300	sq.ft.	Cross sectional area of stack
Cp =	0.84		Pitot tube coefficient
Kp =	85.49		Pitot tube constant
K1 =	17.64	R/in.Hg	constant
K2 =	0.04707	cu.ft/ml	constant
K3 =	0.002669	in.Hg-cf/ml-R	constant

1) Volume of gas sampled at standard conditions, Vmstd
 $Vmstd = K1 * Y * Vm * (Pb + dH/13.6) / Tm$

Vmstd = 36.89 cu.ft
1.04 cu.m

2) Volume of water vapor collected at standard conditions.

$Vw(std) = K2 * Vlc$

Vw(std) = 2.10 scf

3) Decimal fraction of moisture by volume in stack gas

$$Bws = Vwstd / (Vmstd + Vwstd)$$

$$Bws = 0.054$$

4) Molecular weight of the stack gas on a dry basis M_d .

$$Ms = ((44 * \%CO_2) + (28 * \%CO) + (32 * \%O_2) + (28 * \%N_2))$$

$$Ms = 29.08$$

Instrumental gas analysis

% CO ₂	2.68
% CO	0
% O ₂	16.39
% N ₂	80.93

5) Average stack gas velocity.

$$vs = Kp * Cp * (dP^{0.5}) * (Ts / Ps * Md)^{.5}$$

$$vs = 10.51 \text{ ft/sec}$$

6) Average actual stack gas volumetric flowrate.

$$Q = 60 * vs * As$$

$$Q = 1469.58 \text{ cfm}$$

$$41.62 \text{ cmn}$$

7) Average stack gas dry volumetric flowrate.

$$Qstd = Q * (Tstd / Ts) * (Ps / Pstd)$$

$$Qstd = 874.10 \text{ dscfm}$$

$$24.75 \text{ dscmn}$$

8) Analytical data

a) Front half acetone wash

0.0032 g wash net wt
0 g acetone blank net wt
100 ml blank vol.
152 ml Final wash volume
152 ml aliquot

0.0032 g soluble particulate*

b) Front half glass microfibre filter

0.02 g filter net wt

c) Back half water wash - soluble

0.0035 g net wt
0 g water blank net wt
220 ml blank vol
550 ml Final wash volume
550 ml aliquot

0.0035 g soluble net wt*

* Weights are not blank corrected

9) Particulate concentrations

0.0097 grains/dscf Front 1/2
0.0112 grains/dscf Total

11) Particulate emission rate

Conc. * (1 lb/7000 gr) * Qstd * 60 min/hr

W = 0.073 lbs/hr Front 1/2
W = 0.084 lbs/hr Total Particulate

12) Isokinecity

An = 0.001 ft² Area of nozzle orifice

$\% I = 100 \cdot Ts \cdot ((K3 \cdot V1c + (Vm \cdot Y / Tm) (Pb + dH / 13.6)) / (60 \cdot t \cdot Ps \cdot vs \cdot An))$

$\% I = 100.62$

FIELD DATA

Plant ATC - Blue Pine
 Date 9.13.95
 Sampling Location WHB Exhaust
 Sample Type CPA-12
 Run Number ATC-3
 Operator 202 Ad/K
 Ambient Temperature 90
 Barometric Pressure 29.95
 Static Pressure -0.02
 Filter Number(s) -

Pretest Leak Rate 0.614 CFM @ 5 in. Hg
 Read And Record All Data Every 5 Minutes

Schematic of
Traverse Point Layout

Probe Length and Type 3' Glass
 Pitot Tube I.D. No. 5.2A
 Nozzle I.D. No. And Diameter 1/16-6 0.495
 Assumed Moisture, % 6.0
 Meter Box Number 1A
 Meter Delta H@ 1.881
 C Factor -
 Meter Gamma 1.021
 Heater Box Setting 250
 Reference Delta P -
 Post test Leak Rate 0.014 CFM @ 5.0 in. Hg
 Impinger Box No. 3/3 Blank Box No. 3

Traverse Point Number	Sampling Time (minutes)	Clock Time (24 hr clock)	Gas Meter Reading Vm (cubic feet)	Velocity Head Ps (in. H2O)	Orifice Pressure Differential (in. H2O) ΔH		Stack Temp. Ts (F)	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
					Desired	Actual		Inlet Tm in (F)	Outlet Tm out (F)				
1	0	11:25	945.335	0.010	0.42	✓	279	103	103	1.5	249	247	55
2	5	11:30	947.2	0.010	0.42	✓	379	103	103	1.5	250	247	55
3	10	11:35	949.0	0.010	0.42	✓	395	106	104	1.5	251	252	56
4	15	11:40	950.9	0.010	0.42	✓	403	108	105	1.5	252	252	56
5	20	11:45	952.7	0.010	0.42	✓	403	109	105	1.5	249	253	57
6	25	11:50	954.7	0.010	0.42	✓	401	109	105	1.5	252	252	57
7	30	11:55	956.4	0.010	0.42	✓	401	109	106	1.5	254	253	57
8	35	12:00	958.4	0.010	0.42	✓	398	110	106	1.5	257	257	58
1	40	12:05/12:10	960.0	0.010	0.42	✓	360	108	106	1.5	254	254	49
2	45	12:15	962.0	0.010	0.42	✓	395	109	107	1.5	253	246	49
3	50	12:20	963.7	0.010	0.42	✓	405	111	108	1.5	253	289	49
4	55	12:25	965.6	0.010	0.42	✓	405	111	108	1.5	253	280	50
5	60	12:30	967.5	0.010	0.42	✓	405	112	107	1.5	255	289	51
6	65	12:35	969.3	0.015	0.64	✓	407	112	109	1.5	258	252	52
7	70	12:40	971.4	0.020	0.85	✓	405	113	109	2.0	253	260	53
8	75	12:45	973.9	0.025	1.06	✓	399	113	109	3.5	248	250	54
1	80	12:50/12:55	977.2	0.015	0.64	✓	384	111	107	2.0	248	248	54
2	85	13:00	979.5	0.025	1.06	✓	384	113	110	3.5	251	250	54
3	90	13:05	982.7	0.030	1.27	✓	409	115	110	3.5	249	255	56
4	95	13:10	985.7	0.035	1.49	✓	405	115	110	3.5	249	255	57
5	100	13:15	988.8	0.040	1.70	✓	402	114	109	4.0	254	248	57
6	105	13:20	992.6	0.045	1.91	✓	377	114	109	4.5	254	255	60
7	110	13:25	995.5	0.045	1.91	✓	387	114	109	4.0	252	253	60
8	115	13:30	999.3	0.040	1.70	✓	387	114	109	4.0	252	253	60
1	120	13:35	002.708	-	-	-	-	-	-	-	-	-	-

$$T_m = 109 + 460$$

$$T_6 = 988 + 460$$

$$V_m = 57.373 \text{ } \bar{V}_p = 0.131$$

$$Q = 120$$

$$\Delta H = 0.794$$

SAMPLE RETRIEVAL DATA

Plant: ATC
 Date: 9.12.81
 Sampling Location: _____
 Sampling Type (Method): EPH 12
 Run Number: ATC-3
 Sample Box Number: F3B
 Clean-up Man: NN
 Job Number: _____
 Comments: Wash/Catch F 8699
 T 350.7

Filter

Filter Number: _____
 Description of Filter: _____

Moisture

Impingers:			
Final Volume:	<u>707.1</u> mL	<u>627.5</u> mL	<u>479.4</u> mL
Initial Volume:	<u>652.4</u> mL	<u>623.2</u> mL	<u>474.5</u> mL
Net Volume:	<u>56.7</u> mL	<u>4.3</u> mL	<u>0.9</u> mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	<u>691.5</u> g	_____ g	_____ g
Initial Volume:	<u>674.0</u> g	_____ g	_____ g
Net Volume:	<u>17.5</u> g	_____ g	_____ g
Total Moisture:	_____ g	_____ g	_____ g

79.4

Description of Impinger catch: _____

PES, Inc.
Multi-Metals Method Calculations (EPA 12)

Plant ATC-Balboa Pacific
Project # 5102
Operation Pyrolytic Oxidation Unit
Run Batch 2
Location Outlet
Date 9/14/95

Test Data

Vlc =	99.7 cc	Vol. of H2O collected (impingers)
Vm =	74.572 cf	Dry gas meter reading
Pb =	29.88 in. Hg	Barometric pressure
Ps =	29.88 in. Hg	Stack pressure
dP =	0.174	Average sq.rt delta P
dH =	1.286 in. H2O	Average draft gauge reading
Tm =	568.8 R	Average meter temperature
Ts =	853.50 R	Average stack temperature
Dn =	0.495 in.	Nozzle diameter
Y =	1.021	Meter calibration factor
t =	120 min.	Duration of sampling time
A =	2.3300 sq.ft.	Cross sectional area of stack
Cp =	0.84	Pitot tube coefficient
Kp =	85.49	Pitot tube constant
K1 =	17.64 R/in.Hg	constant
K2 =	0.04707 cu.ft/ml	constant
K3 =	0.002669 in.Hg-cf/ml-R	constant

Instrumentation Data

[O2] = 16.4 %
[CO2] = 2.7 %

CALCULATIONS

1) Volume of gas sampled at standard conditions, Vmstd

$$Vmstd = K1 \cdot Y \cdot Vm \cdot (Pb + dH/13.6)/Tm$$

Vmstd = 70.78 cu.ft
2.00 cu.m

2) Volume of water vapor collected at standard conditions.
 $V_w(\text{std}) = K_2 \cdot V_{lc}$

$V_w(\text{std}) =$ 4.69 scf

3) Decimal fraction of moisture by volume in stack gas
 $B_{ws} = V_{wstd}/(V_{mstd} + V_{wstd})$

$B_{ws} =$ 0.062

4) Molecular weight of the stack gas on a dry basis M_d .

$M_d = (1 - B_{ws}) \cdot ((44\% \text{CO}_2) + (28\% \text{CO}) + (32\% \text{O}_2) + (28\% \text{N}_2)) + (18 \cdot B_{ws})$

$M_d =$ 28.40

5) Average stack gas velocity.

$v_s = K_p \cdot C_p \cdot (dP^{0.5}) \cdot (T_s/P_s \cdot M_d)^{0.5}$

$v_s =$ 12.54 ft/sec

6) Average actual stack gas volumetric flowrate.

$Q = 60 \cdot v_s \cdot A_s$

$Q =$ 1752.47 cfm
49.63 cmm

7) Average stack gas dry volumetric flowrate.

$Q_{std} = Q \cdot (T_{std}/T_s) \cdot (P_s/P_{std})$

$Q_{std} =$ 1015.31 dscfm
28.75 dscmm

8) Toxic metal concentrations and emission rates

Element	Sample Mass (ug)	Blank Mass (ug) DL	Conc. (mg/dscm)	Emission Rate (mg/hr)
Copper	13.00	1.00	4.52E-04	7.8E-01
Chromium	11.00	2.00	3.83E-04	6.6E-01
Lead	7.00	0.20	2.43E-04	4.2E-01
Zinc	48.00	8.00	1.67E-03	2.9E+00
Manganese	4.00	1.00	1.39E-04	2.4E-01
Nickel	4.70	0.40	1.63E-04	2.8E-01
Cadmium	5.00	2.00	1.74E-04	3.0E-01
Beryllium	1	1.00	3.48E-05	6.0E-02
Arsenic	2.9	0.20	1.01E-04	1.7E-01
Selenium	7	7.00	2.43E-04	4.2E-01
Molybdenum	2500	3.00	8.69E-02	1.5E+02
Silver	0.1	0.10	3.48E-06	6.0E-03
Antimony	3	3.00	1.04E-04	1.8E-01
Barium	33	0.40	1.15E-03	2.0E+00
Thallium	0.1	0.10	3.48E-06	6.0E-03

9) Isokineticity

An = 0.001 ft² Area of nozzle orifice

$$\% I = 100 \cdot T_s \cdot ((K_3 \cdot V_{lc} + (V_m \cdot Y / T_m) \cdot (P_b + dH / 13.6)) / (60 \cdot t \cdot P_s \cdot v_s \cdot A_n))$$

% I = 101.34

Sample Train Operation Data

Test Date 9/14/95

Barometer 29.88 in.Hg

Run # 2

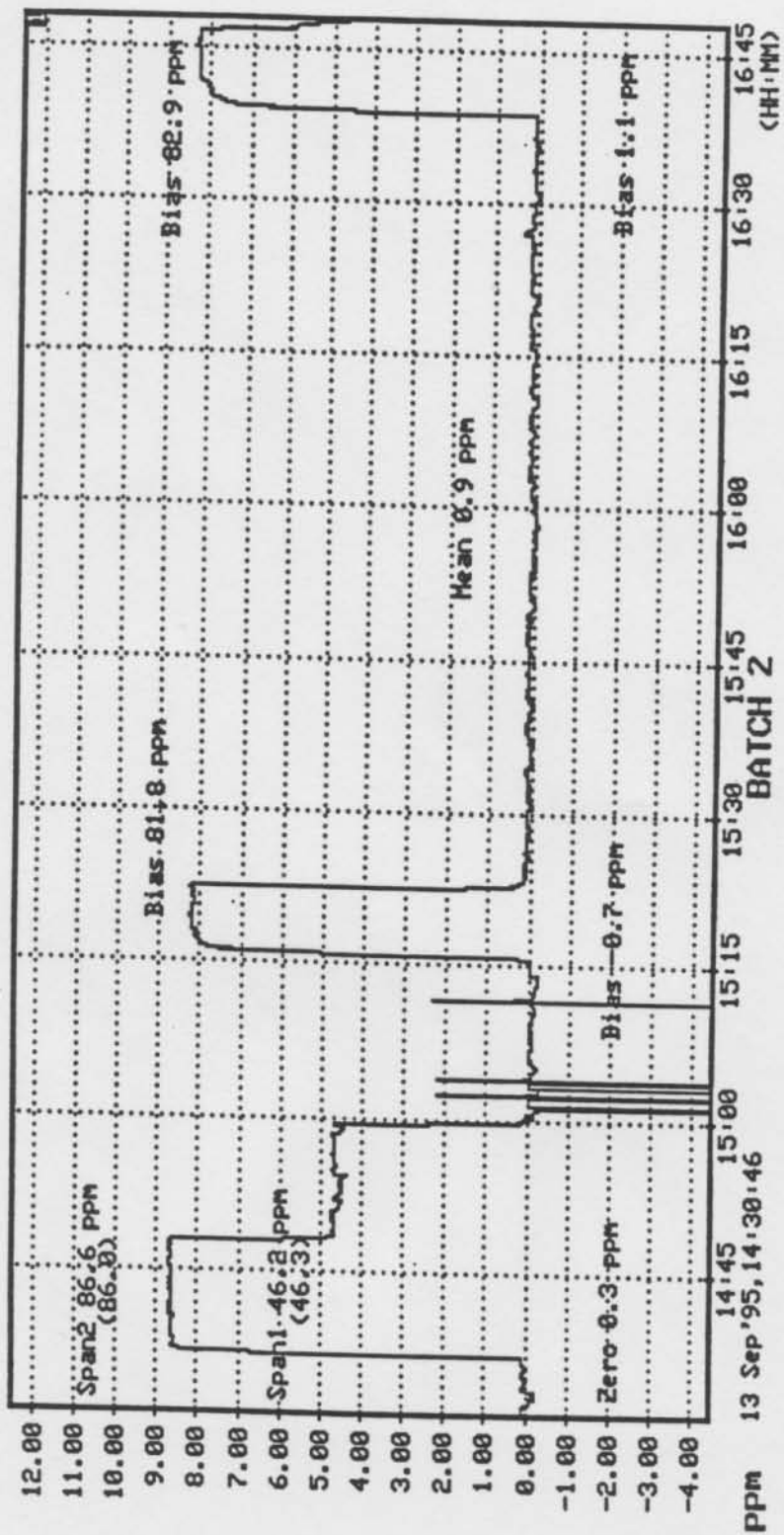
Static P -0.02 in.H2O

Pitot Cp 0.84

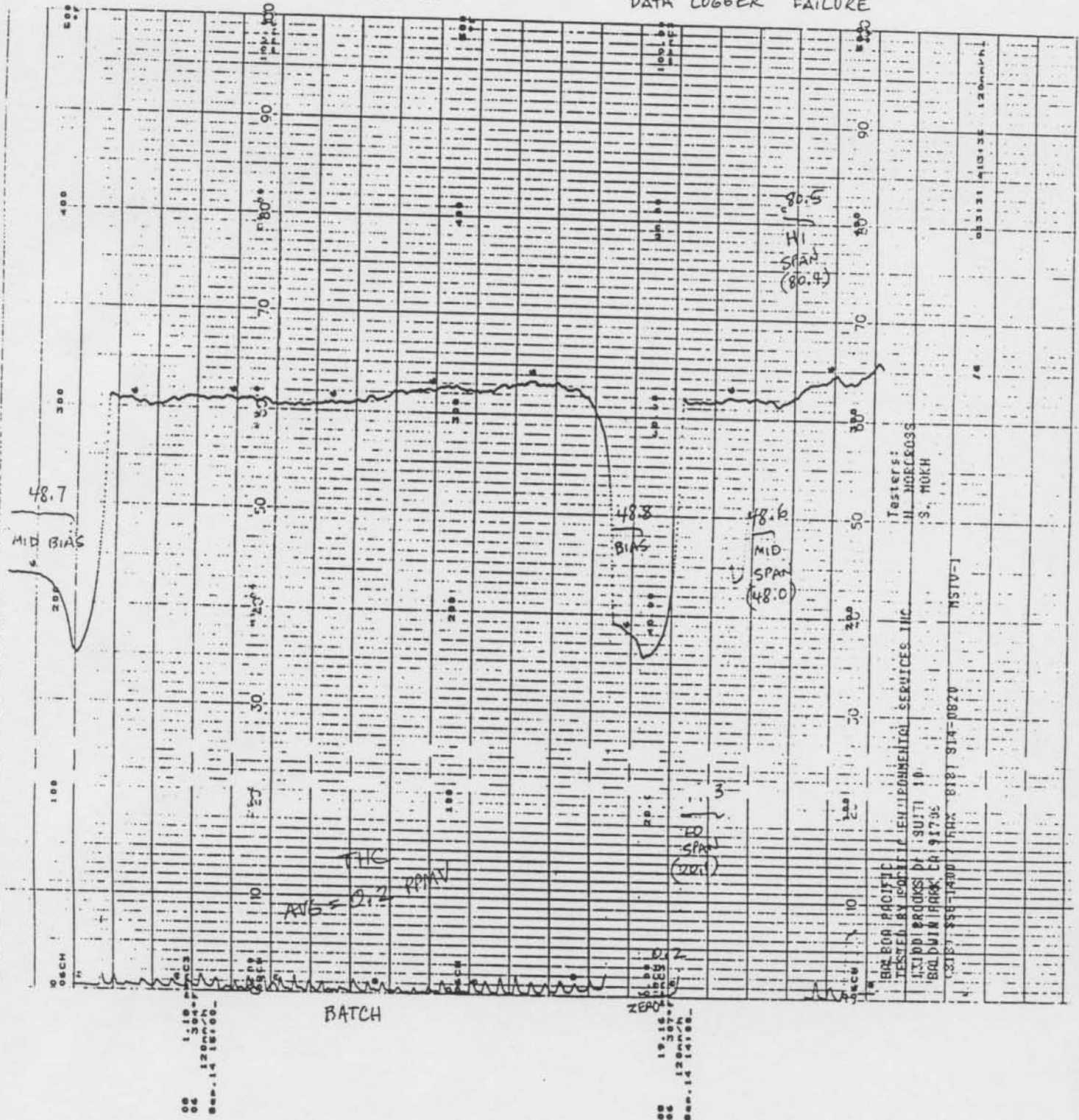
Nozzle 0.495

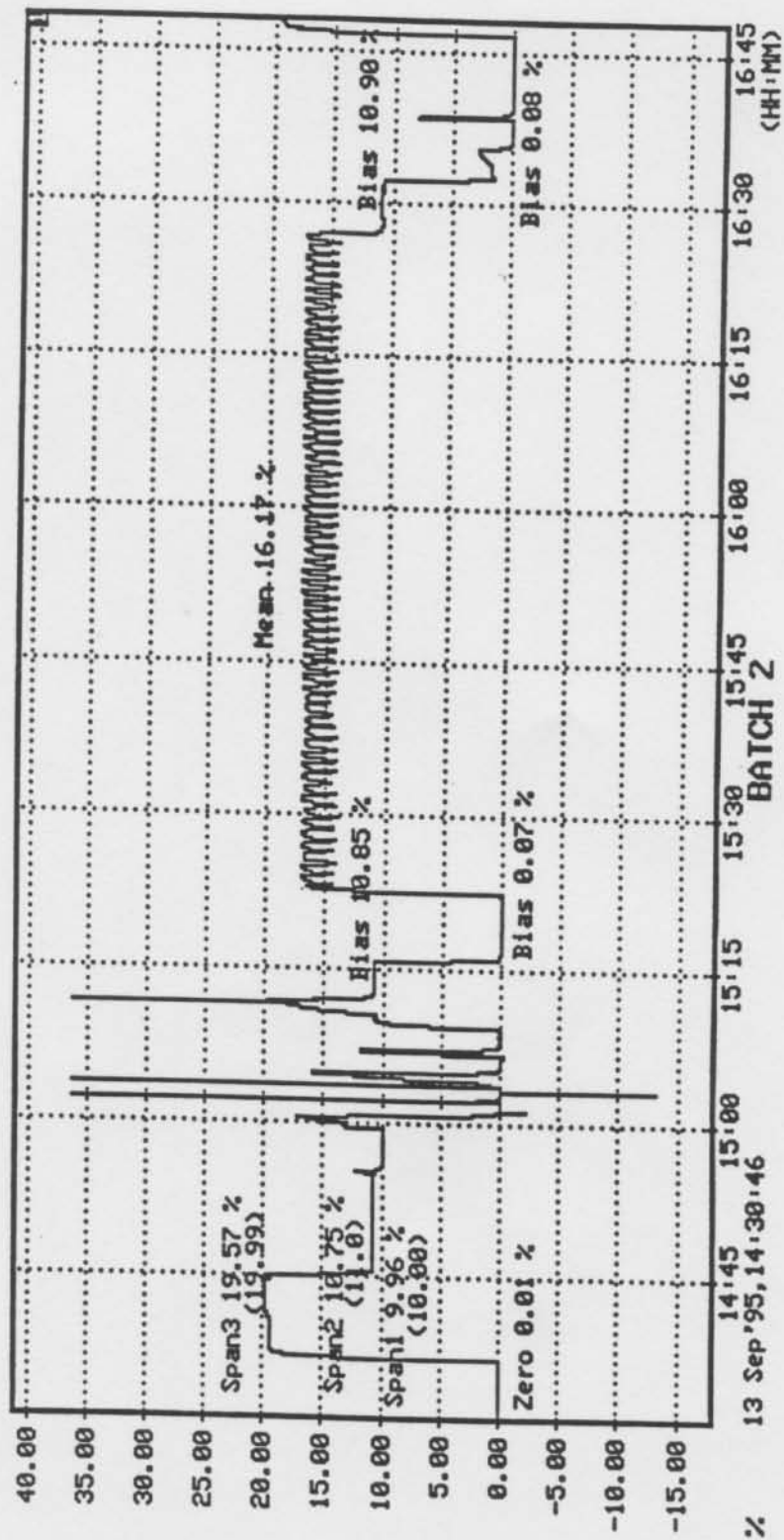
Traverse Point	Delta-P (in. H2O)	Temp. (Deg.F)	delta H	Dry Gas Meter IN	Temp OUT	(dP) ^{.5}
A-1	0.03	397	1.24	101	101	0.173205
A-2	0.03	400	1.24	102	101	0.173205
A-3	0.04	401	1.66	104	101	0.2
A-4	0.035	402	1.45	106	102	0.187083
A-5	0.04	398	1.66	109	104	0.2
A-6	0.04	402	1.66	112	105	0.2
A-7	0.03	376	1.24	111	105	0.173205
A-8	0.03	370	1.24	111	105	0.173205
B-1	0.045	395	1.87	108	105	0.212132
B-2	0.035	403	1.45	110	106	0.187083
B-3	0.04	402	1.66	111	106	0.2
B-4	0.03	403	1.24	112	106	0.173205
B-5	0.03	401	1.24	112	107	0.173205
B-6	0.03	402	1.24	114	108	0.173205
B-7	0.025	378	1.04	114	108	0.158114
B-8	0.03	370	1.24	114	109	0.173205
C-1	0.04	401	1.66	112	110	0.2
C-2	0.035	402	1.45	113	110	0.187083
C-3	0.035	403	1.45	114	109	0.187083
C-4	0.03	402	1.24	115	110	0.173205
C-5	0.025	400	1.04	115	110	0.158114
C-6	0.02	392	0.83	115	110	0.141421
C-7	0.01	373	0.41	114	110	0.1
C-8	0.01	371	0.41	113	110	0.1
Average		393.5	1.28583333	110.916667	106.5833 108.75	0.17404

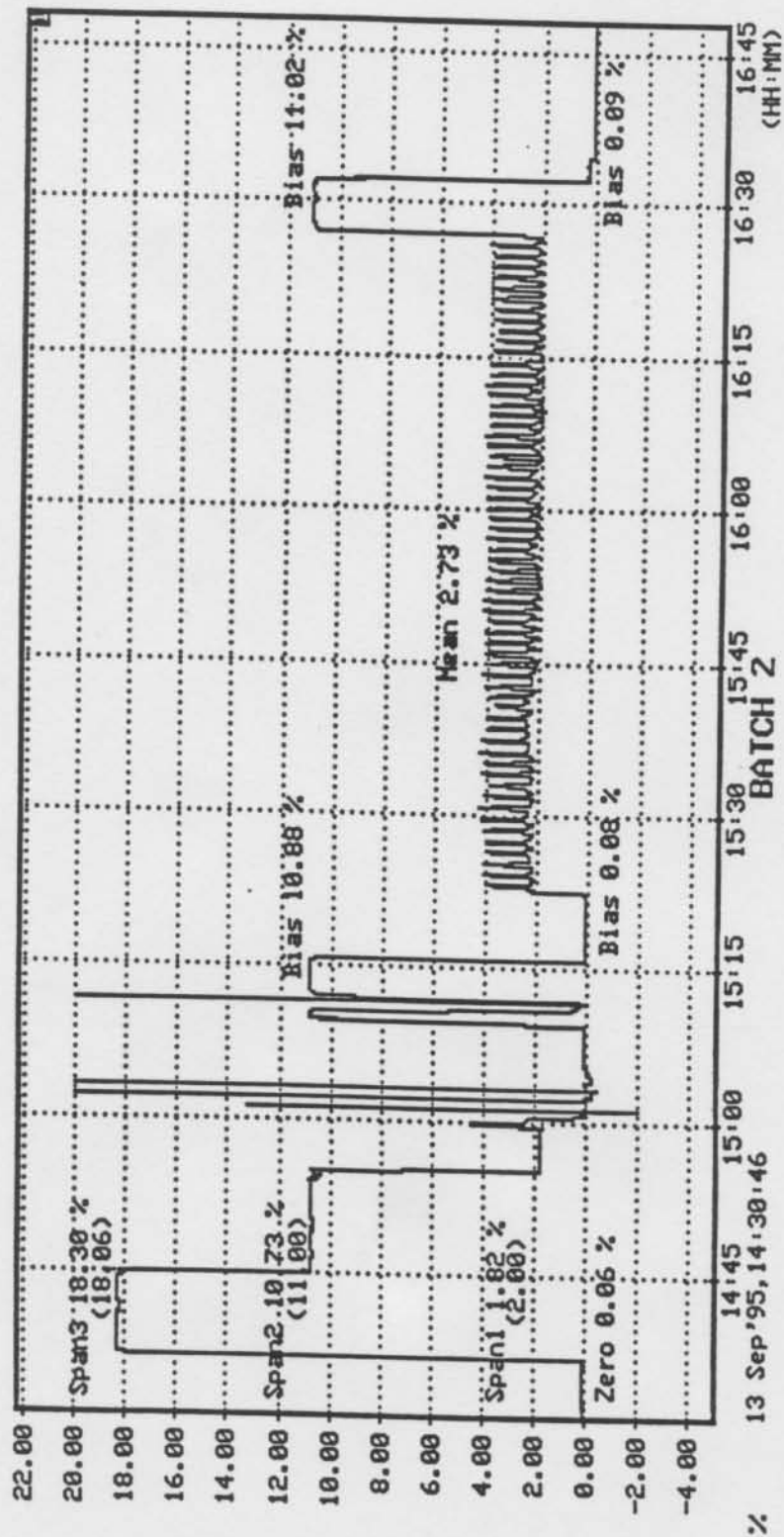
S O 2

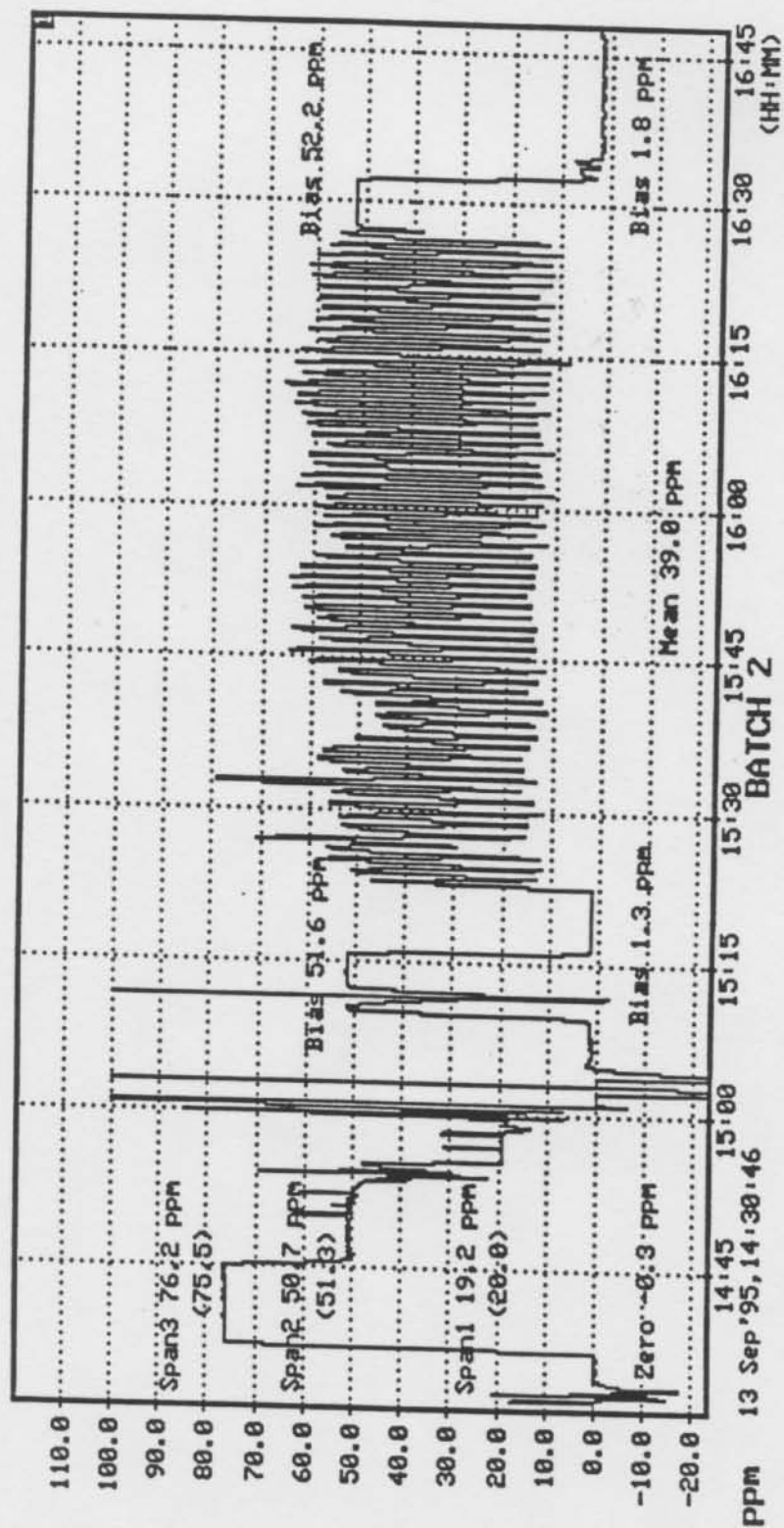


DATA LOGGER FAILURE

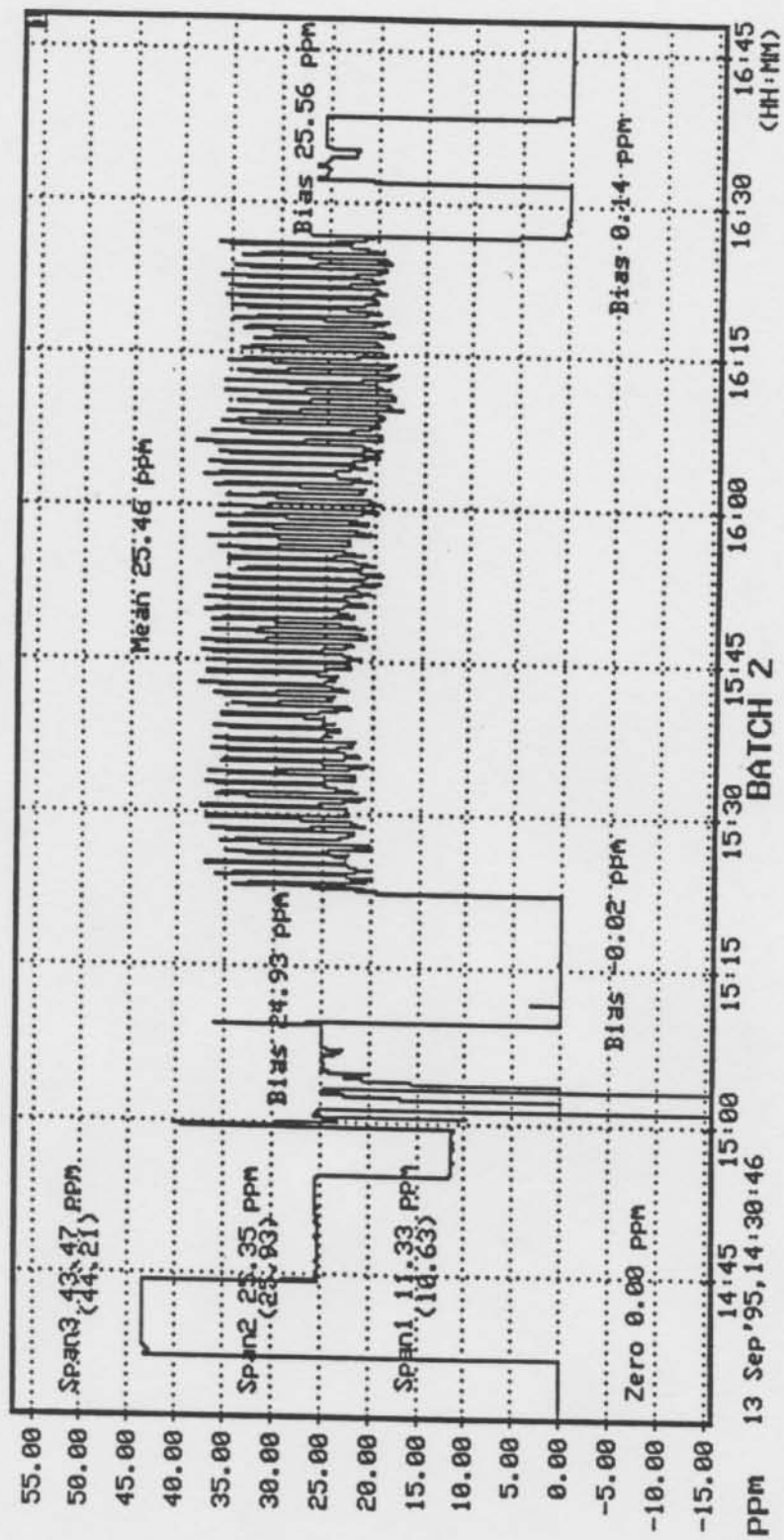








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PES Inc.
Calculations for :

EPA Method 2,3a,4,6c,7E,10
and 25a

Plant ATC Consultants - Balboa Pacific

Project # 5102

Operation Pyrolytic Unit

Run 2

Load Batch 2

Location Santa Fe Springs, CA

Date 9/13/95

D A T A I N P U T

INPUT	Vlc =	44.6	cc	Vol. of H2O collected
INPUT	Vm =	38.972	cf	Dry gas meter reading
INPUT	Pb =	29.85	in. Hg	Barometric pressure
INPUT	Pg =	-0.02	in. H2O	Static pressure
INPUT	dP =	0.149		Avg. sq.rt delta P
INPUT	dH =	1.010	in. H2O	Avg. delta H
INPUT	Tm =	569.3	R	Avg. meter temp.
INPUT	Ts =	837.9	R	Avg. stack temp.
INPUT	Y =	1.021		Meter calibration factor
INPUT	t =	72	min.	Duration of sampling time
INPUT	A =	2.3300	sq.ft.	Stack Area
INPUT	Cp =	0.84		Pitot tube coefficient
	Kp =	85.49		Pitot tube constant
	K1 =	17.64	R/in.Hg	constant
	K2 =	0.04707	cu.ft/ml	constant
	K3 =	0.002669	in.Hg-cf/	constant

Gas Analysis		
INPUT	[O2] =	16.17 % (dry)
INPUT	[O2] =	0.07 initial zero bias
INPUT	[O2] =	0.08 final zero bias
	[O2] =	0.08 average zero bias
INPUT	[O2] =	11 midspan concentration
INPUT	[O2] =	10.85 initial midspan bias
INPUT	[O2] =	10.9 final midspan bias
	[O2] =	10.875 average midspan bias
INPUT	[CO2] =	2.73 % (dry)
INPUT	[CO2] =	0.08 initial zero bias
INPUT	[CO2] =	0.09 final zero bias
	[CO2] =	0.09 average zero bias
INPUT	[CO2] =	11 midspan concentration
INPUT	[CO2] =	10.88 initial midspan bias
INPUT	[CO2] =	11.02 final midspan bias
	[CO2] =	10.95 average midspan bias
	[O2] =	16.39 adjusted concentration
	[CO2] =	2.68 adjusted concentration
	[N2] =	80.9 %
INPUT	[CO] =	39.00 ppmV (dry)
INPUT	[CO] =	1.3 initial zero bias
INPUT	[CO] =	1.8 final zero bias
	[CO] =	1.55 average zero bias
INPUT	[CO] =	51.3 midspan concentration
INPUT	[CO] =	51.6 initial midspan bias
INPUT	[CO] =	52.2 final midspan bias
	[CO] =	51.9 average midspan bias
INPUT	[NOx] =	25.5 ppmV (dry)
INPUT	[NOx] =	-0.02 initial zero bias
INPUT	[NOx] =	0.14 final zero bias
	[NOx] =	0.06 average zero bias
INPUT	[NOx] =	25.93 midspan concentration
INPUT	[NOx] =	24.93 initial midspan bias
INPUT	[NOx] =	25.56 final midspan bias
	[NOx] =	25.245 average midspan bias
INPUT	[THC] =	0.4 ppmV (wet)
INPUT	[THC] =	0.2 initial zero bias
INPUT	[THC] =	0.3 final zero bias
	[THC] =	0.25 average zero bias
INPUT	[THC] =	48 midspan concentration
INPUT	[THC] =	48.7 initial midspan bias
INPUT	[THC] =	48.7 final midspan bias
	[THC] =	48.7 average midspan bias
INPUT	[SO2] =	0.9 ppmV (dry)
INPUT	[SO2] =	-0.7 initial zero bias
INPUT	[SO2] =	1.1 final zero bias
	[SO2] =	0.20 average zero bias
INPUT	[SO2] =	86 midspan concentration
INPUT	[SO2] =	81.8 initial midspan bias
INPUT	[SO2] =	82.9 final midspan bias
	[SO2] =	82.35 average midspan bias
	[CO] =	38.16 ppmV (dry) adj concentration
	[NOx] =	26.15 ppmV (dry) adj concentration
	[THC] =	0.15 ppmV (wet) adj concentration
	[SO2] =	0.73 ppmV (dry) adj concentration

CALCULATIONS

01) Volume of gas sampled at standard conditions, V_{mstd}

$$V_{mstd} = K1 * Y * V_m * (P_b + dH/13.6) / T_m$$

$$V_{mstd} = \begin{array}{ll} 36.90 & \text{cu.ft} \\ 1.04 & \text{cu.m} \end{array}$$

02) Volume of water vapor collected at standard conditions.

$$V_w(std) = K2 * V_{lc}$$

$$V_w(std) = 2.10 \text{ scf}$$

03) Decimal fraction of moisture by volume in stack gas

$$B_{ws} = V_{wstd} / (V_{mstd} + V_{wstd})$$

$$B_{ws} = 0.054$$

04) Molecular weight of the stack gas on a wet basis

$$M_s = (1-Q) * ((44 * \%CO_2) + (28 * \%CO) + (32 * \%O_2) + (28 * \%N_2)) + (18 * Q)$$

$$M_s = 28.44$$

05) Average stack gas velocity.

$$P_s = 29.85 \text{ in. Hg}$$

$$v_s = K_p * C_p * (dP^{0.5}) * (T_s / P_s * M_d)^{.5}$$

$$v_s = 10.66 \text{ ft/sec}$$

06) Average actual stack gas volumetric flowrate.

$$Q = 60 * v_s * A_s$$

$$Q = \begin{array}{ll} 1490.38 & \text{cfm} \\ 42.21 & \text{cmm} \end{array}$$

07) Average stack gas dry volumetric flowrate.

$$Q_{std} = Q * (T_{std} / T_s) * (P_s / P_{std}) * (1 - B_{ws})$$

$$Q_{std} = \begin{array}{ll} 886.46 & \text{dscfm} \\ 25.10 & \text{dscmm} \\ 53187.44 & \text{dscfh} \end{array}$$

08) Emission Calculation - Carbon Monoxide

$$\text{lbs CO/hr} = ([\text{CO}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[CO] =	38.16	ppmv (dry)	Actual conc.
[CO] =	0.15	Lbs/hr	

09) Emission Calculation - Nitrogen Oxides

$$\text{lbs NOx/hr} = ([\text{NOx}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[NOx] =	26.2	ppmv (dry)	Actual Conc.
[NOx] =	0.17	Lbs/hr	

10) Emission Calculation - Total Hydrocarbons

$$\text{lbs THC/hr} = ([\text{THC}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[THC] =	0.2	ppmv (dry)	Actual Conc.
[THC] =	0.00	Lbs/hr	

11) Emission Calculation - Sulfur Dioxide

$$\text{lbs NMHC/hr} = ([\text{NMHC}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[SO2] =	0.7	ppmv (dry)	Actual Conc.
[SO2] =	0.00	Lbs/hr	

Plant ATC - BALBOA PACIFICDate 9-14-95

Sampling Location

Sample Type PARTICULATERun Number ATC-5Operator MOKHAmbient Temperature 102°FBarometric Pressure 29.88Static Pressure 10.005Filter Number(s) —Pretest Leak Rate 0.012 CFM @ 5.0 in. HgRead And Record All Data Every 3 MinutesProbe Length and Type 3' GlassPitot Tube I.D. No. S-2ANozzle I.D. No. And Diameter N-4 0.495Assumed Moisture, % 6.0Meter Box Number 1AMeter Delta H @ 1.861C Factor —Meter Gamma 1.021Heater Box Setting 250Reference Delta P —Post test Leak Rate 0.022 CFM @ 5.0 in. HgImpinger Box No. 5B Blank Box No. 3Schematic of
Traverse Point Layout

Traverse Point Number	Sampling Time Θ (minutes)	Clock Time (24 hr clock)	Gas Meter Reading V_m (cubic feet)	Velocity Head P_v (in. H ₂ O)	Orifice Pressure Differential (in. H ₂ O) ΔH		Stack Temp. T_s (F)	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
					Desired	Actual		Inlet T_{in} (F)	Outlet T_{out} (F)				
C8	0	14:10	117.125	0.040	1.71	✓	397	108	107	4.0	237	223	61
C7	3	14:13	119.2	0.035	1.50	✓	398	109	107	3.5	241	223	60
C6	6	14:16	121.3	0.035	1.50	✓	398	110	107	3.5	240	232	55
C5	9	14:19	123.4	0.030	1.28	✓	395	112	106	3.0	243	238	54
C4	12	14:22	125.3	0.025	1.07	✓	387	113	108	3.0	242	240	55
C3	15	14:25	127.0	0.020	0.86	✓	361	113	109	2.5	244	238	57
C2	18	14:28	128.6	0.015	0.64	✓	281	113	109	2.0	241	253	59
C1	21	14:31	129.9	0.015	0.64	✓	280	114	109	2.0	239	252	64
END LAB	24	14:34/37	131.3	0.040	1.71	✓	384	112	109	4.0	241	252	67
B7	27	14:40	133.4	0.040	1.71	✓	397	113	109	4.0	239	249	60
B6	30	14:43	135.5	0.040	1.71	✓	398	114	110	4.0	241	259	59
B5	33	14:46	137.7	0.040	1.71	✓	396	114	110	4.0	243	257	61
B4	36	14:49	139.9	0.040	1.71	✓	386	114	110	4.0	244	255	63
B3	39	14:52	142.0	0.020	0.86	✓	380	115	110	3.0	241	258	65
B2	42	14:55	143.5	0.015	0.64	✓	348	114	110	2.0	239	253	67
B1	45	14:58	145.0	0.015	0.64	✓	303	114	110	2.0	240	260	61
END LAB	48	15:01/04	146.3	0.030	1.28	✓	381	113	110	3.0	239	250	63
A7	51	15:07	148.2	0.035	1.50	✓	397	114	110	4.0	242	246	65
A6	54	15:10	150.1	0.040	1.71	✓	401	114	110	4.0	244	251	66
A5	57	15:13	152.2	0.035	1.50	✓	394	115	111	4.0	244	252	66
A4	60	15:16	154.3	0.040	1.71	✓	392	116	111	4.0	243	251	67
A3	63	15:19	156.4	0.030	1.28	✓	340	117	111	4.0	245	252	68
A2	66	15:22	158.5	0.030	1.28	✓	340	116	111	4.0	242	252	69
A1	69	15:25	160.4	0.030	1.28	✓	327	118	113	4.0	237	251	66
END	72	15:28	162.445	—	—	—	—	—	—	—	—	—	—

SAMPLE RETRIEVAL DATA

Plant: ATC
 Date: 9.14.96
 Sampling Location: _____
 Sampling Type (Method): EPA 5
 Run Number: ATC-5
 Sample Box Number: 5B
 Clean-up Man: VJ
 Job Number: _____
 Comments: sample F 707.5
 T 127.6

Filter

Filter Number: _____
 Description of Filter: _____

Moisture

Impingers:			
Final Volume:	<u>695.2</u> mL	<u>601.3</u> mL	<u>492.0</u> mL
Initial Volume:	<u>653.9</u> mL	<u>595.2</u> mL	<u>490.7</u> mL
Net Volume:	<u>41.3</u> mL	<u>6.1</u> mL	<u>1.8</u> mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	<u>729.0</u> g	_____ g	_____ g
Initial Volume:	<u>718.3</u> g	_____ g	_____ g
Net Volume:	<u>10.7</u> g	_____ g	_____ g
Total Moisture:	_____ g	_____ g	_____ g

(59.5)

Description of Inpinger catch: _____

PES Inc.

EPA Method 5 Calculations

Plant ATC - Balboa Pacific

Project # 5102

Operation Pyrolytic Waste Incinerator

Run 3 - Particulate

Location Santa Fe Springs, CA

Date 9/14/95

Emission Data

Vlc =	44.6	cc	Vol. of H2O collected (impingers)
Vm =	38.972	cf	Dry gas meter reading
Pb =	29.85	in. Hg	Barometric pressure
Ps =	29.85	in. Hg	Stack pressure
dP =	0.149		Average sq.rt delta P
dH =	1.010	in. H2O	Average draft gauge reading
Tm =	569.0	R	Average meter temperature
Ts =	842.00	R	Average stack temperature
Dn =	0.499	in.	Nozzle diameter
Y =	1.021		Meter calibration factor
t =	72	min.	Duration of sampling time
A =	2.3300	sq.ft.	Cross sectional area of stack
Cp =	0.84		Pitot tube coefficient
Kp =	85.49		Pitot tube constant
K1 =	17.64	R/in.Hg	constant
K2 =	0.04707	cu.ft/ml	constant
K3 =	0.002669	in.Hg-cf/ml-R	constant

1) Volume of gas sampled at standard conditions, Vmstd
 $Vmstd = K1 * Y * Vm * (Pb + dH/13.6) / Tm$

Vmstd = 36.91 cu.ft
1.05 cu.m

2) Volume of water vapor collected at standard conditions.

$Vw(std) = K2 * Vlc$

Vw(std) = 2.10 scf

3) Decimal fraction of moisture by volume in stack gas

$$Bws = Vwstd / (Vmstd + Vwstd)$$

$$Bws = 0.054$$

4) Molecular weight of the stack gas on a dry basis M_d .

$$Ms = ((44 * \%CO_2) + (28 * \%CO) + (32 * \%O_2) + (28 * \%N_2))$$

$$Ms = 29.11$$

Instrumental gas analysis

% CO ₂	2.88
% CO	0
% O ₂	16.33
% N ₂	80.79

5) Average stack gas velocity.

$$vs = Kp * Cp * (dP^{0.5}) * (Ts / Ps * Md)^{.5}$$

$$vs = 10.53 \text{ ft/sec}$$

6) Average actual stack gas volumetric flowrate.

$$Q = 60 * vs * As$$

$$Q = 1472.42 \text{ cfm}$$
$$41.70 \text{ cmm}$$

7) Average stack gas dry volumetric flowrate.

$$Qstd = Q * (Tstd / Ts) * (Ps / Pstd)$$

$$Qstd = 871.55 \text{ dscfm}$$
$$24.68 \text{ dscmm}$$

8) Analytical data

a) Front half acetone wash

0.0019 g wash net wt
0 g acetone blank net wt
100 ml blank vol.
133 ml Final wash volume
133 ml aliquot

0.0019 g soluble particulate*

b) Front half glass microfibre filter

0 g filter net wt

c) Back half water wash - soluble

0.0018 g net wt
0 g water blank net wt
220 ml blank vol
579.9 ml Final wash volume
579.9 ml aliquot

0.0018 g soluble net wt*

* Weights are not blank corrected

9) Particulate concentrations

0.0008 grains/dscf	Front 1/2
0.0015 grains/dscf	Total

11) Particulate emission rate

Conc. * (1 lb/7000 gr) * Qstd * 60 min/hr

W =	0.006 lbs/hr	Front 1/2
W =	0.012 lbs/hr	Total Particulate

12) Isokinecity

An = 0.001 ft² Area of nozzle orifice

$\% I = 100 * Ts * ((K3 * Vlc + (Vm * Y / Tm) (Pb + dH / 13.6)) / (60 * t * Ps * vs * An))$

$\% I = 100.97$

FIELD DATA

Plant ATC-Bu/Pac
 Date 9-14-95
 Sampling Location _____
 Sample Type MULTIPLE METALS
 Run Number ATC-6
 Operator MDKH
 Ambient Temperature 100°F
 Barometric Pressure 29.88
 Static Pressure +0.005
 Filter Number(s) _____
 Pretest Leak Rate 0.118 CFM @ 5.0 in. Hg
 Read And Record All Data Every 5 Minutes

Probe Length and Type 3' GLASS LINEP SS
 Pitot Tube I.D. No. 5-2A
 Nozzle I.D. No. And Diameter 1/6 0.453
 Assumed Moisture, % 6
 Meter Box Number 1A
 Meter Delta H @ 1.461
 C Factor _____
 Meter Gamma 1.021
 Heater Box Setting 020
 Reference Delta P _____
 Post test Leak Rate 0.020 CFM @ 5.0 in. Hg
 Impinger Box No. 3B Blank Box No. _____

Schematic of
Traverse Point Layout

Traverse Point Number	Sampling Time (minutes)	Clock Time (24 hr clock)	Gas Meter Reading Vm (cubic feet)	Velocity Head (in. H2O)	Orifice Pressure Differential (in. H2O) ΔH	Stack Temp. Ts (F)	Dry Gas Meter Temp. Inlet Tm in (F) Outlet Tm out (F)	Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
A6	5	11:20	042.451	0.030	1.24	397	101	3.0	253	222	73
A7	10	11:25	045.6	0.030	1.24	400	101	3.0	257	216	68
A6	15	11:30	048.5	0.040	1.66	401	104	4.0	255	238	66
A5	20	11:35	051.9	0.035	1.45	402	106	3.5	256	239	64
A4	25	11:40	055.1	0.040	1.66	398	107	4.0	257	245	63
A3	30	11:45	058.6	0.040	1.66	402	105	4.0	261	242	63
A2	35	11:50	062.1	0.030	1.24	376	105	3.0	254	237	62
A1	40	11:55	065.4	0.030	1.24	370	105	3.0	252	231	63
END/B0	45	12:00/05	068.3	0.045	1.87	395	108	4.0	250	232	67
B7	50	12:10	072.0	0.035	1.45	403	106	4.0	256	231	64
B4	55	12:15	075.3	0.040	1.66	402	106	4.0	255	238	66
B5	60	12:20	078.9	0.030	1.24	403	106	3.5	256	239	68
B4	65	12:25	082.2	0.030	1.24	401	107	3.5	258	237	68
B3	70	12:30	085.5	0.030	1.24	402	108	3.0	257	262	67
B2	75	12:35	088.5	0.025	1.04	378	108	3.0	254	253	66
B1	80	12:40	091.4	0.030	1.24	370	109	3.0	255	251	67
END/C6	85	12:45/50	094.4	0.040	1.66	401	110	4.0	251	266	67
C7	90	12:55	098.0	0.035	1.45	402	110	4.0	257	251	69
C6	95	13:00	101.2	0.035	1.45	403	110	4.0	254	250	67
C5	100	13:05	104.6	0.030	1.24	402	110	3.5	253	279	67
C4	105	13:10	107.7	0.025	1.04	400	116	3.0	256	272	64
C3	110	13:15	110.6	0.020	0.83	397	116	3.0	253	263	66
C2	115	13:20	113.2	0.010	0.41	373	116	1.0	254	265	67
C1	120	13:25	115.1	0.010	0.41	371	116	1.0	252	247	65
END	120	13:30	117.02-3	—	—	—	—	—	—	—	—

SAMPLE RETRIEVAL DATA

Plant: ATC
 Date: 9.14.92
 Sampling Location: _____
 Sampling Type (Method): EPA 12
 Run Number: ATC-5
 Sample Box Number: 3B
 Clean-up Man: _____
 Job Number: _____
 Comments: Sample # 988.2
T 356.3

Filter

Filter Number: _____
 Description of Filter: _____

Moisture

Impingers:			
Final Volume:	<u>676.0</u> mL	<u>617.5</u> mL	<u>480.4</u> mL
Initial Volume:	<u>626.1</u> mL	<u>609.0</u> mL	<u>474.5</u> mL
Net Volume:	<u>69.9</u> mL	<u>9.5</u> mL	<u>1.9</u> mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	<u>689.5</u> g	_____ g	_____ g
Initial Volume:	<u>676.1</u> g	_____ g	_____ g
Net Volume:	<u>13.4</u> g	_____ g	_____ g
Total Moisture:	_____ g	_____ g	_____ g

Description of Impinger catch: _____

PES, Inc.
Multi-Metals Method Calculations (EPA 12)

Plant ATC-Balboa Pacific

Project # 5102

Operation Pyrolytic Oxidation Unit

Run Batch 3

Location Outlet

Date 9/15/95

Test Data

Vlc =	86.2 cc	Vol. of H2O collected (impingers)
Vm =	65.825 cf	Dry gas meter reading
Pb =	29.85 in. Hg	Barometric pressure
Ps =	29.85 in. Hg	Stack pressure
dP =	0.155	Average sq.rt delta P
dH =	1.053 in. H2O	Average draft gauge reading
Tm =	565.6 R	Average meter temperature
Ts =	843.88 R	Average stack temperature
Dn =	0.495 in.	Nozzle diameter
Y =	1.021	Meter calibration factor
t =	120 min.	Duration of sampling time
A =	2.3300 sq.ft.	Cross sectional area of stack
Cp =	0.84	Pitot tube coefficient
Kp =	85.49	Pitot tube constant
K1 =	17.64 R/in.Hg	constant
K2 =	0.04707 cu.ft/ml	constant
K3 =	0.002669 in.Hg-cf/ml-	constant

Instrumentation Data

[O2] = 16.3 %
[CO2] = 2.9 %

CALCULATIONS

1) Volume of gas sampled at standard conditions, Vmstd
Vmstd = $K1 \cdot Y \cdot Vm \cdot (Pb + dH/13.6) / Tm$

Vmstd = 62.72 cu.ft
1.78 cu.m

2) Volume of water vapor collected at standard conditions.
 $V_w(\text{std}) = K_2 * V_{lc}$

$V_w(\text{std}) = 4.06 \text{ scf}$

3) Decimal fraction of moisture by volume in stack gas
 $B_{ws} = V_{wstd} / (V_{mstd} + V_{wstd})$

$B_{ws} = 0.061$

4) Molecular weight of the stack gas on a dry basis M_d .
 $M_d = (1 - B_{ws}) * ((44 * \%CO_2) + (28 * \%CO) + (32 * \%O_2) + (28 * \%N_2)) + (18 * B_{ws})$

$M_d = 28.44$

5) Average stack gas velocity.
 $v_s = K_p * C_p * (dP^{0.5}) * (T_s / P_s * M_d)^{.5}$

$v_s = 11.09 \text{ ft/sec}$

6) Average actual stack gas volumetric flowrate.
 $Q = 60 * v_s * A_s$

$Q = 1550.67 \text{ cfm}$
 43.92 cmm

7) Average stack gas dry volumetric flowrate.
 $Q_{std} = Q * (T_{std} / T_s) * (P_s / P_{std})$

$Q_{std} = 909.11 \text{ dscfm}$
 25.75 dscmm

8) Toxic metal concentrations and emission rates

Element	Sample Mass (ug)	Blank Mass (ug) DL	Conc. (mg/dscm)	Emission Rate (mg/hr)
Copper	7.00	1.00	2.72E-04	4.2E-01
Chromium	12.00	2.00	4.66E-04	7.2E-01
Lead	6.20	0.20	2.41E-04	3.7E-01
Zinc	58.00	8.00	2.25E-03	3.5E+00
Manganese	5.00	1.00	1.94E-04	3.0E-01
Nickel	5.20	0.40	2.02E-04	3.1E-01
Cadmium	5.00	2.00	1.94E-04	3.0E-01
Beryllium	1	1.00	3.88E-05	6.0E-02
Arsenic	2.4	0.20	9.32E-05	1.4E-01
Selenium	7	7.00	2.72E-04	4.2E-01
Molybdenum	2470	3.00	9.59E-02	1.5E+02
Silver	0.1	0.10	3.88E-06	6.0E-03
Antimony	3	3.00	1.17E-04	1.8E-01
Barium	34.2	0.40	1.33E-03	2.1E+00
Thallium	0.1	0.10	3.88E-06	6.0E-03

9) Isokinecity

An = 0.001 ft² Area of nozzle orifice

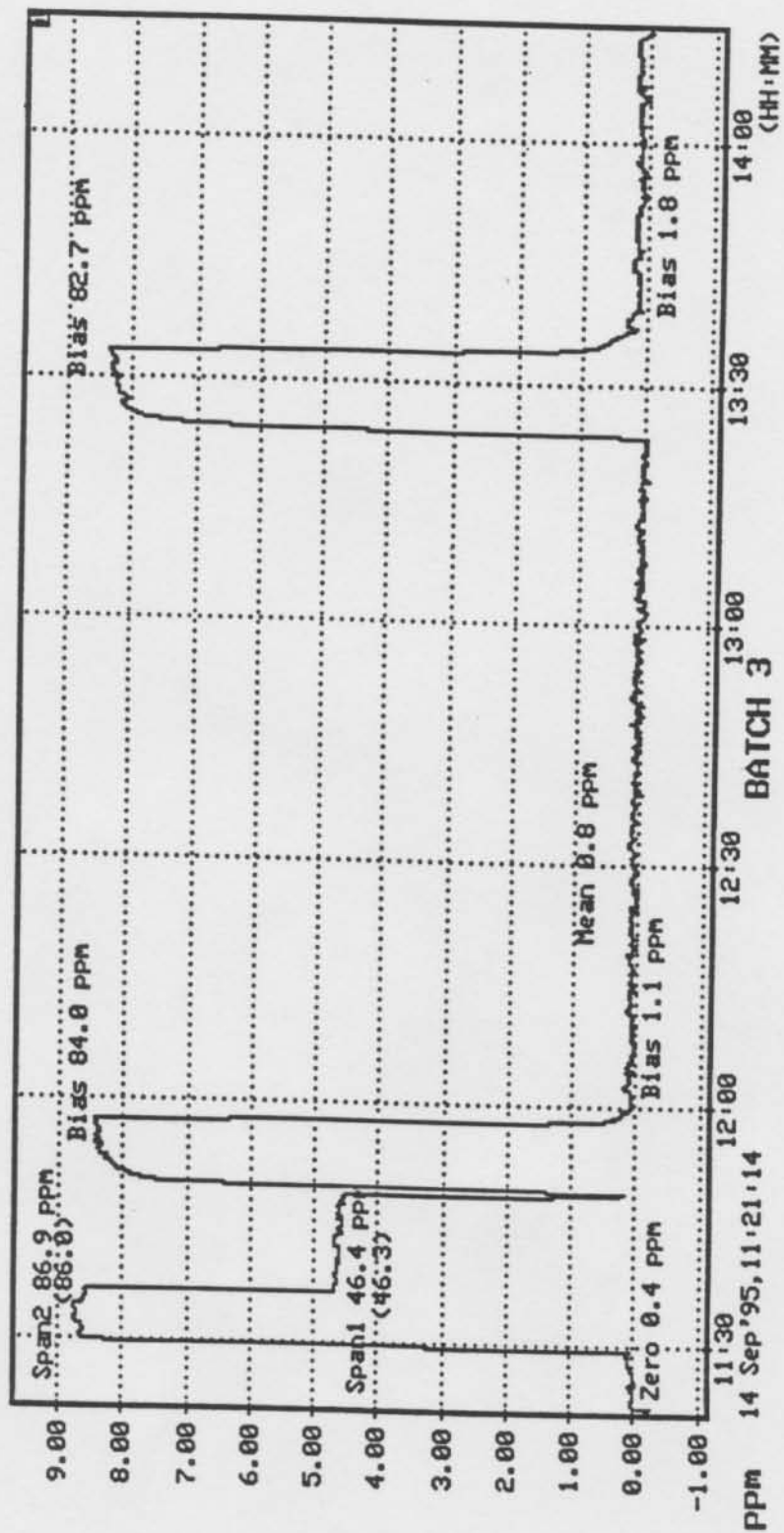
$\% I = 100 \cdot T_s \cdot ((K_3 \cdot V_{lc} + (V_m \cdot Y / T_m) (P_b + dH / 13.6)) / (60 \cdot t \cdot P_s \cdot v_s \cdot A_n))$

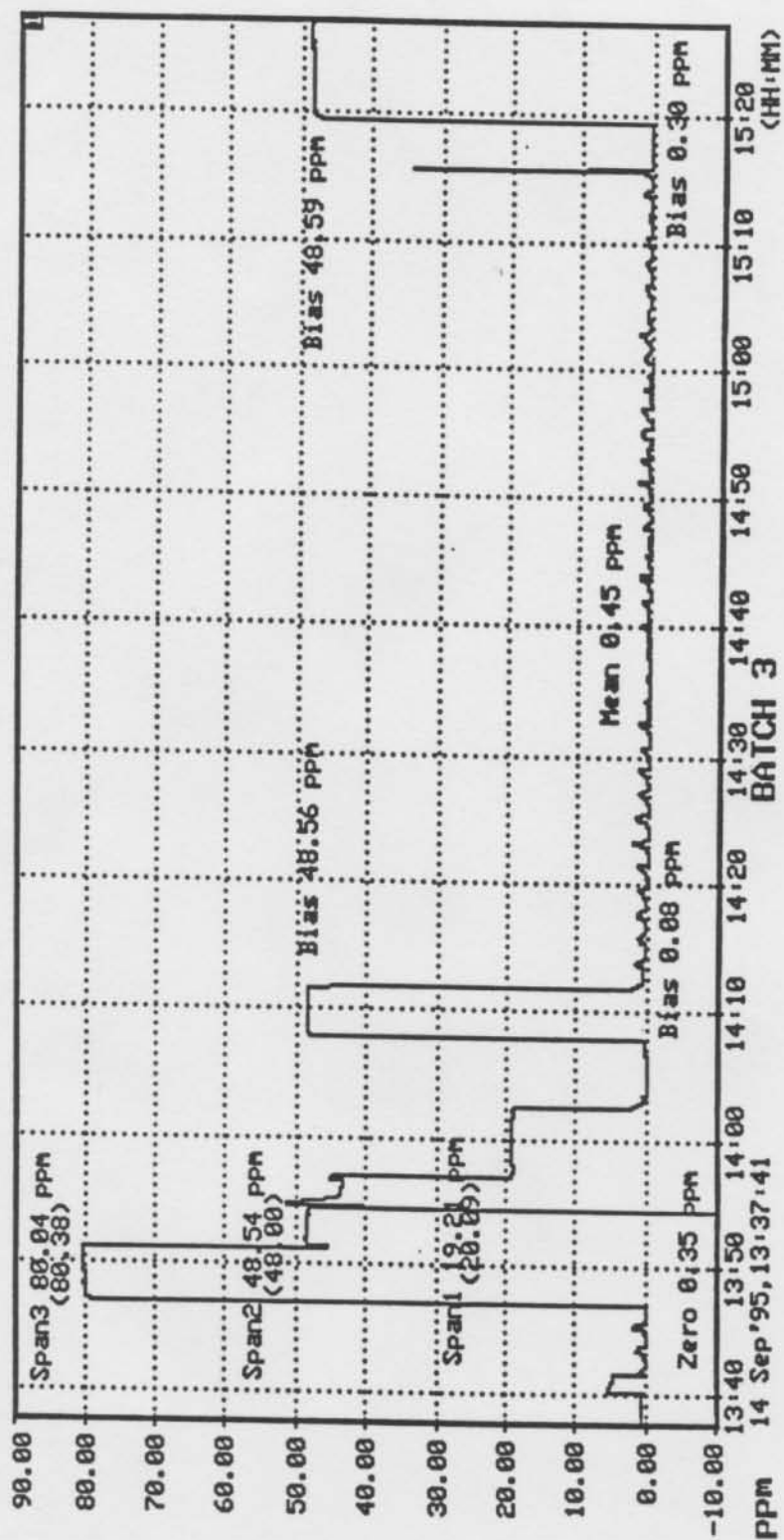
$\% I = 100.29$

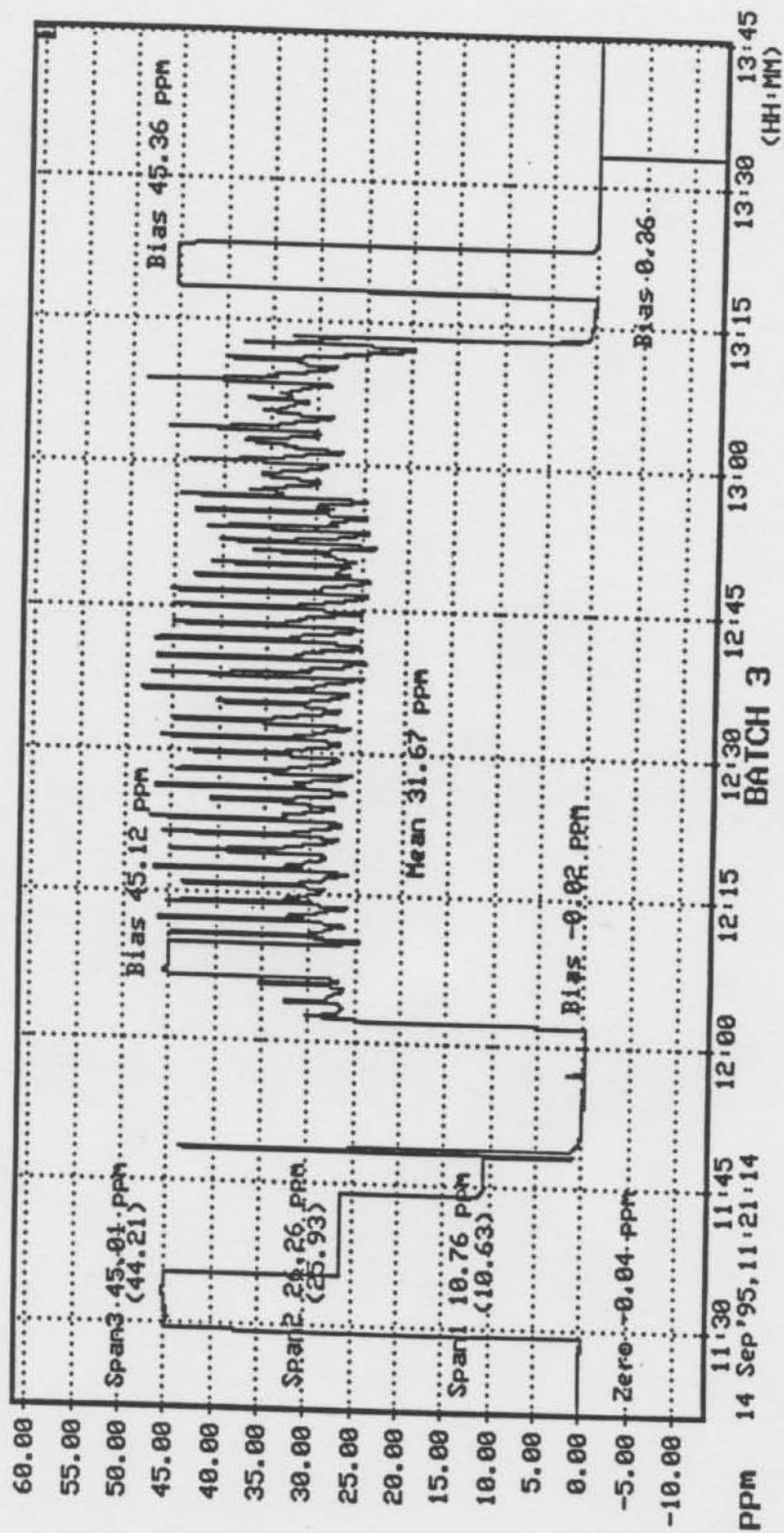
Sample Train Operation Data
 Test Date 9/15/95
 Barometer 29.85 in.Hg
 Run # 3
 Static P -0.02 in.H2O
 Pitot Cp 0.84
 Nozzle 0.495

Traverse Point	Delta-P (in. H2O)	Temp. (Deg.F)	delta H	Dry Gas Meter Temp IN	Meter Temp OUT	(dP) ^{-.5}
A-1	0.01	230	0.41	97	96	0.1
A-2	0.02	376	0.83	97	96	0.14142
A-3	0.03	390	1.24	99	97	0.17321
A-4	0.025	399	1.04	100	97	0.15811
A-5	0.02	405	0.83	103	98	0.14142
A-6	0.02	406	0.83	104	99	0.14142
A-7	0.02	406	0.83	105	100	0.14142
A-8	0.02	405	0.83	107	101	0.14142
B-1	0.01	356	0.41	106	103	0.1
B-2	0.01	366	0.41	107	103	0.1
B-3	0.01	389	0.41	107	103	0.1
B-4	0.015	406	0.62	108	104	0.12247
B-5	0.025	410	1.04	108	105	0.15811
B-6	0.03	409	1.24	111	108	0.17321
B-7	0.03	410	1.24	112	107	0.17321
B-8	0.03	411	1.24	113	107	0.17321
C-1	0.015	309	0.62	112	108	0.12247
C-2	0.02	339	0.83	111	108	0.14142
C-3	0.025	372	1.04	112	108	0.15811
C-4	0.035	398	1.45	112	108	0.18708
C-5	0.04	405	1.66	113	109	0.2
C-6	0.045	407	1.87	113	108	0.21213
C-7	0.05	406	2.07	112	108	0.22361
C-8	0.055	403	2.28	113	108	0.23452
Average		383.875	1.0529167	107.58333	103.708	0.15492
					105.646	

S O 2

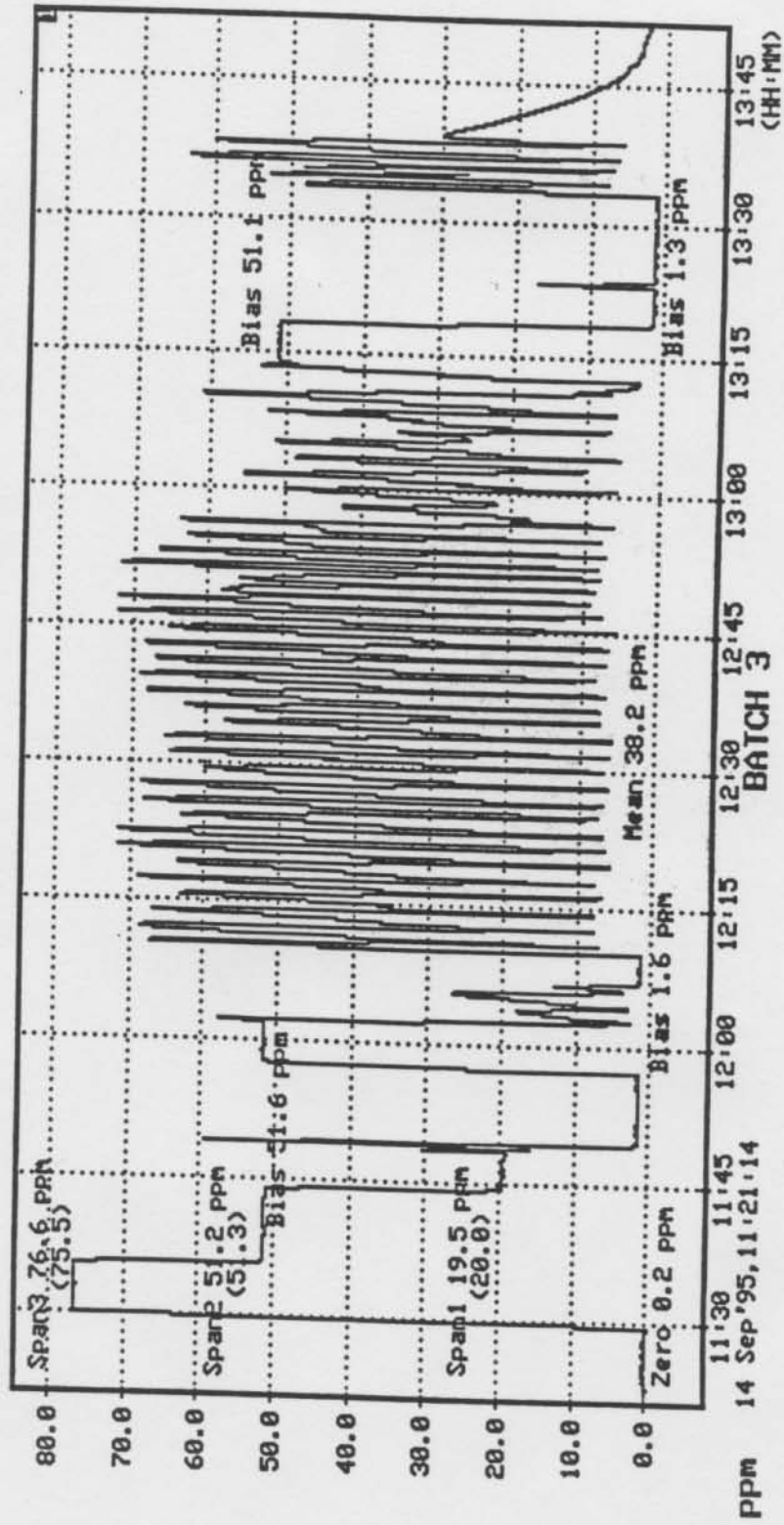




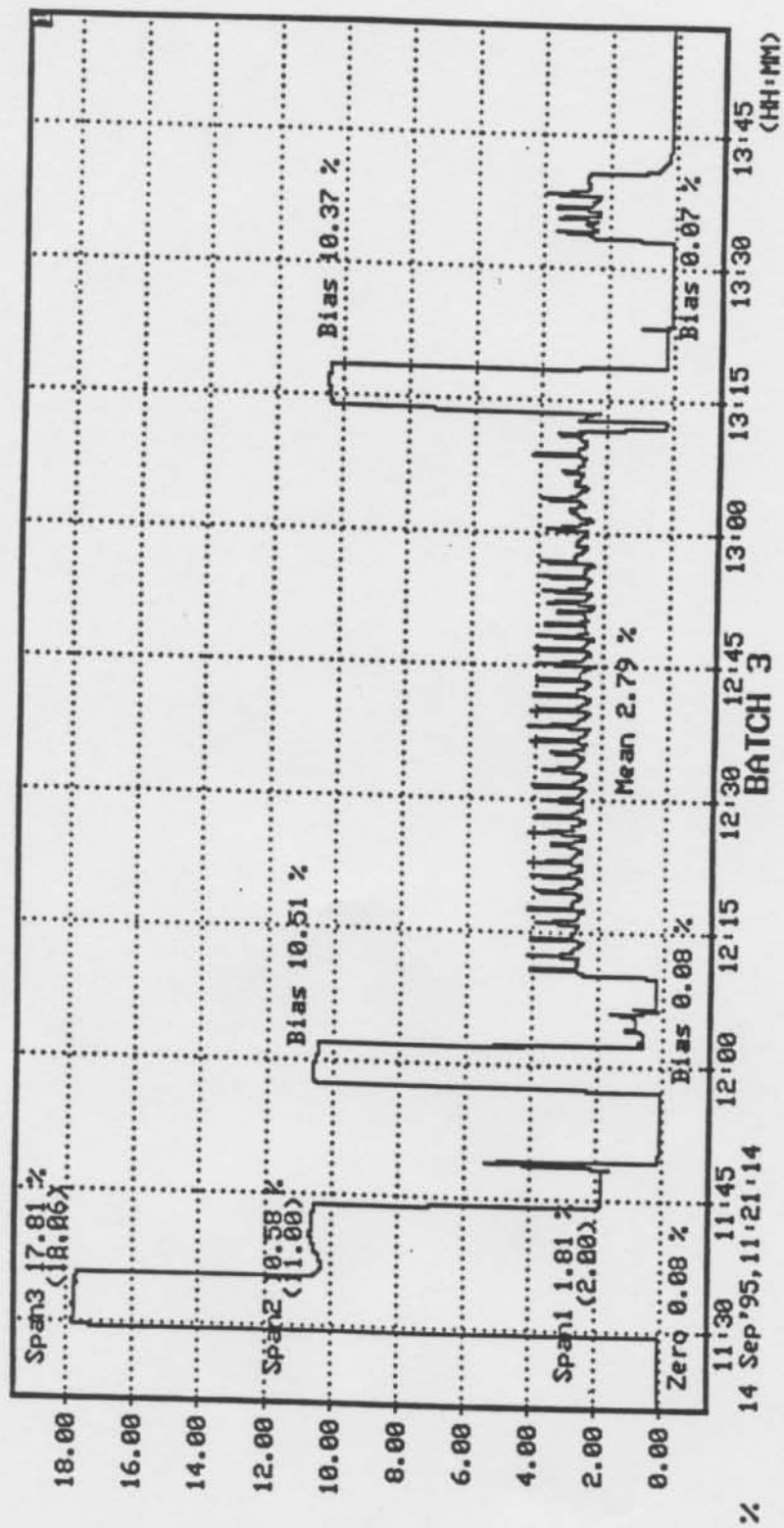


N O X

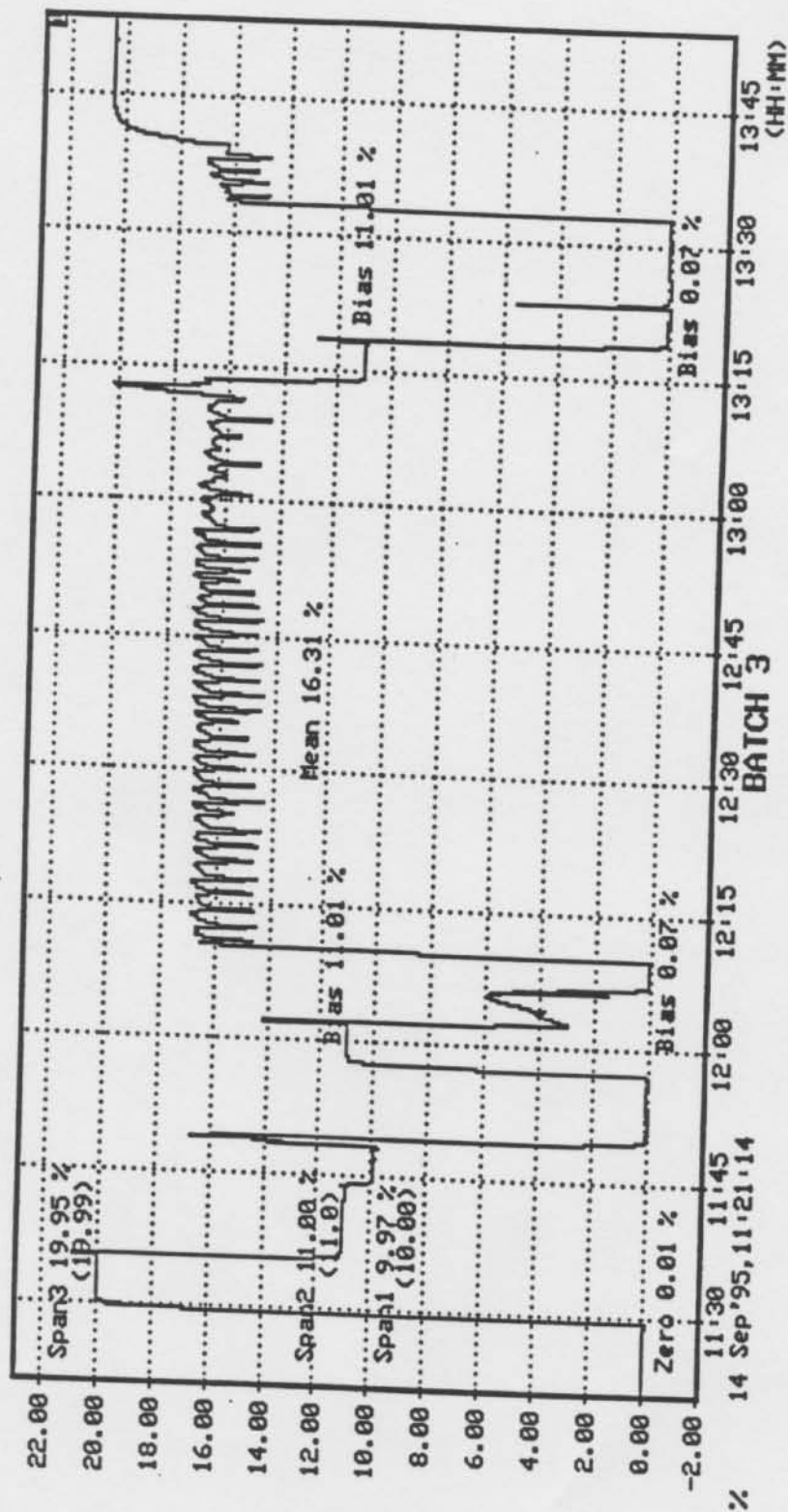
C
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O X Y G E N



PES Inc.

Calculations for :

EPA Method 2,3a,4,6c,7E,10
and 25a

Plant ATC Consultants - Balboa Pacific
Project # 5102
Operation Pyrolytic Unit
Run 3
Load Batch 3
Location Santa Fe Springs, CA
Date 9/14/95

D A T A I N P U T

INPUT	Vlc =	59.9 cc	Vol. of H2O collected
INPUT	Vm =	45.020 cf	Dry gas meter reading
INPUT	Pb =	29.88 in. Hg	Barometric pressure
INPUT	Pg =	-0.02 in. H2O	Static pressure
INPUT	dP =	0.173	Avg. sq.rt delta P
INPUT	dH =	1.310 in. H2O	Avg. delta H
INPUT	Tm =	571.5 R	Avg. meter temp.
INPUT	Ts =	831.9 R	Avg. stack temp.
INPUT	Y =	1.021	Meter calibration factor
INPUT	t =	72 min.	Duration of sampling time
INPUT	A =	2.3300 sq.ft.	Stack Area
INPUT	Cp =	0.84	Pitot tube coefficient
	Kp =	85.49	Pitot tube constant
	K1 =	17.64 R/in.Hg	constant
	K2 =	0.04707 cu.ft/ml	constant
	K3 =	0.002669 in.Hg-cf/	constant

	Gas Analysis	
INPUT	[O2] =	16.31 % (dry)
INPUT	[O2] =	0.07 initial zero bias
INPUT	[O2] =	0.07 final zero bias
	[O2] =	0.07 average zero bias
INPUT	[O2] =	11 midspan concentration
INPUT	[O2] =	11.01 initial midspan bias
INPUT	[O2] =	11.01 final midspan bias
	[O2] =	11.01 average midspan bias
INPUT	[CO2] =	2.79 % (dry)
INPUT	[CO2] =	0.08 initial zero bias
INPUT	[CO2] =	0.07 final zero bias
	[CO2] =	0.08 average zero bias
INPUT	[CO2] =	11 midspan concentration
INPUT	[CO2] =	10.51 initial midspan bias
INPUT	[CO2] =	10.37 final midspan bias
	[CO2] =	10.44 average midspan bias
	[O2] =	16.33 adjusted concentration
	[CO2] =	2.88 adjusted concentration
	[N2] =	80.8 %
INPUT	[CO] =	38.20 ppmV (dry)
INPUT	[CO] =	1.6 initial zero bias
INPUT	[CO] =	1.3 final zero bias
	[CO] =	1.45 average zero bias
INPUT	[CO] =	51.3 midspan concentration
INPUT	[CO] =	51.6 initial midspan bias
INPUT	[CO] =	51.1 final midspan bias
	[CO] =	51.35 average midspan bias
INPUT	[NOx] =	31.7 ppmV (dry)
INPUT	[NOx] =	-0.02 initial zero bias
INPUT	[NOx] =	0.36 final zero bias
	[NOx] =	0.17 average zero bias
INPUT	[NOx] =	44.21 midspan concentration
INPUT	[NOx] =	45.12 initial midspan bias
INPUT	[NOx] =	45.36 final midspan bias
	[NOx] =	45.24 average midspan bias
INPUT	[THC] =	0.5 ppmV (wet)
INPUT	[THC] =	0.08 initial zero bias
INPUT	[THC] =	0.3 final zero bias
	[THC] =	0.19 average zero bias
INPUT	[THC] =	48 midspan concentration
INPUT	[THC] =	48.56 initial midspan bias
INPUT	[THC] =	48.59 final midspan bias
	[THC] =	48.575 average midspan bias
INPUT	[SO2] =	0.8 ppmV (dry)
INPUT	[SO2] =	1.1 initial zero bias
INPUT	[SO2] =	1.8 final zero bias
	[SO2] =	1.45 average zero bias
INPUT	[SO2] =	86 midspan concentration
INPUT	[SO2] =	84 initial midspan bias
INPUT	[SO2] =	82.7 final midspan bias
	[SO2] =	83.35 average midspan bias
	[CO] =	37.78 ppmV (dry) adj concentration
	[NOx] =	30.90 ppmV (dry) adj concentration
	[THC] =	0.26 ppmV (wet) adj concentration
	[SO2] =	-0.68 ppmV (dry) adj concentration

CALCULATIONS

01) Volume of gas sampled at standard conditions, V_{mstd}

$$V_{mstd} = K_1 * Y * V_m * (P_b + dH/13.6) / T_m$$

$$V_{mstd} = \begin{array}{ll} 42.53 & \text{cu.ft} \\ 1.20 & \text{cu.m} \end{array}$$

02) Volume of water vapor collected at standard conditions.

$$V_w(std) = K_2 * V_{lc}$$

$$V_w(std) = 2.82 \text{ scf}$$

03) Decimal fraction of moisture by volume in stack gas

$$B_{ws} = V_{wstd} / (V_{mstd} + V_{wstd})$$

$$B_{ws} = 0.062$$

04) Molecular weight of the stack gas on a wet basis

$$M_s = (1-Q) * ((44 * \%CO_2) + (28 * \%CO) + (32 * \%O_2) + (28 * \%N_2)) + (18 * Q)$$

$$M_s = 28.38$$

05) Average stack gas velocity.

$$P_s = 29.88 \text{ in. Hg}$$

$$v_s = K_p * C_p * (dP^{0.5}) * (T_s / P_s * M_d)^{-0.5}$$

$$v_s = 12.29 \text{ ft/sec}$$

06) Average actual stack gas volumetric flowrate.

$$Q = 60 * v_s * A_s$$

$$Q = \begin{array}{ll} 1717.44 & \text{cfm} \\ 48.64 & \text{cmm} \end{array}$$

07) Average stack gas dry volumetric flowrate.

$$Q_{std} = Q * (T_{std} / T_s) * (P_s / P_{std}) * (1 - B_{ws})$$

$$Q_{std} = \begin{array}{ll} 1020.89 & \text{dscfm} \\ 28.91 & \text{dscmm} \\ 61253.10 & \text{dscfh} \end{array}$$

08) Emission Calculation - Carbon Monoxide

$$\text{lbs CO/hr} = ([\text{CO}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[CO] =	37.78	ppmv (dry)	Actual conc.
[CO] =	0.17	Lbs/hr	

09) Emission Calculation - Nitrogen Oxides

$$\text{lbs NOx/hr} = ([\text{NOx}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[NOx] =	30.9	ppmv (dry)	Actual Conc.
[NOx] =	0.23	Lbs/hr	

10) Emission Calculation - Total Hydrocarbons

$$\text{lbs THC/hr} = ([\text{THC}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[THC] =	0.3	ppmv (dry)	Actual Conc.
[THC] =	0.00	Lbs/hr	

11) Emission Calculation - Sulfur Dioxide

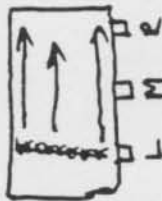
$$\text{lbs NMHC/hr} = ([\text{NMHC}] * \text{DSCFH} * \text{MW}) / 387 * 10^6$$

[SO2] =	-0.7	ppmv (dry)	Actual Conc.
[SO2] =	0.00	Lbs/hr	

FIELD DATA

Plant ATC Ballboa Pacific
 Date 10-3-95
 Sampling Location EXHAUST STACK
 Sample Type EPA METHOD 5
 Run Number 135/ATC2 FMI
 Operator NEWMAN/MARKH
 Ambient Temperature 90
 Barometric Pressure 29.80
 Static Pressure -0.005
 Filter: Number(s) —
 Pretest Leak Rate 0.017 CFM @ 4 in. Hg
 Read And Record All Data Every 3 Minutes

TOP VIEW



FLOW OUT OF PAPER

Schematic of

Traverse Point Layout

Traverse Point Number	Sampling Time (minutes)	Clock Time (24 hr clock)	Gas Meter Reading V_m (cubic feet)	Velocity Head P_s (in. H ₂ O)	Orifice Pressure Differential (in. H ₂ O) ΔH		Stack Temp. T_s (F)	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
					Desired	Actual		Inlet T_m in (F)	Outlet T_m out (F)				
L0	0	9:42	037.516	0.04	1.70	✓	391	90	76	3.5	248	269	68
L7	3	9:45	041.300	0.03	1.25	✓	394	80	76	3.0	252	268	67
L6	6	9:48	043.072	0.03	1.25	✓	395	83	77	3.0	251	269	64
L5	9	9:51	044.800	0.03	1.25	✓	395	83	77	3.0	253	269	65
L4	12	9:54	046.531	0.03	0.84	✓	388	84	79	2.5	251	269	64
L3	15	9:57	048.280	0.01	0.44	✓	347	85	80	2.0	241	269	64
L2	18	10:00	049.223	0.01	0.44	✓	354	85	80	2.0	248	269	65
L1	21	10:03	050.000	0.005	0.22	✓	354	85	80	2.0	248	269	64
END/HR	24	10:06/10:10	051.500	0.01	0.44	✓	367	86	82	2.0	247	269	63
M7	27	10:13	052.517	0.01	0.44	✓	388	87	82	2.0	246	271	63
M6	30	10:16	053.641	0.01	0.44	✓	395	89	83	2.0	250	270	63
M5	33	10:19	054.752	0.005	0.22	✓	353	89	84	2.0	249	270	64
M4	36	11:22	055.580	0.005	0.22	✓	385	91	85	2.0	247	270	64
M3	39	11:25	056.415	0.005	0.22	✓	361	91	85	2.0	248	270	66
M2	42	11:28	057.229	0.005	0.22	✓	301	92	86	2.0	248	269	65
M1	45	11:31	058.049	0.005	0.22	✓	301	92	87	2.0	246	268	64
END/RR	48	11:34/11:36	059.882	0.02	0.84	✓	344	93	88	2.5	244	269	67
R7	51	10:39	060.300	0.01	0.44	✓	373	94	91	2.5	246	270	59
R6	54	10:42	061.579	0.01	0.44	✓	396	95	91	2.5	251	270	60
R5	57	10:45	062.730	0.01	0.44	✓	395	95	91	2.0	248	270	62
R4	60	10:48	063.420	0.01	0.44	✓	394	96	91	2.0	247	271	63
R3	63	10:51	064.177	0.005	0.22	✓	387	96	92	2.0	246	269	63
R2	66	10:54	065.796	0.005	0.22	✓	305	96	93	2.0	246	271	65
R1	69	10:57	066.583	0.005	0.22	✓	—	96	93	2.0	247	268	65
END	72	11:00	067.453	—	—	—	—	—	93	—	—	—	—

0:72

 $V_m = 27.937 \text{ fpm} = 0.106$ $\Delta H = 0.54$ $T_m = 86 + 460$ $= 546$

SAMPLE RETRIEVAL DATA

Plant: ATC-BALBOA
 Date: 10-3-95
 Sampling Location: OUTLET
 Sampling Type (Method): PARTICULATE
 Run Number: PM1
 Sample Box Number: 7B
 Clean-up Man: MOKH
 Job Number: _____
 Comments: _____

Filter

Filter Number: _____
 Description of Filter: SLIGHTLY COLORED WITH SMALL BLACK PARTICLES
(WDS)

Moisture

	#1	#2	#3
Impingers:			
Final Volume:	<u>605.4</u> mL	<u>603.3</u> mL	<u>501.8</u> mL
Initial Volume:	<u>584.9</u> mL	<u>596.0</u> mL	<u>500.1</u> mL
Net Volume:	<u>20.5</u> mL	<u>7.3</u> mL	<u>1.7</u> mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	<u>656.6</u> g	_____ g	_____ g
Initial Volume:	<u>649.4</u> g	_____ g	_____ g
Net Volume:	<u>7.2</u> g	_____ g	_____ g
Total Moisture:	_____ g	_____ g	_____ g

Description of Impinger catch: 36.7

PES Inc.

EPA Method 5 Calculations

Plant ATC - Balboa Pacific

Project # 5102

Operation Pyrolytic Waste Incinerator

Run 1 - Particulate - set 2

Location Santa Fe Springs, CA

Date 10/3/95

Emission Data

Vlc =	36.7	cc	Vol. of H2O collected (impingers)
Vm =	27.937	cf	Dry gas meter reading
Pb =	29.8	in. Hg	Barometric pressure
Ps =	29.80	in. Hg	Stack pressure
dP =	0.106		Average sq.rt delta P
dH =	0.540	in. H2O	Average draft gauge reading
Tm =	546.0	R	Average meter temperature
Ts =	897.00	R	Average stack temperature
Dn =	0.494	in.	Nozzle diameter
Y =	1.003		Meter calibration factor
t =	72	min.	Duration of sampling time
A =	2.3300	sq.ft.	Cross sectional area of stack
Cp =	0.84		Pitot tube coefficient
Kp =	85.49		Pitot tube constant
K1 =	17.64	R/in.Hg	constant
K2 =	0.04707	cu.ft/ml	constant
K3 =	0.002669	in.Hg-cf/ml-R	constant

1) Volume of gas sampled at standard conditions, Vmstd
 $Vmstd = K1 * Y * Vm * (Pb + dH/13.6) / Tm$

Vmstd = 27.01 cu.ft
0.77 cu.m

2) Volume of water vapor collected at standard conditions.

$Vw(std) = K2 * Vlc$

Vw(std) = 1.73 scf

3) Decimal fraction of moisture by volume in stack gas

$$Bws = Vwstd / (Vmstd + Vwstd)$$

$$Bws = 0.060$$

4) Molecular weight of the stack gas on a dry basis M_d .

$$Ms = ((44 * \%CO_2) + (28 * \%CO) + (32 * \%O_2) + (28 * \%N_2))$$

$$Ms = 29.06$$

Instrumental gas analysis

% CO ₂	2.65
% CO	0
% O ₂	15.95
% N ₂	81.4

5) Average stack gas velocity.

$$vs = Kp * Cp * (dP^{0.5}) * (Ts / Ps * Md)^{-0.5}$$

$$vs = 7.75 \text{ ft/sec}$$

6) Average actual stack gas volumetric flowrate.

$$Q = 60 * vs * As$$

$$Q = 1083.02 \text{ cfm}$$

$$30.67 \text{ cmm}$$

7) Average stack gas dry volumetric flowrate.

$$Qstd = Q * (Tstd / Ts) * (Ps / Pstd)$$

$$Qstd = 596.77 \text{ dscfm}$$

$$16.90 \text{ dscmm}$$

8) Analytical data

a) Front half acetone wash

0.0022 g wash net wt
0.0002 g acetone blank net wt
100 ml blank vol.
133 ml Final wash volume
133 ml aliquot

0.0022 g soluble particulate*

b) Front half glass microfibre filter

0.0032 g filter net wt

c) Back half water wash - soluble

0.0012 g net wt
0 g water blank net wt
220 ml blank vol
579.9 ml Final wash volume
579.9 ml aliquot

0.0012 g soluble net wt*

* Weights are not blank corrected

9) Particulate concentrations

0.0031 grains/dscf Front 1/2
0.0038 grains/dscf Total

11) Particulate emission rate

Conc. * (1 lb/7000 gr) * Qstd * 60 min/hr

W = 0.016 lbs/hr Front 1/2
W = 0.019 lbs/hr Total Particulate

12) Isokinecity

An = 0.001 ft² Area of nozzle orifice

$\% I = 100 * Ts * ((K3 * Vlc + (Vm * Y / Tm) (Pb + dH / 13.6)) / (60 * t * Ps * vs * An))$

$\% I = 110.11$

FIELD DATA

Plant ATC Ballboa Pacific
 Date 10-3-95
 Sampling Location EXHAUST STACK
 Sample Type EPA METHOD 12
 Run Number RES/ATC 2 MM1
 Operator NEWMAN/MOKH
 Ambient Temperature 90
 Barometric Pressure 24.20
 Static Pressure + 0.01
 Filter Number(s) —

Pretest Leak Rate 0.016 CFM @ 5 in. Hg
 Read And Record All Data Every 5 Minutes

Probe Length and Type 3' Glass Lined
 Pitot Tube I.D. No. S-21
 Nozzle I.D. No. And Diameter M4 0.504
 Assumed Moisture, % 2
 Meter Box Number 4A
 Meter Delta H @ 1.826
 C Factor 1.25
 Meter Gamma 1.095
 Heater Box Setting 250
 Reference Delta P $\Delta Pa = 0.041$
 Post test Leak Rate 0.017 CFM @ 3 in. Hg
 Impinger Box No. 33 Blank Box No. —

Schematic of
Traverse Point Layout

Traverse Point Number	Sampling Time (minutes)	Clock Time (24 hr clock)	Gas Meter Reading Vm (cubic feet)	Velocity Head Ps (in. H2O)	Orifice Pressure Differential (in. H2O) ΔH		Stack Temp. Ts (F)	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
					Desired	Actual		Inlet Tm in (F)	Outlet Tm out (F)				
L6	0	11:00	613.203	0.03	1.35	✓	400	86	86	2.0	284	280	107
L7	5	11:15	616.689	0.03	1.35	✓	399	89	86	2.0	—	232	55
L6	10	11:20	619.168	0.04	1.80	✓	402	93	88	2.5	252	246	50
L5	15	11:25	622.684	0.03	1.35	✓	402	97	94	3.0	253	252	53
L4	20	11:30	625.565	0.02	0.90	✓	399	100	91	2.6	253	251	54
L3	25	11:35	628.579	0.01	0.45	✓	397	102	93	2.0	254	244	51
L2	30	11:40	630.550	0.005	0.24	✓	355	100	97	1.0	—	250	63
L1	35	11:45	632.1070	0.005	0.24	✓	359	99	72	1.0	244	247	62
END/MS	40	11:50/12:14	633.400	0.01	0.45	✓	346	99	99	1.0	246	246	61
M7	45	12:19	635.561	0.005	0.24	✓	398	101	99	1.0	250	244	102
M6	50	12:24	636.900	0.005	0.24	✓	396	100	99	1.0	250	244	104
M5	55	12:29	638.200	0.005	0.24	✓	396	102	100	1.5	249	247	66
M4	60	12:34	639.968	0.02	0.90	✓	396	105	103	1.5	249	247	60
M3	65	12:39	642.000	0.02	0.90	✓	391	106	103	1.5	251	247	63
M2	70	12:44	645.350	0.02	0.90	✓	350	107	103	1.5	251	247	66
M1	75	12:49	647.944	0.02	0.90	✓	350	107	103	1.5	251	247	66
END/MS	80	12:54/12:58	650.700	0.02	0.90	✓	391	106	103	2.0	252	248	64
R7	85	13:01	653.500	0.03	1.35	✓	392	110	104	2.0	252	248	66
R6	90	13:06	656.623	0.03	1.35	✓	391	110	103	2.0	248	244	66
R5	95	13:11	659.849	0.03	1.35	✓	385	107	103	2.0	244	244	66
R4	100	13:16	663.081	0.03	1.35	✓	383	109	103	1.5	250	246	67
R3	105	13:21	666.361	0.02	0.90	✓	380	111	106	1.5	246	243	67
R2	110	13:26	669.142	0.02	0.90	✓	349	111	107	1.5	246	244	67
R1	115	13:31	671.900	0.01	0.45	✓	—	114	107	—	—	—	—
END	120	13:36	674.990	—	—	—	—	—	—	—	—	—	—

Q=120

Vm=61.787 VAP=0.126

AT=0.875

Ts=345.440

Tm=100 +460

=425

SAMPLE RETRIEVAL DATA

Plant: ATC-BALBOA
 Date: 10-3-95
 Sampling Location: OUTLET
 Sampling Type (Method): M.M.
 Run Number: MM1
 Sample Box Number: LB
 Clean-up Man: MUKH
 Job Number: _____
 Comments: 579.0-60.1 =
284.6-59.0 =

Filter

Filter Number: _____
 Description of Filter: SLIGHTLY COLORED (GREEN) BLACK SOLID PARTICLES
ON FILTER (LOOSE)

Moisture

Impingers:			
Final Volume:	<u>669.9</u> mL	<u>607.4</u> mL	<u>483.9</u> mL
Initial Volume:	<u>616.7</u> mL	<u>596.9</u> mL	<u>482.1</u> mL
Net Volume:	<u>53.2</u> mL	<u>10.5</u> mL	<u>1.8</u> mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	<u>689.0</u> g	_____ g	_____ g
Initial Volume:	<u>677.2</u> g	_____ g	_____ g
Net Volume:	<u>11.8</u> g	_____ g	_____ g
Total Moisture:	_____ g	_____ g	_____ g

77.3

Description of Impinger catch: WEAR

PES, Inc.
Multi-Metals Method Calculations (EPA 12)

Plant ATC-Balboa Pacific
Project # 5102
Operation Pyrolytic Oxidation Unit
Run ↓
Location Outlet
Date 10/3/95

Test Data

Vlc =	77.3 cc	Vol. of H2O collected (impingers)
Vm =	61.787 cf	Dry gas meter reading
Pb =	29.8 in. Hg	Barometric pressure
Ps =	29.80 in. Hg	Stack pressure
dP =	0.132	Average sq.rt delta P
dH =	0.875 in. H2O	Average draft gauge reading
Tm =	560.3 R	Average meter temperature
Ts =	841.42 R	Average stack temperature
Dn =	0.504 in.	Nozzle diameter
Y =	1.005	Meter calibration factor
t =	120 min.	Duration of sampling time
A =	2.3300 sq.ft.	Cross sectional area of stack
Cp =	0.84	Pitot tube coefficient
Kp =	85.49	Pitot tube constant
K1 =	17.64 R/in.Hg	constant
K2 =	0.04707 cu.ft/ml	constant
K3 =	0.002669 in.Hg-cf/ml	constant

Instrumentation Data

[O2] = 16.0 %
[CO2] = 2.7 %

CALCULATIONS

1) Volume of gas sampled at standard conditions, Vmstd
Vmstd = $K1 \cdot Y \cdot Vm \cdot (Pb + dH/13.6) / Tm$

Vmstd = 58.39 cu.ft
1.65 cu.m

2) Volume of water vapor collected at standard conditions.
 $V_w(\text{std}) = K_2 * V_{lc}$

$V_w(\text{std}) = 3.64 \text{ scf}$

3) Decimal fraction of moisture by volume in stack gas
 $B_{ws} = V_{wstd} / (V_{mstd} + V_{wstd})$

$B_{ws} = 0.059$

4) Molecular weight of the stack gas on a dry basis M_d .
 $M_d = (1 - B_{ws}) * ((44 * \%CO_2) + (28 * \%CO) + (32 * \%O_2) + (28 * \%N_2)) + (18 * B_{ws})$

$M_d = 28.41$

5) Average stack gas velocity.
 $v_s = K_p * C_p * (dP^{0.5}) * (T_s / P_s * M_d)^{-0.5}$

$v_s = 9.44 \text{ ft/sec}$

6) Average actual stack gas volumetric flowrate.
 $Q = 60 * v_s * A_s$

$Q = 1320.01 \text{ cfm}$
 37.38 cmm

7) Average stack gas dry volumetric flowrate.
 $Q_{std} = Q * (T_{std} / T_s) * (P_s / P_{std})$

$Q_{std} = 776.62 \text{ dscfm}$
 21.99 dscmm

8) Toxic metal concentrations and emission rates

Element	Sample Mass (ug)	Blank Mass (ug) DL	Conc. (mg/dscm)	Emission Rate (mg/hr)
Copper	12.00	1.00	5.46E-04	7.2E-01
Chromium	6.00	6.00	2.73E-04	3.6E-01
Lead	12.70	0.10	5.77E-04	7.6E-01
Zinc	109.00	9.00	4.96E-03	6.5E+00
Manganese	4.00	4.00	1.82E-04	2.4E-01
Nickel	9.00	9.00	4.09E-04	5.4E-01
Cadmium	3.00	1.00	1.36E-04	1.8E-01
Beryllium	1.00	1.00	4.55E-05	6.0E-02
Arsenic	0.10	0.10	4.55E-06	6.0E-03
Selenium	10.00	10.00	4.55E-04	6.0E-01
Molybdenum	801.00	2.00	3.64E-02	4.8E+01
Silver	0.10	0.10	4.55E-06	6.0E-03
Antimony	2.00	2.00	9.09E-05	1.2E-01
Barium	4.00	1.00	1.82E-04	2.4E-01
Thallium	0.20	0.20	9.09E-06	1.2E-02

9) Isokinecity

An = 0.001 ft² Area of nozzle orifice

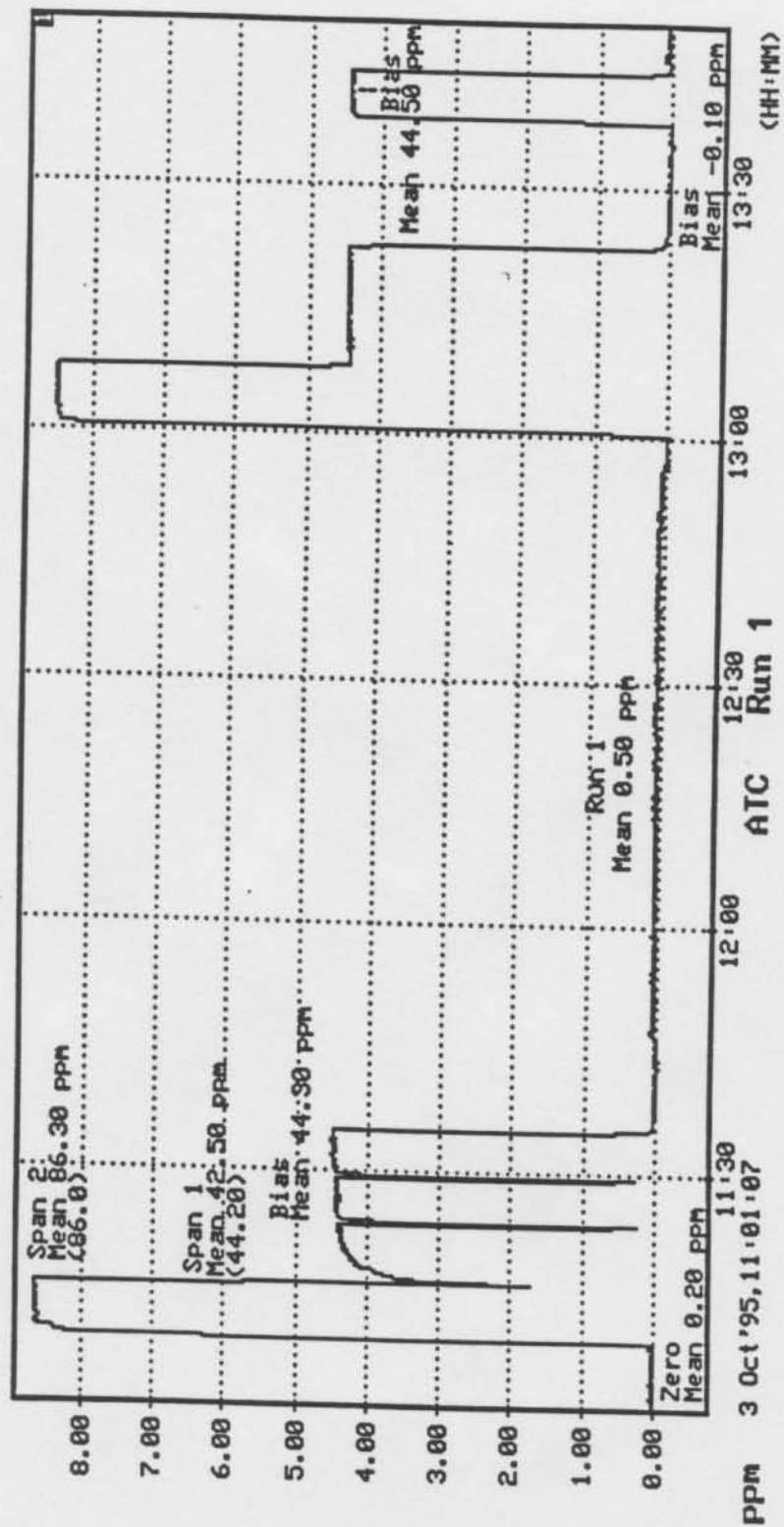
$\% I = 100 \cdot T_s \cdot ((K_3 \cdot V_{lc} + (V_m \cdot Y / T_m) (Pb + dH / 13.6)) / (60 \cdot t \cdot P_s \cdot v_s \cdot A_n))$

$\% I = 105.41$

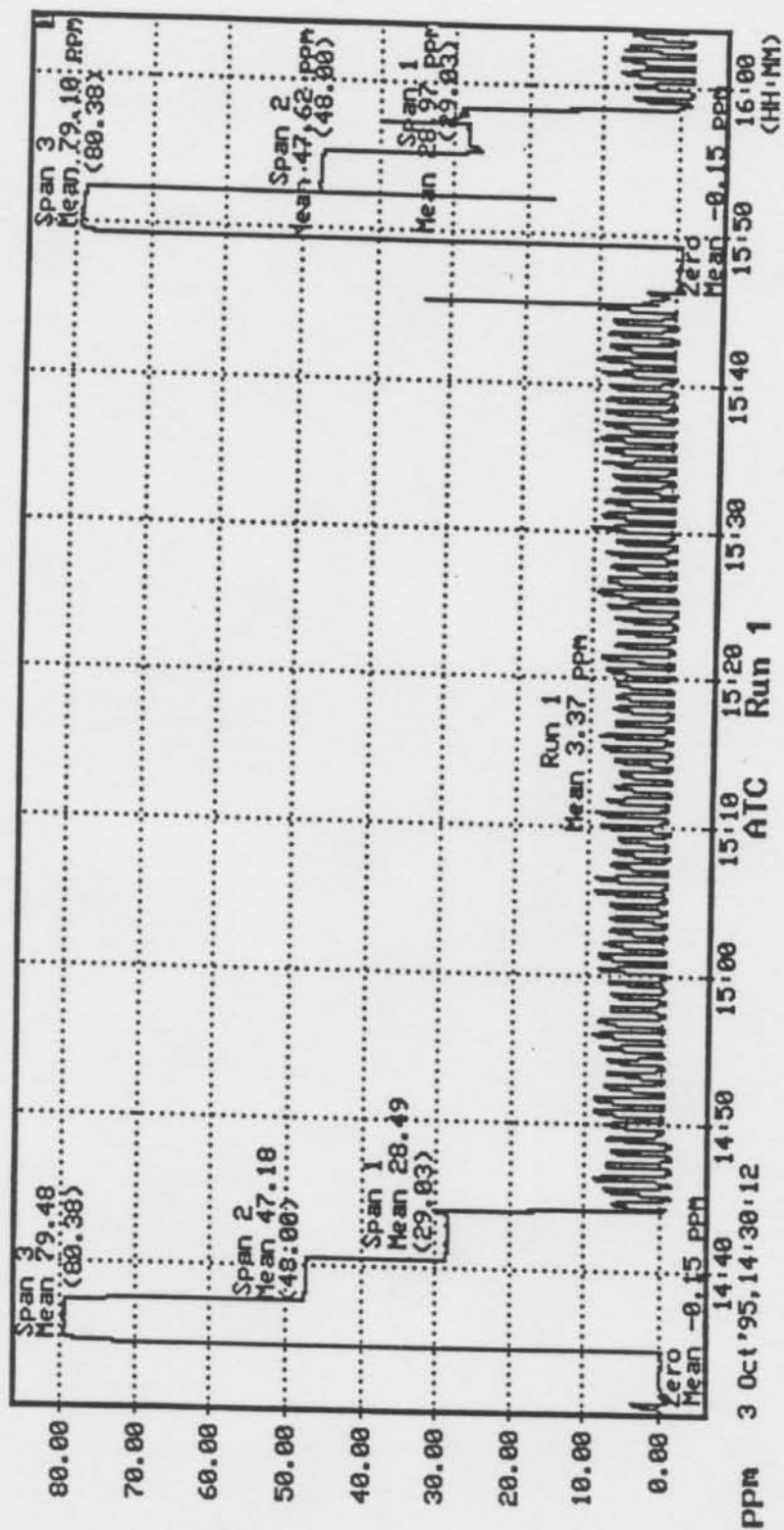
Sample Train Operation Data
 Test Date 10/3/95
 Barometer 29.85 in.Hg
 Run # 1
 Static P 0.01 in.H2O
 Pitot Cp 0.84
 Nozzle 0.504

Traverse Point	Delta-P (in. H2O)	Temp. (Deg.F)	delta H	Dry Gas Meter Temp IN	Temp OUT	(dP) ^{-.5}
A-1	0.03	400	1.35	88	86	0.17321
A-2	0.02	399	1.35	89	86	0.14142
A-3	0.04	402	1.8	93	88	0.2
A-4	0.03	402	1.35	97	89	0.17321
A-5	0.02	399	0.9	100	91	0.14142
A-6	0.01	397	0.45	102	93	0.1
A-7	0.005	355	0.24	100	97	0.07071
A-8	0.005	359	0.24	99	92	0.07071
B-1	0.01	340	0.45	99	97	0.1
B-2	0.005	398	0.24	101	99	0.07071
B-3	0.005	396	0.24	99	98	0.07071
B-4	0.005	396	0.24	100	99	0.07071
B-5	0.02	396	0.9	102	100	0.14142
B-6	0.02	391	0.9	105	102	0.14142
B-7	0.02	348	0.9	106	102	0.14142
B-8	0.02	350	0.9	107	102	0.14142
C-1	0.02	355	0.9	106	102	0.14142
C-2	0.03	391	1.35	106	103	0.17321
C-3	0.03	392	1.35	110	104	0.17321
C-4	0.03	391	1.35	110	105	0.17321
C-5	0.03	385	1.35	107	103	0.17321
C-6	0.02	383	0.9	109	105	0.14142
C-7	0.02	380	0.9	111	106	0.14142
C-8	0.01	349	0.45	111	107	0.1
Average		381.416667	0.875	102.375	98.1667	0.1319
					100.271	

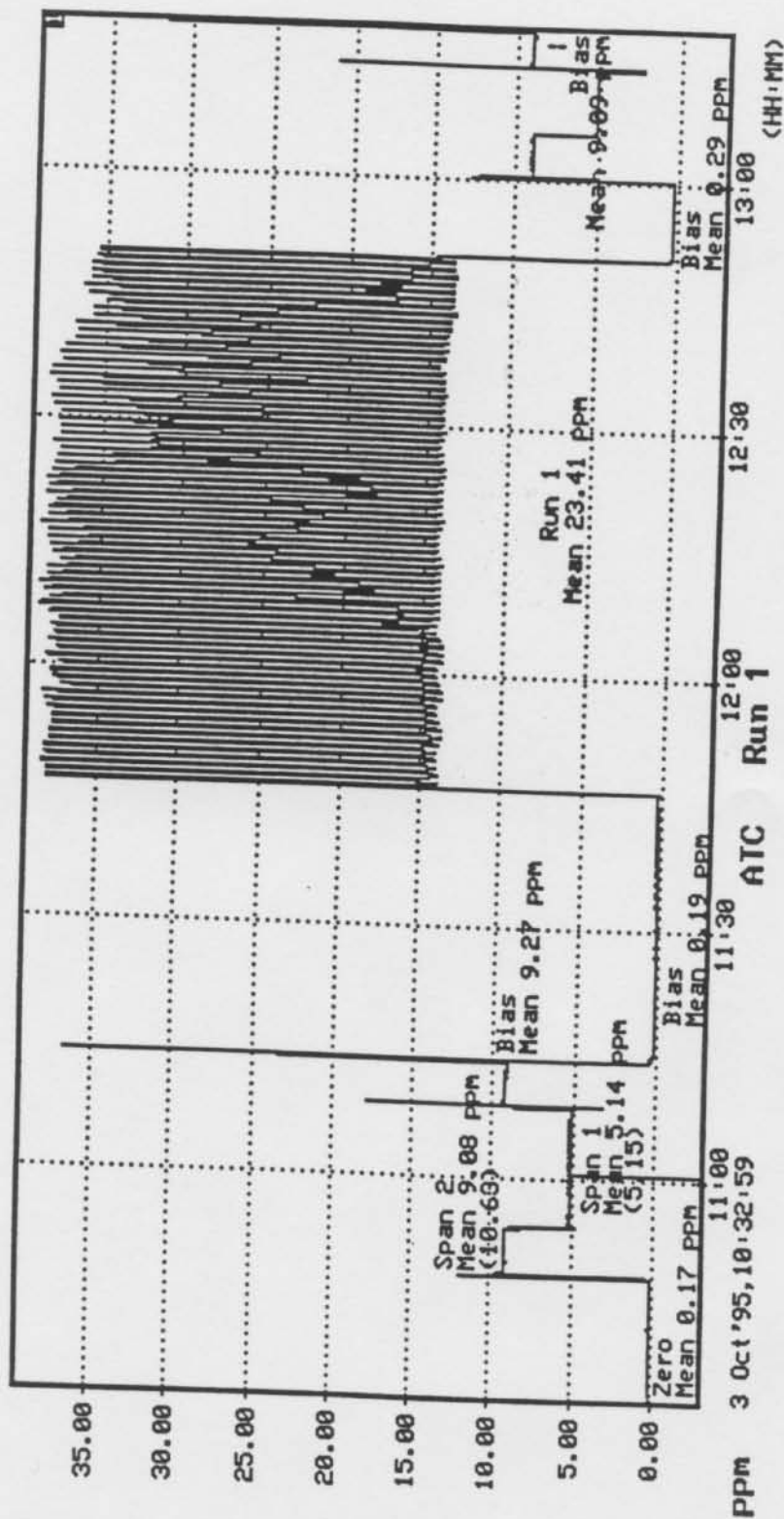
Sulfur Dioxide

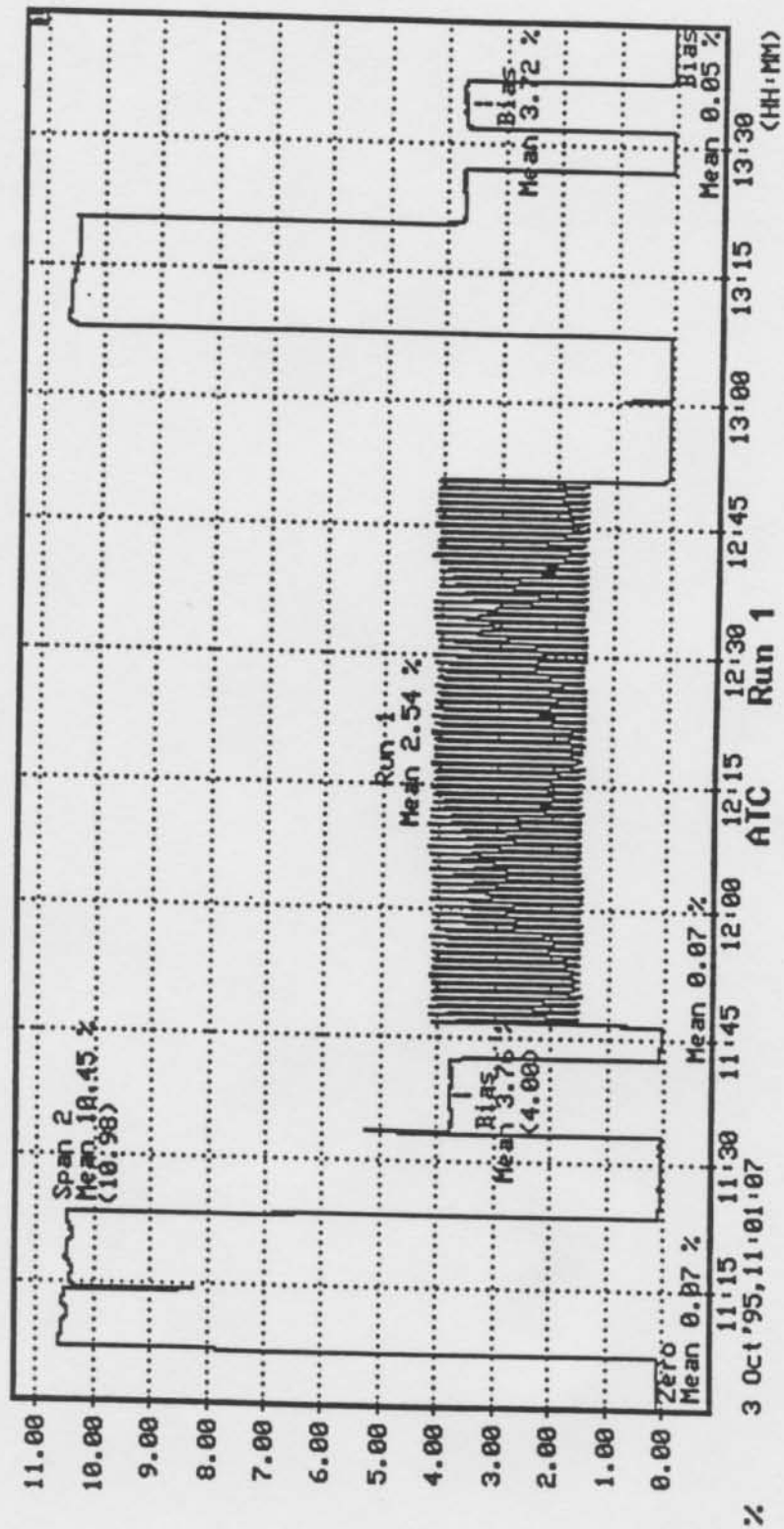


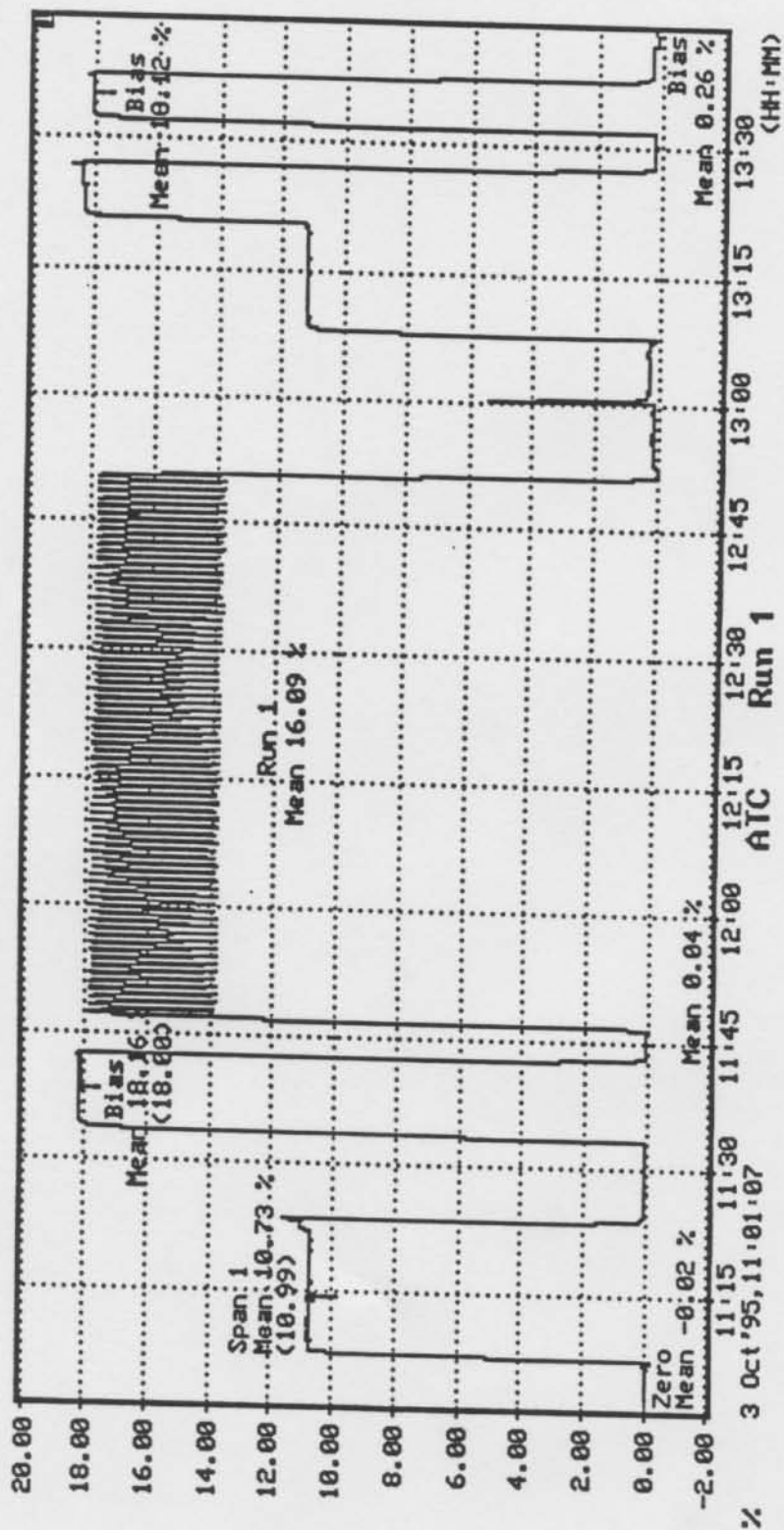
I H C



N O x







PES Inc.
Calculations for :

EPA Method 2,3a,4,6c,7E,10
and 25a

Plant	ATC Consultants - Balboa Pacific
Project #	5102
Operation	Pyrolytic Unit
Run	1
Load	Batch 1
Location	Santa Fe Springs, CA
Date	10/3/95

DATA INPUT

INPUT	Vic =	36.7 cc	Vol. of H2O collected
INPUT	Vm =	27.937 cf	Dry gas meter reading
INPUT	Pb =	29.80 in. Hg	Barometric pressure
INPUT	Pg =	-0.01 in. H2O	Static pressure
INPUT	dP =	0.106	Avg. sq.rt delta P
INPUT	dH =	0.540 in. H2O	Avg. delta H
INPUT	Tm =	546.0 R	Avg. meter temp.
INPUT	Ts =	897.0 R	Avg. stack temp.
INPUT	Y =	1.003	Meter calibration factor
INPUT	t =	72 min.	Duration of sampling time
INPUT	A =	2.3300 sq.ft.	Stack Area
INPUT	Cp =	0.84	Pitot tube coefficient
	Kp =	85.49	Pitot tube constant
	K1 =	17.64 R/in.Hg	constant
	K2 =	0.04707 cu.ft/ml	constant
	K3 =	0.002669 in.Hg-cf/ml	constant

Gas Analysis

INPUT	[O2] =	16.09	%(dry)
INPUT	[O2] =	0.04	initial zero bias
INPUT	[O2] =	0.26	final zero bias
	[O2] =	0.15	average zero bias
INPUT	[O2] =	18	midspan concentration
INPUT	[O2] =	18.16	initial midspan bias
INPUT	[O2] =	18.12	final midspan bias
	[O2] =	18.14	average midspan bias
INPUT	[CO2] =	2.54	%(dry)
INPUT	[CO2] =	0.07	initial zero bias
INPUT	[CO2] =	0.05	final zero bias
	[CO2] =	0.06	average zero bias
INPUT	[CO2] =	4	midspan concentration
INPUT	[CO2] =	3.88	initial midspan bias
INPUT	[CO2] =	3.72	final midspan bias
	[CO2] =	3.80	average midspan bias
	[O2] =	15.95	adjusted concentration
	[CO2] =	2.65	adjusted concentration
	[N2] =	81.4	%
INPUT	[CO] =	29.40	ppmV(dry)
INPUT	[CO] =	0.1	initial zero bias
INPUT	[CO] =	0.1	final zero bias
	[CO] =	0.10	average zero bias
INPUT	[CO] =	50	midspan concentration
INPUT	[CO] =	51	initial midspan bias
INPUT	[CO] =	40.8	final midspan bias
	[CO] =	45.9	average midspan bias
INPUT	[NOx] =	23.4	ppmV(dry)
INPUT	[NOx] =	0.19	initial zero bias
INPUT	[NOx] =	0.29	final zero bias
	[NOx] =	0.24	average zero bias
INPUT	[NOx] =	10.63	midspan concentration
INPUT	[NOx] =	9.27	initial midspan bias
INPUT	[NOx] =	9.09	final midspan bias
	[NOx] =	9.18	average midspan bias
INPUT	[THC] =	3.4	ppmV(wet)
INPUT	[THC] =	-0.15	initial zero bias
INPUT	[THC] =	-0.15	final zero bias
	[THC] =	-0.15	average zero bias
INPUT	[THC] =	48	midspan concentration
INPUT	[THC] =	47.18	initial midspan bias
INPUT	[THC] =	47.62	final midspan bias
	[THC] =	47.4	average midspan bias
INPUT	[SO2] =	0.5	ppmV(dry)
INPUT	[SO2] =	0.2	initial zero bias
INPUT	[SO2] =	-0.1	final zero bias
	[SO2] =	0.05	average zero bias
INPUT	[SO2] =	44.2	midspan concentration
INPUT	[SO2] =	44.3	initial midspan bias
INPUT	[SO2] =	44.5	final midspan bias
	[SO2] =	44.4	average midspan bias

[CO] =	31.99	ppmV(dry)	adj concentration
[NOx] =	27.55	ppmV(dry)	adj concentration
[THC] =	3.55	ppmV(wet)	adj concentration
[SO2] =	0.45	ppmV(dry)	adj concentration

CALCULATIONS

01) Volume of gas sampled at standard conditions, Vmstd

$$Vmstd = K1 \cdot Y \cdot Vm \cdot (Pb + dH/13.6)/Tm$$

Vmstd =	27.01	cu.ft
	0.77	cu.m

02) Volume of water vapor collected at standard conditions.

$$Vw(std) = K2 \cdot Vlc$$

Vw(std) =	1.73	scf
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03) Decimal fraction of moisture by volume in stack gas

$$Bws = Vwstd/(Vmstd + Vwstd)$$

Bws =	0.060
-------	-------

04) Molecular weight of the stack gas on a wet basis

$$Ms = (1-Q) \cdot ((44 \cdot \%CO_2) + (28 \cdot \%CO) + (32 \cdot \%O_2) + (28 \cdot \%N_2)) + (18 \cdot Q)$$

Ms =	28.39
------	-------

05) Average stack gas velocity.

Ps =	29.80	in. Hg
------	-------	--------

$$vs = Kp \cdot Cp \cdot (dP^{0.5}) \cdot (Ts/Ps \cdot Md)^{.5}$$

vs =	7.84	ft/sec
------	------	--------

06) Average actual stack gas volumetric flowrate.

$$Q = 60 \cdot vs \cdot As$$

Q =	1095.69	cfm
	31.03	cmm

07) Average stack gas dry volumetric flowrate.

$$Q_{std} = Q \cdot (T_{std}/T_s) \cdot (P_s/P_{std}) \cdot (1-Bws)$$

Qstd = 603.75 dscfm
 17.10 dscmm
 36225.23 dscfh

08) Emission Calculation - Carbon Monoxide

$$\text{lbs CO/hr} = ([\text{CO}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

[CO] =	31.99	ppmv (dry)	Actual conc.
[CO] =	0.08	Lbs/hr	

09) Emission Calculation - Nitrogen Oxides

$$\text{lbs NOx/hr} = ([\text{NOx}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

[NOx] =	27.6	ppmv (dry)	Actual Conc.
[NOx] =	0.12	Lbs/hr	

10) Emission Calculation - Total Hydrocarbons

$$\text{lbs THC/hr} = ([\text{THC}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

[THC] =	3.8	ppmv (dry)	Actual Conc.
[THC] =	0.02	Lbs/hr	

11) Emission Calculation - Sulfur Dioxide

$$\text{lbs NMHC/hr} = ([\text{NMHC}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

[SO2] =	0.4	ppmv (dry)	Actual Conc.
[SO2] =	0.02	Lbs/hr	

Plant ATC BALBOA PACIFIC
 Date 10-4-95
 Sampling Location EXHAUST STACK
 Sample Type EPA 5
 Run Number PE5/HTC2 AM 2
 Operator NEWMAN/BROWN
 Ambient Temperature 29.70
 Barometric Pressure 29.70
 Static Pressure -0.01
 Filter Number(s) 0.4429
 Pretest Leak Rate 0.014 CFM @ 6 in. Hg
 Read And Record All Data Every 3 Minutes

Probe Length and Type 3' Stainless Steel lined
 Pilot Tube I.D. No. 5-4A
 Nozzle I.D. No. And Diameter M2 0.494
 Assumed Moisture, % 2
 Meter Box Number 4A
 Meter Delta H @ 1.826
 C Factor 1.15
 Meter Gamma 1.005
 Heater Box Setting 250
 Reference Delta P 0.041
 Post test Leak Rate 0.008 CFM @ 3 in. Hg
 Impinger Box No. 5B Blank Box No. 3

Schematic of

Traverse Point Layout

Traverse Point Number	Sampling Time (minutes)	Clock Time (24 hr clock)	Gas Meter Reading V_m (cubic feet)	Velocity Head P_v (in. H2O)	Orifice Pressure Differential (in. H2O) ΔH		Stack Temp. T_s (F)	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
					Desired	Actual		Inlet T_m in (F)	Outlet T_m out (F)				
L8	0	10:15	750.685	0.03	1.35	✓	387	77	74	2.0	247	258	61
L7	3	10:16	752.621	0.03	1.35	✓	389	75	73	2.0	248	265	62
L6	6	10:21	754.449	0.03	1.35	✓	391	77	74	2.0	248	268	61
L5	9	10:24	756.289	0.03	1.35	✓	393	79	75	1.5	248	269	63
L4	12	10:27	758.195	0.03	1.35	✓	392	81	75	1.5	250	270	64
L3	15	10:30	759.907	0.02	0.90	✓	388	84	76	1.0	249	270	65
L2	18	10:33	761.590	0.01	0.45	✓	381	84	77	1.0	250	269	65
L1	21	10:36	762.981	0.01	0.45	✓	—	85	78	1.0	251	266	64
END/MS	24	10:37/10:43	763.959	0.02	0.90	✓	348	84	78	1.0	250	267	65
M7	27	10:46	765.528	0.02	0.90	✓	359	86	79	1.0	249	269	62
M6	30	10:49	767.127	0.02	0.90	✓	393	87	80	1.0	251	267	62
M5	33	10:52	768.731	0.02	0.90	✓	391	89	81	1.0	251	268	63
M4	36	10:55	770.325	0.02	0.90	✓	389	90	81	1.0	251	267	63
M3	39	10:58	771.952	0.02	0.90	✓	374	92	82	1.0	251	267	63
M2	42	11:01	773.409	0.01	0.45	✓	346	92	83	1.0	251	267	63
M1	45	11:04	774.780	0.01	0.45	✓	—	93	84	1.0	251	266	64
END/MS	48	11:07/11:09	775.359	0.02	0.90	✓	356	92	85	1.0	250	266	66
R7	51	11:12	777.518	0.02	0.90	✓	382	95	86	1.0	250	266	65
R6	54	11:15	779.120	0.02	0.90	✓	388	96	86	1.0	251	266	65
R5	57	11:18	780.756	0.02	0.90	✓	391	97	87	1.0	251	266	64
R4	60	11:21	782.371	0.02	0.90	✓	389	98	88	1.0	252	266	64
R3	63	11:24	783.972	0.02	0.90	✓	383	100	86	1.0	253	267	64
R2	66	11:27	785.569	0.01	0.45	✓	351	100	90	1.0	251	263	64
R1	69	11:30	786.777	0.01	0.45	✓	3—	100	91	1.0	250	263	64
END	72	11:33	787.932	—	—	—	—	100	91	1.0	250	263	64

0-72

 $V_m = 37.247$ $\Delta P = 0.138$ $\Delta H = 0.88$ $T_s = 378 + 460$ $T_m = 85 + 460$

= 545

0003 SAMPLE RETRIEVAL DATA

Plant: ATC-BALBOA
 Date: 10-3-95
 Sampling Location: _____
 Sampling Type (Method): PARTICULATE
 Run Number: PM2
 Sample Box Number: 58
 Clean-up Man: _____
 Job Number: _____
 Comments: _____

Filter

Filter Number: 0.4429
 Description of Filter: _____

Moisture

	#1	#2	#3
Impingers:			
Final Volume:	<u>676.2</u> mL	<u>600.3</u> mL	<u>485.3</u> mL
Initial Volume:	<u>588.7</u> mL	<u>591.6</u> mL	<u>484.7</u> mL
Net Volume:	<u>37.5</u> mL	<u>8.7</u> mL	<u>0.6</u> mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	<u>681.7</u> g	_____ g	_____ g
Initial Volume:	<u>473.4</u> g	_____ g	_____ g
Net Volume:	<u>4.3</u> g	_____ g	_____ g
Total Moisture:	_____ g	_____ g	_____ g

Description of Impinger catch: 55.1

PES Inc.

EPA Method 5 Calculations

Plant ATC - Balboa Pacific

Project # 5102

Operation Pyrolytic Waste Incinerator

Run 2 - Particulate - set 2

Location Santa Fe Springs, CA

Date 10/4/95

Emission Data

Vlc =	55.1	cc	Vol. of H2O collected (impingers)
Vm =	37.247	cf	Dry gas meter reading
Pb =	29.7	in. Hg	Barometric pressure
Ps =	29.70	in. Hg	Stack pressure
dP =	0.138		Average sq.rt delta P
dH =	0.880	in. H2O	Average draft gauge reading
Tm =	545.0	R	Average meter temperature
Ts =	838.00	R	Average stack temperature
Dn =	0.494	in.	Nozzle diameter
Y =	1.005		Meter calibration factor
t =	72	min.	Duration of sampling time
A =	2.3300	sq.ft.	Cross sectional area of stack
Cp =	0.84		Pitot tube coefficient
Kp =	85.49		Pitot tube constant
K1 =	17.64	R/in.Hg	constant
K2 =	0.04707	cu.ft/ml	constant
K3 =	0.002669	in.Hg-cf/ml-R	constant

1) Volume of gas sampled at standard conditions, Vmstd
 $Vmstd = K1 * Y * Vm * (Pb + dH/13.6) / Tm$

Vmstd = 36.06 cu.ft
1.02 cu.m

2) Volume of water vapor collected at standard conditions.

$Vw(std) = K2 * Vlc$

Vw(std) = 2.59 scf

3) Decimal fraction of moisture by volume in stack gas

$$Bws = Vwstd / (Vmstd + Vwstd)$$

$$Bws = 0.067$$

4) Molecular weight of the stack gas on a dry basis M_d .

$$Ms = ((44 * \%CO_2) + (28 * \%CO) + (32 * \%O_2) + (28 * \%N_2))$$

$$Ms = 29.08$$

Instrumental gas analysis

% CO ₂	2.71
% CO	0
% O ₂	16.05
% N ₂	81.24

5) Average stack gas velocity.

$$vs = Kp * Cp * (dP^{0.5}) * (Ts / Ps * Md)^{-0.5}$$

$$vs = 9.76 \text{ ft/sec}$$

6) Average actual stack gas volumetric flowrate.

$$Q = 60 * vs * As$$

$$Q = 1364.79 \text{ cfm}$$
$$38.65 \text{ cmm}$$

7) Average stack gas dry volumetric flowrate.

$$Qstd = Q * (Tstd / Ts) * (Ps / Pstd)$$

$$Qstd = 796.30 \text{ dscfm}$$
$$22.55 \text{ dscmm}$$

8) Analytical data

a) Front half acetone wash

0.0053 g wash net wt
0.0002 g acetone blank net wt
100 ml blank vol.
196 ml Final wash volume
196 ml aliquot

0.0053 g soluble particulate*

b) Front half glass microfibre filter

0.0006 g filter net wt

c) Back half water wash - soluble

0.0031 g net wt
0 g water blank net wt
220 ml blank vol
602.3 ml Final wash volume
602.3 ml aliquot

0.0031 g soluble net wt*

* Weights are not blank corrected

9) Particulate concentrations

0.0025 grains/dscf	Front 1/2
0.0039 grains/dscf	Total

11) Particulate emission rate

Conc. * (1 lb/7000 gr) * Qstd * 60 min/hr

W =	0.017 lbs/hr	Front 1/2
W =	0.026 lbs/hr	Total Particulate

12) Isokinecity

An = 0.001 ft² Area of nozzle orifice

$I = 100 \cdot T_s \cdot ((K_3 \cdot V_{lc} + (V_m \cdot Y / T_m) (P_b + dH / 13.6)) / (60 \cdot t \cdot P_s \cdot v_s \cdot A_n))$

$I = 110.16$

FIELD DATA

Plant ARC BALBOA PACIFIC
 Date 10-3-95
 Sampling Location EXHAUST STACK
 Sample Type EPA METHOD 12
 Run Number RES/1122 MM2
 Operator NEWMAN/MOKH
 Ambient Temperature 90
 Barometric Pressure 29.80
 Static Pressure + 0.04
 Filter Number(s) _____
 Pretest Leak Rate 0.001CFM @ 4 in. Hg
 Read And Record All Data Every 5 Minutes

Probe Length and Type 3' GLASS LINED
 Pitot Tube I.D. No. S-2A
 Nozzle I.D. No. And Diameter M4 0.504
 Assumed Moisture, % 2
 Meter Box Number 4A
 Meter Delta H@ 1.826
 C Factor 1.15
 Meter Gamma 1.005
 Heater Box Setting 250
 Reference Delta P $\Delta P_s = 0.041$
 Post test Leak Rate 0.001CFM @ 5 in. Hg
 Impinger Box No. 2B Blank Box No. _____

Schematic of
 Traverse Point Layout

Traverse Point Number	Sampling Time θ (minutes)	Clock Time (24 hr clock)	Gas Meter Reading V_m (cubic feet)	Velocity Head P_s (in. H2O)	Orifice Pressure Differential (in. H2O) ΔH		Stack Temp. T_s (F)	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
					Desired	Actual		Inlet T_m in (F)	Outlet T_m out (F)				
R9	0	14:15	674.576	0.005	0.24	✓	394	107	108	1.0	247	—	68
R7	5	14:20	676.190	0.02	0.96	✓	391	107	107	1.5	248	—	68
R6	10	14:25	679.010	0.01	0.45	✓	390	105	105	1.0	245	230	68
R5	15	14:30	681.045	0.005	0.24	✓	394	109	109	1.0	247	248	65
R4	20	14:35	682.568	0.003	1.35	✓	389	109	108	1.0	247	247	62
R3	25	14:40	684.040	0.02	1.35	✓	388	109	109	1.5	246	247	62
R2	30	14:45	686.700	0.04	1.80	✓	373	111	109	1.5	248	245	57
R1	35	14:50	689.900	0.04	1.35	✓	365	112	109	2.0	246	242	56
END/M9	40	14:55/14:58	693.511	0.03	1.35	✓	372	111	109	2.0	244	244	59
M7	45	15:01	696.801	0.03	1.35	✓	392	112	110	2.0	249	244	58
M6	50	15:06	700.051	0.03	1.35	✓	395	112	110	2.0	244	244	59
M5	55	15:11	703.901	0.02	1.35	✓	395	115	112	1.5	250	245	61
M4	60	15:16	706.400	0.04	1.80	✓	392	115	112	1.5	250	246	62
M3	65	15:21	709.090	0.04	1.80	✓	386	116	112	2.0	245	245	62
M2	70	15:26	712.710	0.04	1.80	✓	359	117	113	2.5	249	245	63
M1	75	15:31	716.620	0.05	2.25	✓	386	117	113	3.5	247	245	66
END/L8	80	15:36/15:38	720.293	0.05	2.25	✓	389	112	109	4.0	246	242	56
L7	85	15:43	725.189	0.05	1.80	✓	391	112	110	3.0	249	241	57
L6	90	15:49	728.471	0.04	1.80	✓	391	116	112	3.0	251	243	57
L5	95	15:53	732.618	0.04	1.80	✓	391	116	112	3.0	251	243	58
L4	100	15:58	736.390	0.04	1.80	✓	365	115	111	2.5	245	244	60
L3	105	16:03	740.061	0.03	1.35	✓	—	115	111	2.0	245	—	—
L2	110	16:08	743.770	0.03	1.35	✓	—	114	112	2.0	245	—	—
L1	115	16:13	747.002	0.03	—	—	—	—	—	—	—	—	—
END	120	16:19	750.235	—	—	—	—	—	—	—	—	—	—

SAMPLE RETRIEVAL DATA

Plant: ATC-BALBOA
 Date: 10-3-95
 Sampling Location: OUTLET
 Sampling Type (Method): M.M.
 Run Number: MM 2
 Sample Box Number: 2B
 Clean-up Man: MAKH
 Job Number: _____
 Comments: 521.8-60.1=
410.0-58.9=

Filter

Filter Number: _____
 Description of Filter: SLIGHTLY COLORED WITH SMALL BLACK PARTICLES
(LOOSE)

Moisture

Impingers:			
Final Volume:	<u>622.5</u> mL	<u>596.6</u> mL	<u>457.0</u> mL
Initial Volume:	<u>556.7</u> mL	<u>580.8</u> mL	<u>450.4</u> mL
Net Volume:	<u>65.8</u> mL	<u>15.8</u> mL	<u>3.6</u> mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	<u>733.5</u> g	_____ g	_____ g
Initial Volume:	<u>718.1</u> g	_____ g	_____ g
Net Volume:	<u>15.4</u> g	_____ g	_____ g
Total Moisture:	<u>100.6</u> g	_____ g	_____ g

Description of Impinger catch: CLEAR

PES, Inc.
Multi-Metals Method Calculations (EPA 12)

Plant ATC-Balboa Pacific

Project # 5102

Operation Pyrolytic Oxidation Unit

Run 2

Location Outlet

Date 10/3/95

Test Data

Vlc =	100.6 cc	Vol. of H2O collected (impingers)
Vm =	75.659 cf	Dry gas meter reading
Pb =	29.85 in. Hg	Barometric pressure
Ps =	29.85 in. Hg	Stack pressure
dP =	0.169	Average sq.rt delta P
dH =	1.383 in. H2O	Average draft gauge reading
Tm =	571.1 R	Average meter temperature
Ts =	842.63 R	Average stack temperature
Dn =	0.504 in.	Nozzle diameter
Y =	1.005	Meter calibration factor
t =	120 min.	Duration of sampling time
A =	2.3300 sq.ft.	Cross sectional area of stack
Cp =	0.84	Pitot tube coefficient
Kp =	85.49	Pitot tube constant
K1 =	17.64 R/in.Hg	constant
K2 =	0.04707 cu.ft/ml	constant
K3 =	0.002669 in.Hg-cf/ml	constant

Instrumentation Data

[O2] = 16.1 %
[CO2] = 2.7 %

CALCULATIONS

1) Volume of gas sampled at standard conditions, Vmstd

$$Vmstd = K1 * Y * Vm * (Pb + dH/13.6) / Tm$$

Vmstd = 70.34 cu.ft
1.99 cu.m

2) Volume of water vapor collected at standard conditions.
 $Vw(std) = K2 * Vlc$

$Vw(std) = 4.74 \text{ scf}$

3) Decimal fraction of moisture by volume in stack gas
 $Bws = Vwstd / (Vmstd + Vwstd)$

$Bws = 0.063$

4) Molecular weight of the stack gas on a dry basis Md .
 $Md = (1 - Bws) * ((44 * \%CO2) + (28 * \%CO) + (32 * \%O2) + (28 * \%N2)) + (18 * Bws)$

$Md = 28.38$

5) Average stack gas velocity.
 $vs = Kp * Cp * (dP^{0.5}) * (Ts / Ps * Md)^{.5}$

$vs = 12.09 \text{ ft/sec}$

6) Average actual stack gas volumetric flowrate.
 $Q = 60 * vs * As$

$Q = 1690.21 \text{ cfm}$
 47.87 cmm

7) Average stack gas dry volumetric flowrate.
 $Qstd = Q * (Tstd / Ts) * (Ps / Pstd)$

$Qstd = 990.08 \text{ dscfm}$
 28.04 dscmm

8) Toxic metal concentrations and emission rates

Element	Sample Mass (ug)	Blank Mass (ug) DL	Conc. (mg/dscm)	Emission Rate (mg/hr)
Copper	9.00	1.00	3.21E-04	5.4E-01
Chromium	6.00	6.00	2.14E-04	3.6E-01
Lead	7.50	0.10	2.67E-04	4.5E-01
Zinc	65.00	9.00	2.32E-03	3.9E+00
Manganese	4.00	4.00	1.43E-04	2.4E-01
Nickel	9.00	9.00	3.21E-04	5.4E-01
Cadmium	3.00	1.00	1.07E-04	1.8E-01
Beryllium	1.00	1.00	3.57E-05	6.0E-02
Arsenic	0.10	0.10	3.57E-06	6.0E-03
Selenium	10.00	10.00	3.57E-04	6.0E-01
Molybdenum	592.00	2.00	2.11E-02	3.6E+01
Silver	0.10	0.10	3.57E-06	6.0E-03
Antimony	2.00	2.00	7.13E-05	1.2E-01
Barium	3.00	1.00	1.07E-04	1.8E-01
Thallium	0.20	0.20	7.13E-06	1.2E-02

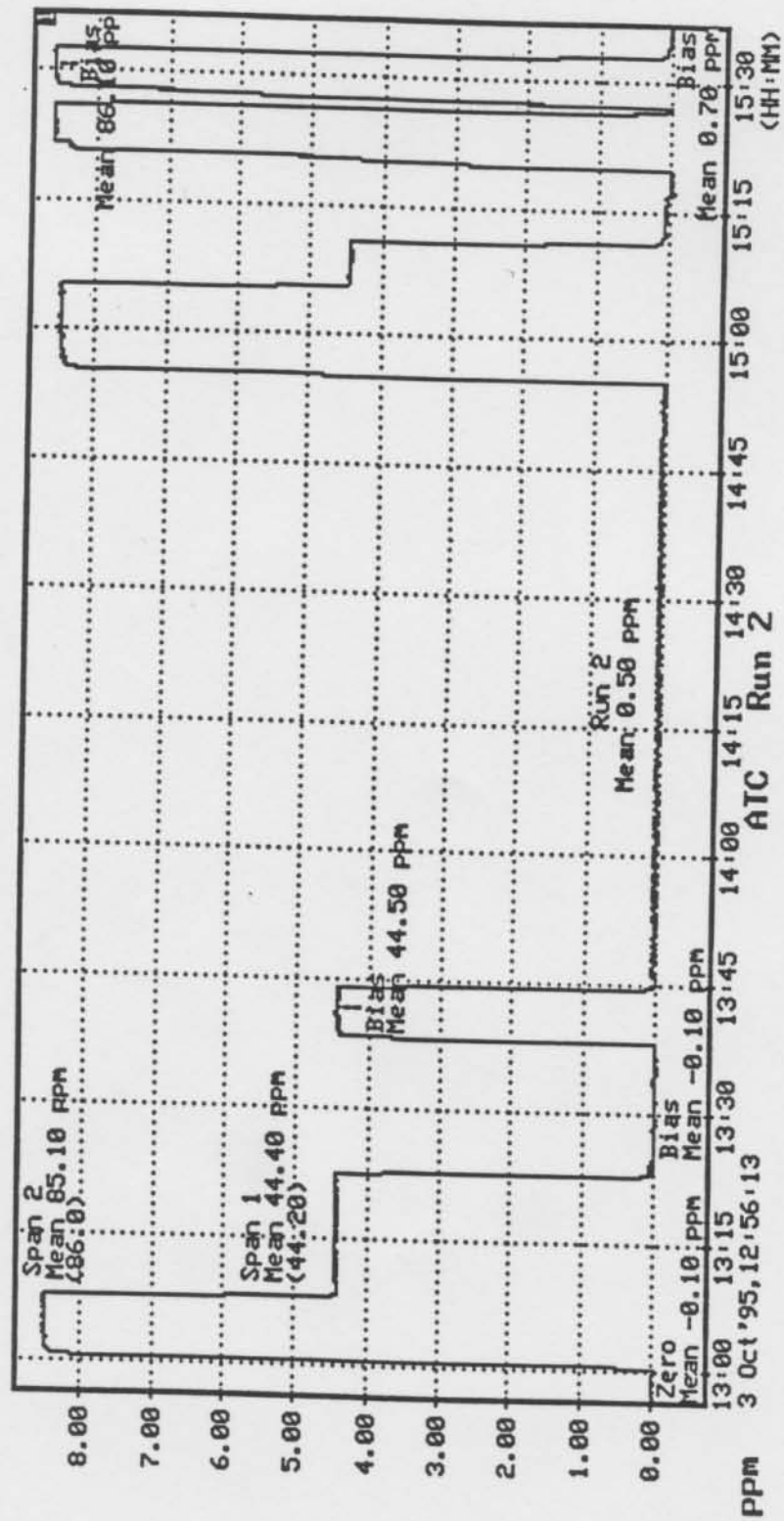
9) Isokinecity

$A_n = 0.001 \text{ ft}^2$ Area of nozzle orifice
 $\% I = 100 \cdot T_s \cdot ((K_3 \cdot V_{lc} + (V_m \cdot Y / T_m) (P_b + dH / 13.6)) / (60 \cdot t \cdot P_s \cdot v_s \cdot A_n))$
 $\% I = 99.61$

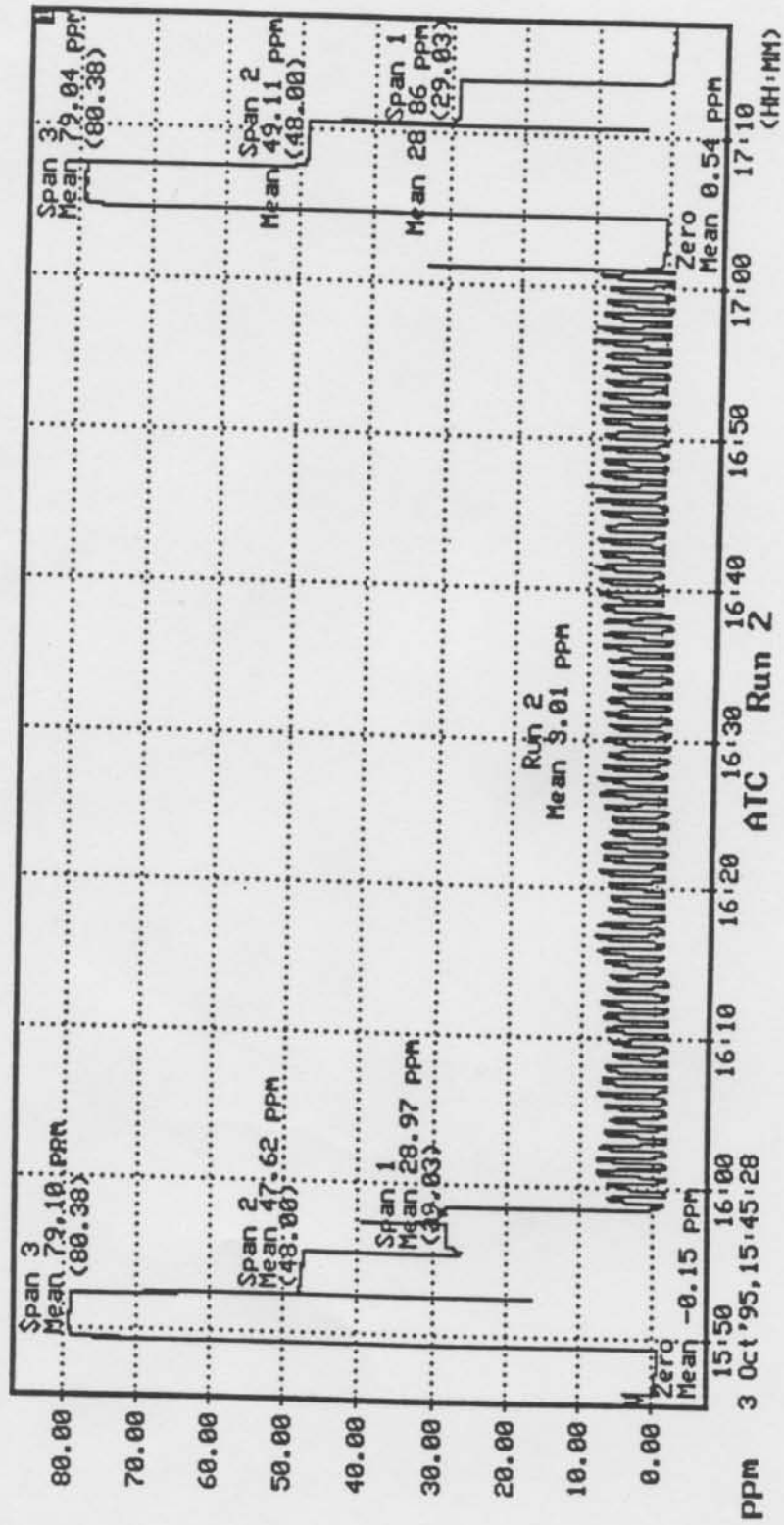
Sample Train Operation Data
 Test Date 10/3/95
 Barometer 29.85 in.Hg
 Run # 2
 Static P 0.04 in.H2O
 Pitot Cp 0.84
 Nozzle 0.504

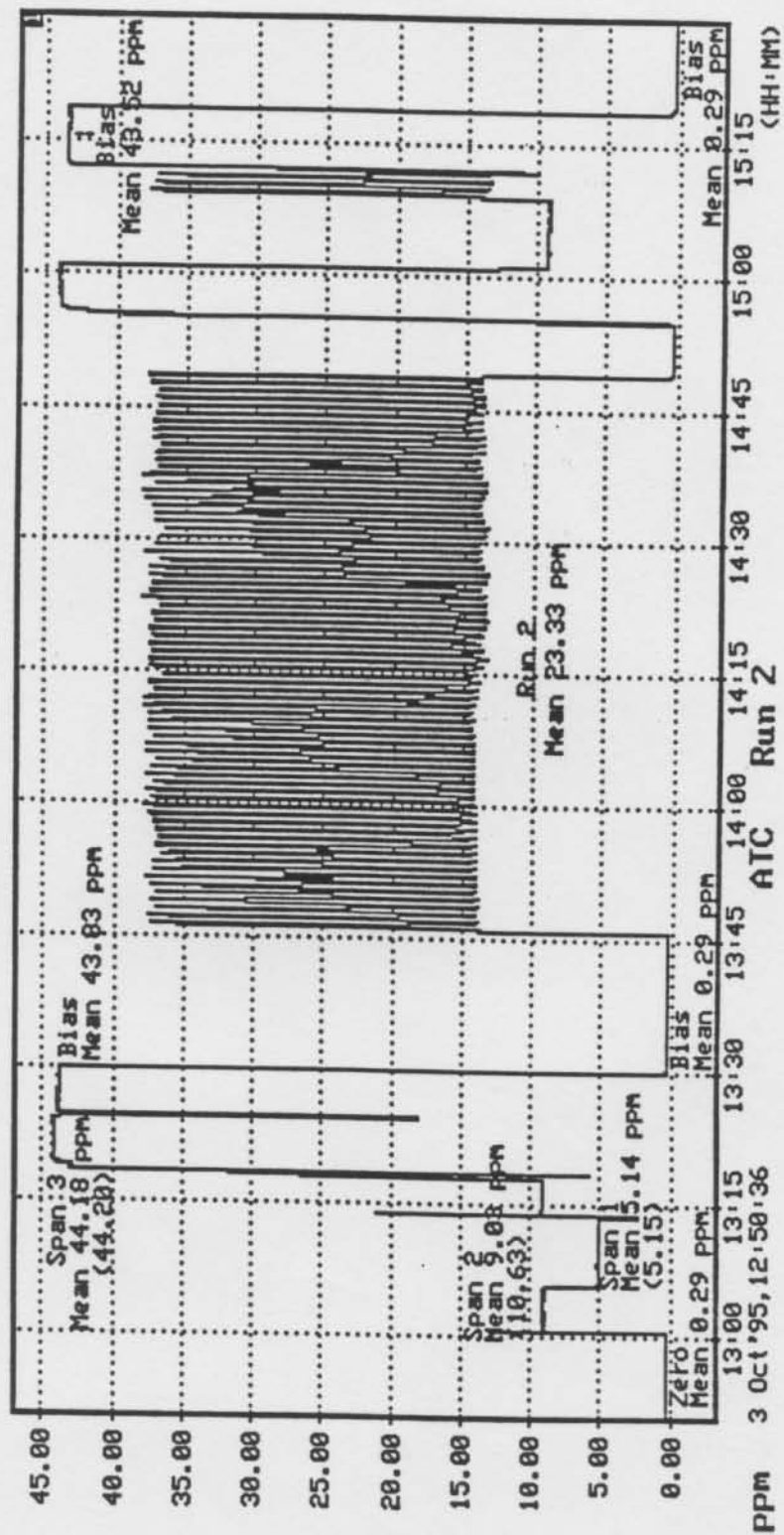
Traverse Point	Delta-P (in. H2O)	Temp. (Deg.F)	delta H	Dry Gas Meter Temp IN	Temp OUT	(dP) ^{0.5}
A-1	0.005	394	0.24	107	108	0.07071
A-2	0.02	391	0.96	107	107	0.14142
A-3	0.01	390	0.45	105	105	0.1
A-4	0.005	394	0.24	109	109	0.07071
A-5	0.005	389	0.24	109	108	0.07071
A-6	0.03	388	1.35	109	109	0.17321
A-7	0.03	373	1.35	111	109	0.17321
A-8	0.04	365	1.8	112	109	0.2
B-1	0.03	377	1.35	111	109	0.17321
B-2	0.03	392	1.35	112	110	0.17321
B-3	0.03	395	1.35	112	110	0.17321
B-4	0.02	395	0.9	115	112	0.14142
B-5	0.03	392	1.35	115	112	0.17321
B-6	0.04	386	1.8	115	112	0.2
B-7	0.04	367	1.8	116	112	0.2
B-8	0.04	359	1.8	117	113	0.2
C-1	0.05	374	2.25	112	112	0.22361
C-2	0.05	388	2.25	111	109	0.22361
C-3	0.05	389	2.25	112	110	0.22361
C-4	0.04	391	1.8	116	112	0.2
C-5	0.04	391	1.8	116	112	0.2
C-6	0.04	389	1.8	115	110	0.2
C-7	0.03	365	1.35	115	111	0.17321
C-8	0.03	349	1.35	114	112	0.17321
Average		382.625	1.3825	112.20833	110.083	0.16881
					111.146	

Sulfur Dioxide



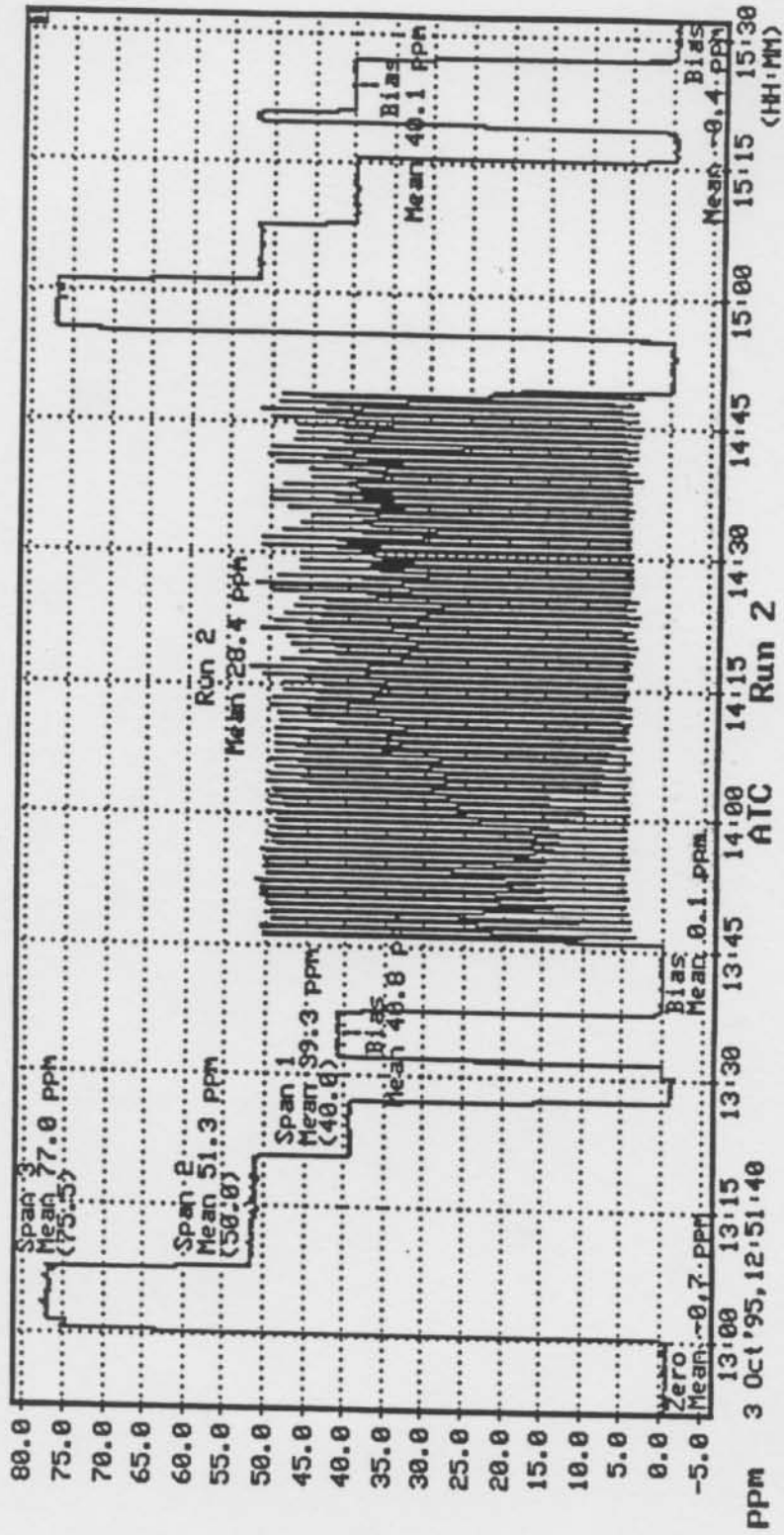
T H C





NOx

Carbon Monoxide



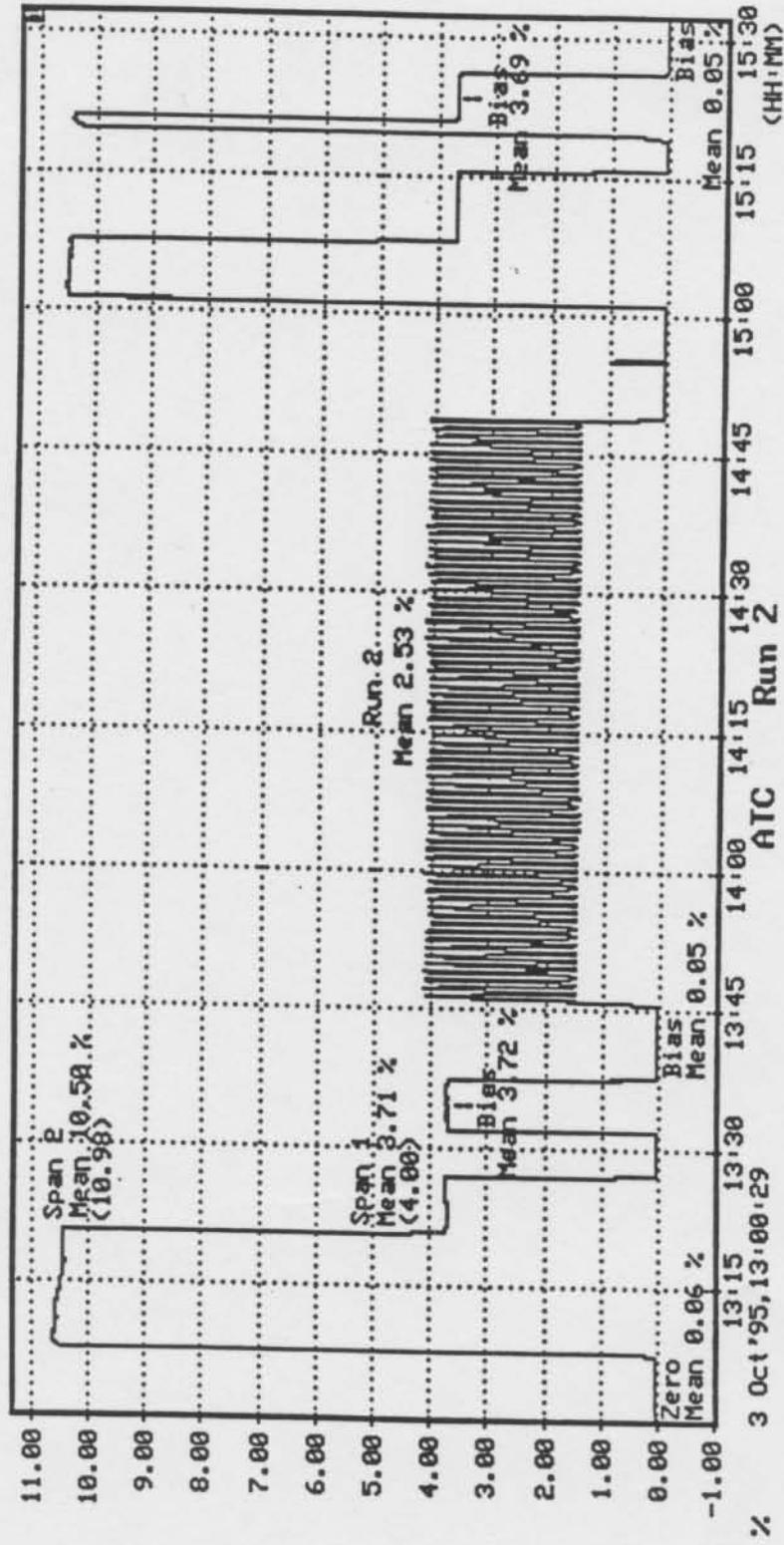
ppm 3 Oct '95, 12:51:40

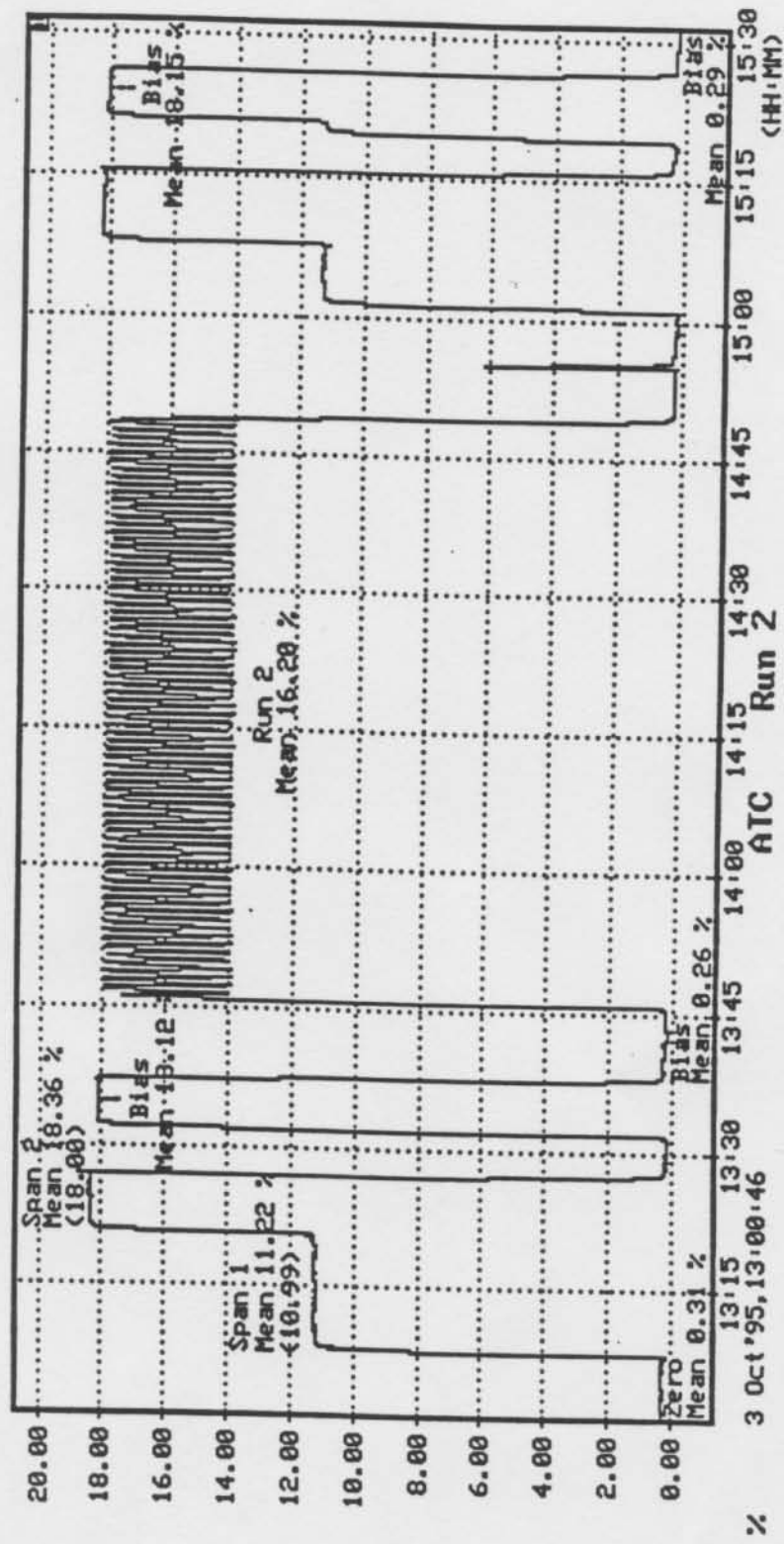
ATC

Run 2

(HH:MM)

Carbon Dioxide





oxygen

PES Inc.
Calculations for :

EPA Method 2,3a,4,6c,7E,10
and 25a

Plant	ATC Consultants - Balboa Pacific
Project #	5102
Operation	Pyrolytic Unit
Run	2
Load	Batch 2
Location	Santa Fe Springs, CA
Date	10/4/95

DATA INPUT

INPUT	Vic =	55.1 cc	Vol. of H2O collected
INPUT	Vm =	37.247 cf	Dry gas meter reading
INPUT	Pb =	29.70 in. Hg	Barometric pressure
INPUT	Pg =	-0.01 in. H2O	Static pressure
INPUT	dP =	0.138	Avg. sq.rt delta P
INPUT	dH =	0.880 in. H2O	Avg. delta H
INPUT	Tm =	545.0 R	Avg. meter temp.
INPUT	Ts =	838.0 R	Avg. stack temp.
INPUT	Y =	1.005	Meter calibration factor
INPUT	t =	72 min.	Duration of sampling time
INPUT	A =	2.3300 sq.ft.	Stack Area
INPUT	Cp =	0.84	Pitot tube coefficient
	Kp =	85.49	Pitot tube constant
	K1 =	17.64 R/in.Hg	constant
	K2 =	0.04707 cu.ft/ml	constant
	K3 =	0.002669 in.Hg-cf/ml	constant

	Gas Analysis	
INPUT	[O2] =	16.20 %(dry)
INPUT	[O2] =	0.26 initial zero bias
INPUT	[O2] =	0.29 final zero bias
	[O2] =	0.28 average zero bias
INPUT	[O2] =	18 midspan concentration
INPUT	[O2] =	18.12 initial midspan bias
INPUT	[O2] =	18.15 final midspan bias
	[O2] =	18.135 average midspan bias
INPUT	[CO2] =	2.53 %(dry)
INPUT	[CO2] =	0.05 initial zero bias
INPUT	[CO2] =	0.05 final zero bias
	[CO2] =	0.05 average zero bias
INPUT	[CO2] =	4 midspan concentration
INPUT	[CO2] =	3.72 initial midspan bias
INPUT	[CO2] =	3.69 final midspan bias
	[CO2] =	3.71 average midspan bias
	[O2] =	16.05 adjusted concentration
	[CO2] =	2.71 adjusted concentration
	[N2] =	81.2 %
INPUT	[CO] =	28.40 ppmV(dry)
INPUT	[CO] =	0.1 initial zero bias
INPUT	[CO] =	-0.4 final zero bias
	[CO] =	-0.15 average zero bias
INPUT	[CO] =	40 midspan concentration
INPUT	[CO] =	40.8 initial midspan bias
INPUT	[CO] =	40.1 final midspan bias
	[CO] =	40.45 average midspan bias
INPUT	[NOx] =	23.3 ppmV(dry)
INPUT	[NOx] =	0.29 initial zero bias
INPUT	[NOx] =	0.29 final zero bias
	[NOx] =	0.29 average zero bias
INPUT	[NOx] =	44.2 midspan concentration
INPUT	[NOx] =	43.83 initial midspan bias
INPUT	[NOx] =	43.52 final midspan bias
	[NOx] =	43.675 average midspan bias
INPUT	[THC] =	3.0 ppmV(wet)
INPUT	[THC] =	-0.15 initial zero bias
INPUT	[THC] =	0.54 final zero bias
	[THC] =	0.20 average zero bias
INPUT	[THC] =	48 midspan concentration
INPUT	[THC] =	47.62 initial midspan bias
INPUT	[THC] =	49.11 final midspan bias
	[THC] =	48.365 average midspan bias
INPUT	[SO2] =	0.5 ppmV(dry)
INPUT	[SO2] =	-0.1 initial zero bias
INPUT	[SO2] =	0.7 final zero bias
	[SO2] =	0.30 average zero bias
INPUT	[SO2] =	44.2 midspan concentration
INPUT	[SO2] =	44.5 initial midspan bias
INPUT	[SO2] =	86.1 final midspan bias
	[SO2] =	65.3 average midspan bias

[CO] =	28.13 ppmV(dry) adj concentration
[NOx] =	23.47 ppmV(dry) adj concentration
[THC] =	2.81 ppmV(wet) adj concentration
[SO2] =	0.14 ppmV(dry) adj concentration

CALCULATIONS

01) Volume of gas sampled at standard conditions, Vmstd

$$Vmstd = K1 \cdot Y \cdot Vm \cdot (Pb + dH/13.6)/Tm$$

Vmstd = 36.06 cu.ft
 1.02 cu.m

02) Volume of water vapor collected at standard conditions.

$$Vw(std) = K2 \cdot Vlc$$

Vw(std) = 2.59 scf

03) Decimal fraction of moisture by volume in stack gas

$$Bws = Vwstd/(Vmstd + Vwstd)$$

Bws = 0.067

04) Molecular weight of the stack gas on a wet basis

$$Ms = (1-Q) \cdot ((44 \cdot \%CO_2) + (28 \cdot \%CO) + (32 \cdot \%O_2) + (28 \cdot \%N_2)) + (18 \cdot Q)$$

Ms = 28.30

05) Average stack gas velocity.

Ps = 29.70 in. Hg

$$vs = Kp \cdot Cp \cdot (dP^{0.5}) \cdot (Ts/Ps \cdot Md)^{.5}$$

vs = 9.89 ft/sec

06) Average actual stack gas volumetric flowrate.

$$Q = 60 \cdot vs \cdot As$$

Q = 1383.31 cfm
 39.18 cmm

07) Average stack gas dry volumetric flowrate.

$$Q_{std} = Q \cdot (T_{std}/T_s) \cdot (P_s/P_{std}) \cdot (1-Bws)$$

Qstd =
807.11 dscfm
22.86 dscmm
48426.43 dscfh

08) Emission Calculation - Carbon Monoxide

$$\text{lbs CO/hr} = ([\text{CO}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

[CO] =	28.13	ppmv (dry)	Actual conc.
[CO] =	0.10	Lbs/hr	

09) Emission Calculation - Nitrogen Oxides

$$\text{lbs NOx/hr} = ([\text{NOx}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

[NOx] =	23.5	ppmv (dry)	Actual Conc.
[NOx] =	0.14	Lbs/hr	

10) Emission Calculation - Total Hydrocarbons

$$\text{lbs THC/hr} = ([\text{THC}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

[THC] =	3.0	ppmv (dry)	Actual Conc.
[THC] =	0.02	Lbs/hr	

11) Emission Calculation - Sulfur Dioxide

$$\text{lbs NMHC/hr} = ([\text{NMHC}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

[SO2] =	0.1	ppmv (dry)	Actual Conc.
[SO2] =	0.02	Lbs/hr	

FIELD DATA

Plant ATC BALBET PLANT
 Date 10-4-95
 Sampling Location EXHAUST STACK
 Sample Type EPA METHOD 5
 Run Number PES/ATC2 PM3
 Operator NEWMAN/BROWN
 Ambient Temperature 90
 Barometric Pressure 29.70
 Static Pressure 2.03
 Filter Number(s) 0.4490
 Pretest Leak Rate 0.016 CFM @ 5 in. Hg
 Read And Record All Data Every 3 Minutes

Probe Length and Type 3' - SS LINED
 Pitot Tube I.D. No. 54A
 Nozzle I.D. No. And Diameter M2 0.494
 Assumed Moisture, % 2
 Meter Box Number 44
 Meter Delta H @ 1.826
 C Factor 1.15
 Meter Gamma 1.005
 Heater Box Setting 250
 Reference Delta P $\Delta P_a = 0.041$
 Post test Leak Rate 0.020 CFM @ 3 in. Hg
 Impinger Box No. 7B Blank Box No. —

Schematic of
Traverse Point Layout

Traverse Point Number	Sampling Time Θ (minutes)	Clock Time (24 hr clock)	Gas Meter Reading V_m (cubic feet)	Velocity Head P_s (in. H2O)	Orifice Pressure Differential (in. H2O) ΔH		Stack Temp. T_s (F)	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
					Desired	Actual		Inlet T_m in (F)	Outlet T_m out (F)				
L8	0	14:56	851.472	0.03	1.35	✓	381	109	108	2.0	247	236	68
L7	3	14:59	853.363	0.03	1.35	✓	382	109	108	2.0	248	249	68
L6	6	15:02	855.244	0.03	1.35	✓	382	111	109	2.0	248	251	65
L5	9	15:05	857.159	0.03	1.35	✓	382	112	109	2.0	250	250	65
L4	12	15:08	859.061	0.03	1.35	✓	382	114	109	2.0	250	250	65
L3	15	15:11	860.960	0.03	1.35	✓	385	115	110	2.0	250	248	65
L2	18	15:14	862.863	0.03	1.35	✓	387	116	110	2.0	252	246	68
L1	21	15:17	864.768	0.03	1.35	✓	387	116	110	2.0	252	247	68
DATA	24	15:20/15:22	866.646	0.03	1.35	✓	389	116	111	2.0	249	247	65
M7	27	15:25	868.532	0.03	1.35	✓	389	117	111	2.0	249	248	65
M6	30	15:28	870.399	0.02	0.90	✓	392	117	111	1.5	250	245	68
M5	33	15:31	872.180	0.02	0.90	✓	390	118	112	1.5	249	246	68
M4	36	15:34	873.712	0.02	0.90	✓	388	118	112	1.5	249	247	67
M3	39	15:37	875.340	0.02	0.90	✓	383	119	113	1.5	250	247	65
M2	42	15:40	876.464	0.02	0.90	✓	387	118	113	1.5	250	246	62
M1	45	15:43	878.624	0.02	0.90	✓	387	119	113	1.5	250	246	62
DATA	48	15:46/15:50	880.252	0.03	1.35	✓	389	116	113	2.0	250	246	67
R7	51	15:53	882.123	0.03	1.35	✓	389	118	113	2.0	248	246	67
R6	54	15:56	883.949	0.03	1.35	✓	390	118	113	2.0	250	247	62
R5	57	15:59	885.891	0.03	1.35	✓	390	120	114	2.0	250	246	62
R4	60	16:02	887.782	0.03	1.35	✓	388	120	114	2.0	251	246	63
R3	63	16:05	889.688	0.03	1.35	✓	383	120	114	2.0	251	247	62
R2	66	16:08	891.616	0.03	1.35	✓	376	120	114	2.0	250	245	62
R1	69	16:11	893.517	0.03	1.35	✓	341	121	114	2.0	250	245	64
END	72	16:14	895.412	—	—	—	—	—	—	—	—	—	—

$$V_m = 43.94 \quad \sqrt{\Delta P} = 0.165 \quad \Delta H = 1.24 \quad T_m = 114 \quad 1460$$

$$0.72 \quad 2.924 \quad = 5.74$$

SAMPLE RETRIEVAL DATA

Plant: A7C BALBOA
 Date: 10-4-95
 Sampling Location: _____
 Sampling Type (Method): PARTICULATE
 Run Number: PM3
 Sample Box Number: 7B
 Clean-up Man: _____
 Job Number: _____
 Comments: _____

Filter

Filter Number: 0.4490
 Description of Filter: LT. GREEN

Moisture

	#1	#2	#3
Impingers:			
Final Volume:	<u>612.2</u> mL	<u>625.6</u> mL	<u>500.5</u> mL
Initial Volume:	<u>582.8</u> mL	<u>604.2</u> mL	<u>499.5</u> mL
Net Volume:	<u>29.4</u> mL	<u>21.4</u> mL	<u>1.0</u> mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	<u>668.2</u> g	_____ g	_____ g
Initial Volume:	<u>659.7</u> g	_____ g	_____ g
Net Volume:	<u>8.5</u> g	_____ g	_____ g
Total Moisture:	_____ g	_____ g	_____ g

Description of Impinger catch: 60.3
CLEAR

PES Inc.

EPA Method 5 Calculations

Plant ATC - Balboa Pacific

Project # 5102

Operation Pyrolytic Waste Incinerator

Run 3 - Particulate - set 2

Location Santa Fe Springs, CA

Date 10/4/95

Emission Data

Vlc =	60.3	cc	Vol. of H2O collected (impingers)
Vm =	43.94	cf	Dry gas meter reading
Pb =	29.7	in. Hg	Barometric pressure
Ps =	29.70	in. Hg	Stack pressure
dP =	0.165		Average sq.rt delta P
dH =	1.240	in. H2O	Average draft gauge reading
Tm =	574.0	R	Average meter temperature
Ts =	839.00	R	Average stack temperature
Dn =	0.494	in.	Nozzle diameter
Y =	1.005		Meter calibration factor
t =	72	min.	Duration of sampling time
A =	2.3300	sq.ft.	Cross sectional area of stack
Cp =	0.84		Pitot tube coefficient
Kp =	85.49		Pitot tube constant
K1 =	17.64	R/in.Hg	constant
K2 =	0.04707	cu.ft/ml	constant
K3 =	0.002669	in.Hg-cf/ml-R	constant

1) Volume of gas sampled at standard conditions, Vmstd
 $Vmstd = K1 * Y * Vm * (Pb + dH/13.6) / Tm$

Vmstd = 40.43 cu.ft
 1.14 cu.m

2) Volume of water vapor collected at standard conditions.

$Vw(std) = K2 * Vlc$

Vw(std) = 2.84 scf

3) Decimal fraction of moisture by volume in stack gas

$$Bws = Vwstd / (Vmstd + Vwstd)$$

$$Bws = 0.066$$

4) Molecular weight of the stack gas on a dry basis M_d .

$$Ms = ((44 * \%CO_2) + (28 * \%CO) + (32 * \%O_2) + (28 * \%N_2))$$

$$Ms = 29.08$$

Instrumental gas analysis

% CO ₂	2.73
% CO	0
% O ₂	16.04
% N ₂	81.23

5) Average stack gas velocity.

$$vs = Kp * Cp * (dP^{0.5}) * (Ts / Ps * Md)^{.5}$$

$$vs = 11.68 \text{ ft/sec}$$

6) Average actual stack gas volumetric flowrate.

$$Q = 60 * vs * As$$

$$Q = \begin{array}{ll} 1632.75 & \text{cfm} \\ 46.24 & \text{cm}^3/\text{min} \end{array}$$

7) Average stack gas dry volumetric flowrate.

$$Qstd = Q * (Tstd / Ts) * (Ps / Pstd)$$

$$Qstd = \begin{array}{ll} 952.99 & \text{dscfm} \\ 26.99 & \text{dscmm} \end{array}$$

8) Analytical data

a) Front half acetone wash

0.0005 g wash net wt
0.0002 g acetone blank net wt
100 ml blank vol.
175 ml Final wash volume
175 ml aliquot

0.0005 g soluble particulate*

b) Front half glass microfibre filter

0.0042 g filter net wt

c) Back half water wash - soluble

0.0009 g net wt
0 g water blank net wt
220 ml blank vol
550 ml Final wash volume
550 ml aliquot

0.0009 g soluble net wt*

* Weights are not blank corrected

9) Particulate concentrations

0.0018 grains/dscf	Front 1/2
0.0021 grains/dscf	Total

11) Particulate emission rate

Conc. * (1 lb/7000 gr) * Qstd * 60 min/hr

W =	0.015 lbs/hr	Front 1/2
W =	0.017 lbs/hr	Total Particulate

12) Isokineticity

An = 0.001 ft² Area of nozzle orifice

$\% I = 100 * Ts * ((K3 * Vlc + (Vm * Y / Tm) (Pb + dH / 13.6))) / (60 * t * Ps * vs * An)$

$\% I = 103.19$

FIELD DATA

Plant ATC BALBOA PACIFIC
 Date 10-11-95
 Sampling Location EXHAUST STACK
 Sample Type EXHAUST STACK
 Run Number PES/ATC 2 MM3
 Operator NEWMAN/BROWN
 Ambient Temperature 90
 Barometric Pressure 29.70
 Static Pressure -0.02
 Filter Number(s)

Pretest Leak Rate 0.020 CFM @ -4 in. Hg
 Read And Record All Data Every 5 Minutes

Probe Length and Type 3' GLASS LINED
 Pitot Tube I.D. No. 3-24
 Nozzle I.D. No. And Diameter M4 0.504
 Assumed Moisture, % 2
 Meter Box Number 4A
 Meter Delta H @ 1.826
 C Factor 1.15
 Meter Gamma 1.005
 Heater Box Setting 4 250
 Reference Delta P 0.025 CFM @ 2 in. Hg
 Post test Leak Rate 0.025 CFM @ 2 in. Hg
 Impinger Box No. 8B Blank Box No.

Schematic of
Traverse Point Layout

Traverse Point Number	Sampling Time (minutes)	Clock Time (24 hr clock)	Gas Meter Reading V_m (cubic feet)	Velocity Head P_v (in. H ₂ O)	Orifice Pressure Differential (in. H ₂ O)		Stack Temp. T_s (F)	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)	Heated Probe Temp. (F)	Filter Box Temp. (F)	Impinger Temp. (F)
					Desired	Actual		Inlet T_m (F)	Outlet T_m (F)				
R 6	0	12:20	719.384	0.03	1.35	✓	363	98	95	8.0	225	262	68
R 7	5	12:25	748.459	0.03	1.35	✓	395	102	97	2.0	248	266	68
R 8	10	12:30	795.500	0.02	0.90	✓	326	105	98	1.5	245	262	66
R 9	15	12:35	798.260	0.02	0.90	✓	394	107	99	1.5	246	259	63
R 4	20	12:40	800.920	0.02	0.90	✓	391	107	100	1.5	249	257	61
R 3	25	12:45	803.157	0.02	0.90	✓	387	108	100	1.5	245	257	60
R 2	30	12:50	806.289	0.02	0.90	✓	280	108	100	1.5	247	258	60
R 1	35	12:55	805.978	0.01	0.45	✓	305	109	102	1.0	245	256	62
END	40	1:00/13:01	811.023	0.02	0.90	✓	318	107	102	1.5	246	256	68
M 7	45	13:06	812.625	0.02	0.90	✓	397	109	103	1.5	249	257	63
M 6	50	13:11	816.349	0.02	0.90	✓	395	110	103	1.5	249	256	64
M 5	55	13:16	821.731	0.02	0.90	✓	347	111	104	1.5	248	255	64
M 4	60	13:21	821.731	0.01	0.45	✓	392	112	105	1.0	248	255	67
M 3	65	13:24	823.666	0.01	0.45	✓	378	111	106	1.0	250	254	67
M 2	70	13:31	823.510	0.01	0.45	✓	343	111	105	1.0	244	252	68
M 1	75	13:36	827.426	0.01	0.45	✓	—	111	105	1.0	244	252	68
END	80	13:41/13:45	829.199	0.03	1.35	✓	378	111	106	1.0	247	254	68
L 7	85	13:50	832.230	0.03	1.35	✓	314	110	106	2.0	250	253	68
L 6	90	13:55	835.349	0.03	1.35	✓	346	113	107	2.0	249	254	64
L 5	95	14:00	838.439	0.03	1.35	✓	398	116	108	2.0	247	253	67
L 4	100	14:05	841.537	0.02	0.90	✓	397	116	109	1.5	249	251	68
L 3	105	14:10	844.269	0.02	0.90	✓	393	117	109	1.5	249	249	67
L 2	110	14:15	847.021	0.01	0.45	✓	383	116	109	1.0	251	249	67
L 1	115	14:20	849.084	0.01	0.45	✓	323	115	110	1.0	252	245	68
END	120	14:25	851.027	—	—	—	—	—	—	—	—	—	—

0:120

 $V_m = 61.643 \text{ ft}^3/\text{P} = 0.137$ $\Delta H = 0.68$ $T_g = 381^\circ\text{F}$ $T_m = 107^\circ\text{F}$

F 567

F 841

PES, Inc.
Multi-Metals Method Calculations (EPA 12)

Plant ATC-Balboa Pacific

Project # 5102

Operation Pyrolytic Oxidation Unit

Run 3

Location Outlet

Date 10/4/95

Test Data

Vlc =	88.1 cc	Vol. of H2O collected (impingers)
Vm =	61.643 cf	Dry gas meter reading
Pb =	29.7 in. Hg	Barometric pressure
Ps =	29.70 in. Hg	Stack pressure
dP =	0.137	Average sq.rt delta P
dH =	0.881 in. H2O	Average draft gauge reading
Tm =	567.0 R	Average meter temperature
Ts =	840.21 R	Average stack temperature
Dn =	0.504 in.	Nozzle diameter
Y =	1.005	Meter calibration factor
t =	120 min.	Duration of sampling time
A =	2.3300 sq.ft.	Cross sectional area of stack
Cp =	0.84	Pitot tube coefficient
Kp =	85.49	Pitot tube constant
K1 =	17.64 R/in.Hg	constant
K2 =	0.04707 cu.ft/ml	constant
K3 =	0.002669 in.Hg-cf/ml	constant

Instrumentation Data

[O2] = 16.0 %
[CO2] = 2.7 %

CALCULATIONS

1) Volume of gas sampled at standard conditions, Vmstd
Vmstd = $K1 * Y * Vm * (Pb + dH/13.6) / Tm$

Vmstd = 57.37 cu.ft
1.62 cu.m

2) Volume of water vapor collected at standard conditions.
 $V_w(\text{std}) = K_2 * V_{lc}$

$V_w(\text{std}) = 4.15 \text{ scf}$

3) Decimal fraction of moisture by volume in stack gas
 $B_{ws} = V_{wstd} / (V_{mstd} + V_{wstd})$

$B_{ws} = 0.067$

4) Molecular weight of the stack gas on a dry basis M_d .
 $M_d = (1 - B_{ws}) * ((44 * \%CO_2) + (28 * \%CO) + (32 * \%O_2) + (28 * \%N_2)) + (18 * B_{ws})$

$M_d = 28.33$

5) Average stack gas velocity.
 $v_s = K_p * C_p * (dP^{0.5}) * (T_s / P_s * M_d)^{.5}$

$v_s = 9.85 \text{ ft/sec}$

6) Average actual stack gas volumetric flowrate.
 $Q = 60 * v_s * A_s$

$Q = 1377.27 \text{ cfm}$
 39.00 cmm

7) Average stack gas dry volumetric flowrate.
 $Q_{std} = Q * (T_{std} / T_s) * (P_s / P_{std})$

$Q_{std} = 801.18 \text{ dscfm}$
 22.69 dscmm

8) Toxic metal concentrations and emission rates

Element	Sample Mass (ug)	Blank Mass (ug) DL	Conc. (mg/dscm)	Emission Rate (mg/hr)
Copper	10.00	2.00	4.41E-04	6.0E-01
Chromium	7.00	4.00	3.09E-04	4.2E-01
Lead	4.00	4.00	1.76E-04	2.4E-01
Zinc	491.00	10.00	2.16E-02	2.9E+01
Manganese	3.00	2.00	1.32E-04	1.8E-01
Nickel	19.00	10.00	8.37E-04	1.1E+00
Cadmium	7.00	7.00	3.09E-04	4.2E-01
Beryllium	3.00	3.00	1.32E-04	1.8E-01
Arsenic	0.50	0.30	2.20E-05	3.0E-02
Selenium	20.00	20.00	8.81E-04	1.2E+00
Molybdenum	3000.00	2.00	1.32E-01	1.8E+02
Silver	0.10	0.10	4.41E-06	6.0E-03
Antimony	3.00	3.00	1.32E-04	1.8E-01
Barium	14.00	1.00	6.17E-04	8.4E-01
Thallium	0.10	0.10	4.41E-06	6.0E-03

9) Isokineticity

$A_n = 0.001 \text{ ft}^2$ Area of nozzle orifice
 $\% I = 100 \cdot T_s \cdot ((K_3 \cdot V_{lc} + (V_m \cdot Y / T_m) (P_b + dH / 13.6))) / (60 \cdot t \cdot P_s \cdot v_s \cdot A_n)$
 $\% I = 100.40$

Sample Train Operation Data
 Test Date 10/4/95
 Barometer 29.70 in.Hg
 Run # 3
 Static P -0.02 in.H2O
 Pitot Cp 0.84
 Nozzle 0.504

Traverse Point	Delta-P (in. H2O)	Temp. (Deg.F)	delta H	Dry Gas Meter Temp IN	Temp OUT	(dP) ^{-.5}
A-1	0.03	383	1.35	98	96	0.17321
A-2	0.03	395	1.35	102	97	0.17321
A-3	0.02	396	0.9	105	98	0.14142
A-4	0.02	394	0.9	107	99	0.14142
A-5	0.02	391	0.9	107	100	0.14142
A-6	0.02	382	0.9	108	100	0.14142
A-7	0.02	380	0.9	108	100	0.14142
A-8	0.01	305	0.45	109	102	0.1
B-1	0.02	368	0.9	107	102	0.14142
B-2	0.02	397	0.9	109	103	0.14142
B-3	0.02	395	0.9	110	103	0.14142
B-4	0.02	397	0.9	111	104	0.14142
B-5	0.01	392	0.45	112	105	0.1
B-6	0.01	378	0.45	111	106	0.1
B-7	0.01	343	0.45	111	105	0.1
B-8	0.01	359	0.45	111	106	0.1
C-1	0.03	378	1.35	110	106	0.17321
C-2	0.03	394	1.35	113	107	0.17321
C-3	0.03	396	1.35	114	107	0.17321
C-4	0.03	398	1.35	116	108	0.17321
C-5	0.02	397	0.9	116	109	0.14142
C-6	0.02	393	0.9	117	109	0.14142
C-7	0.01	389	0.45	116	109	0.1
C-8	0.01	325	0.45	115	110	0.1
Average		380.208333	0.88125	110.125	103.792 106.958	0.13729

SAMPLE RETRIEVAL DATA

Plant: ATC-BALBOA
 Date: 10-4-95
 Sampling Location: BLANK
 Sampling Type (Method): M.M.
 Run Number: MM-4
 Sample Box Number: _____
 Clean-up Man: _____
 Job Number: _____
 Comments: 399.6-60.1=

Filter

Filter Number: _____
 Description of Filter: _____

Moisture

Impingers:			
Final Volume:	_____ mL	_____ mL	_____ mL
Initial Volume:	_____ mL	_____ mL	_____ mL
Net Volume:	_____ mL	_____ mL	_____ mL
Total H ₂ O:	_____ mL	_____ mL	_____ mL

Silica Gel

Final Volume:	_____ g	_____ g	_____ g
Initial Volume:	_____ g	_____ g	_____ g
Net Volume:	_____ g	_____ g	_____ g
Total Moisture:	_____ g	_____ g	_____ g

Description of Impinger catch: _____

SAMPLE RETRIEVAL DATA

Plant: ATC BALBOA
 Date: 10-4-95
 Sampling Location: _____
 Sampling Type (Method): M.M.
 Run Number: MM3
 Sample Box Number: 88
 Clean-up Man: BROWN/NEWMAN
 Job Number: 5024.0
 Comments: _____

Filter

Filter Number: _____
 Description of Filter: LT. GREEN

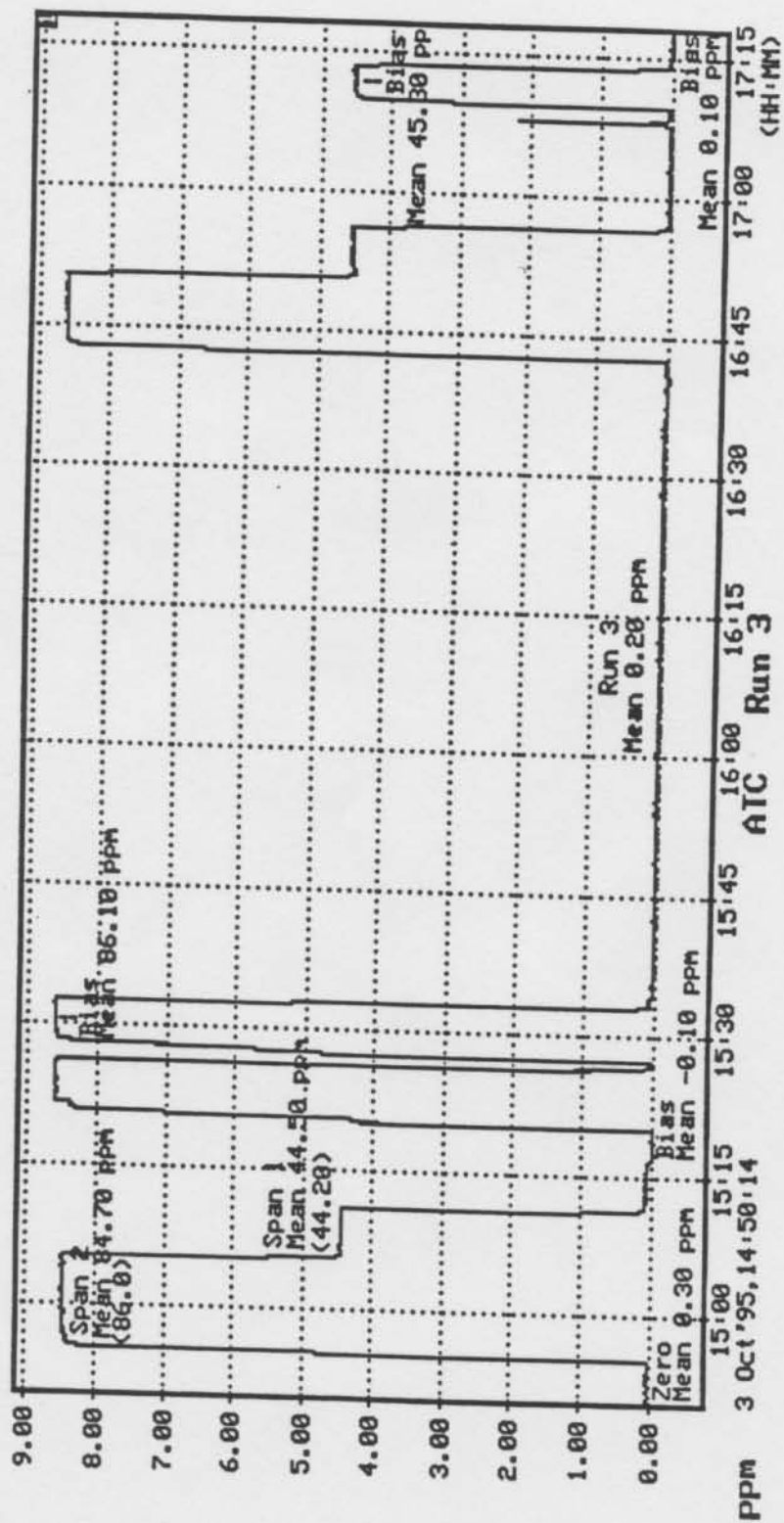
Moisture

	#1	#2	#3
Impingers:			
Final Volume:	694.1 mL	610.1 mL	482.9 mL
Initial Volume:	630.7 mL	600.5 mL	480.8 mL
Net Volume:	63.4 mL	9.6 mL	2.1 mL
Total H ₂ O:			

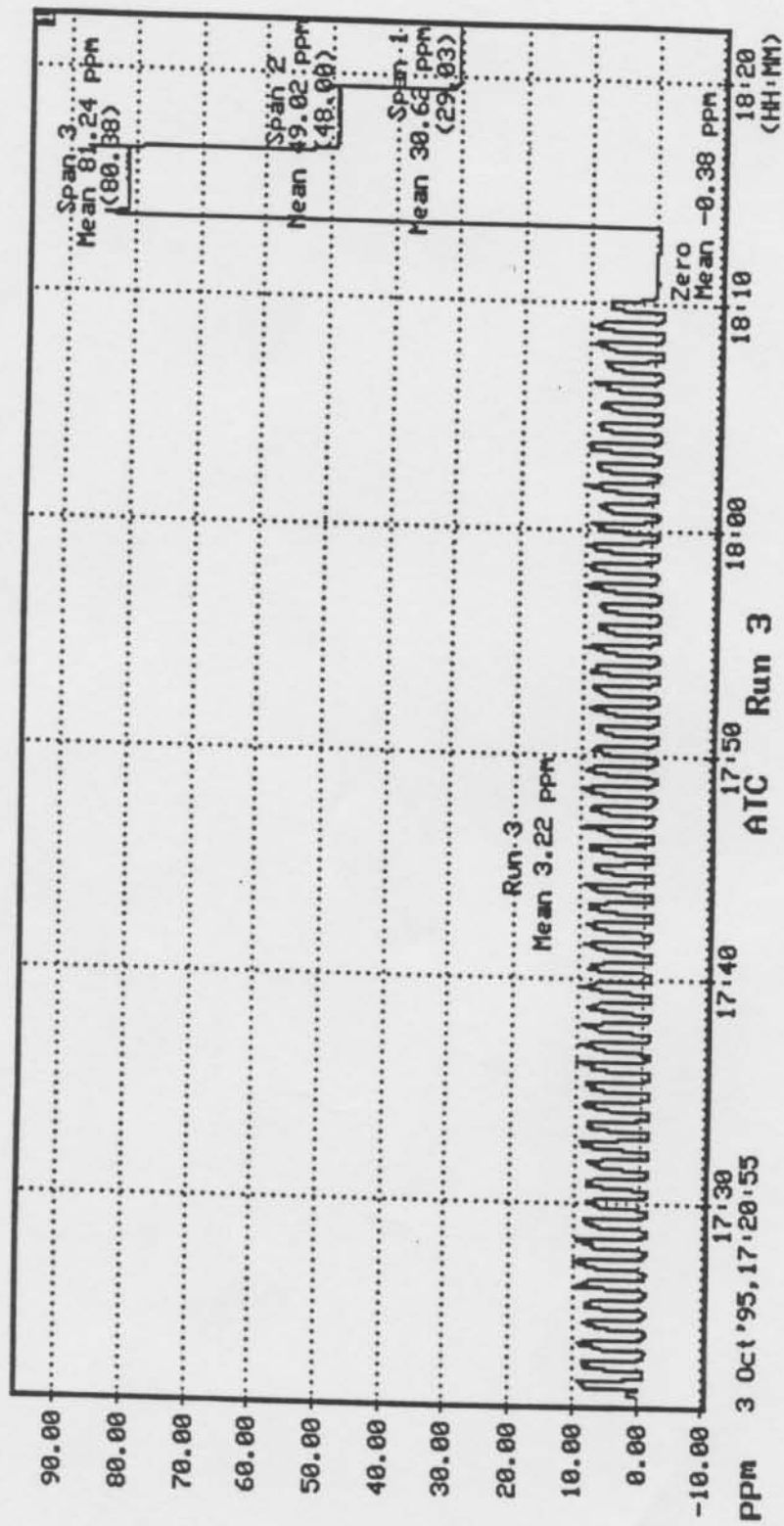
Silica Gel

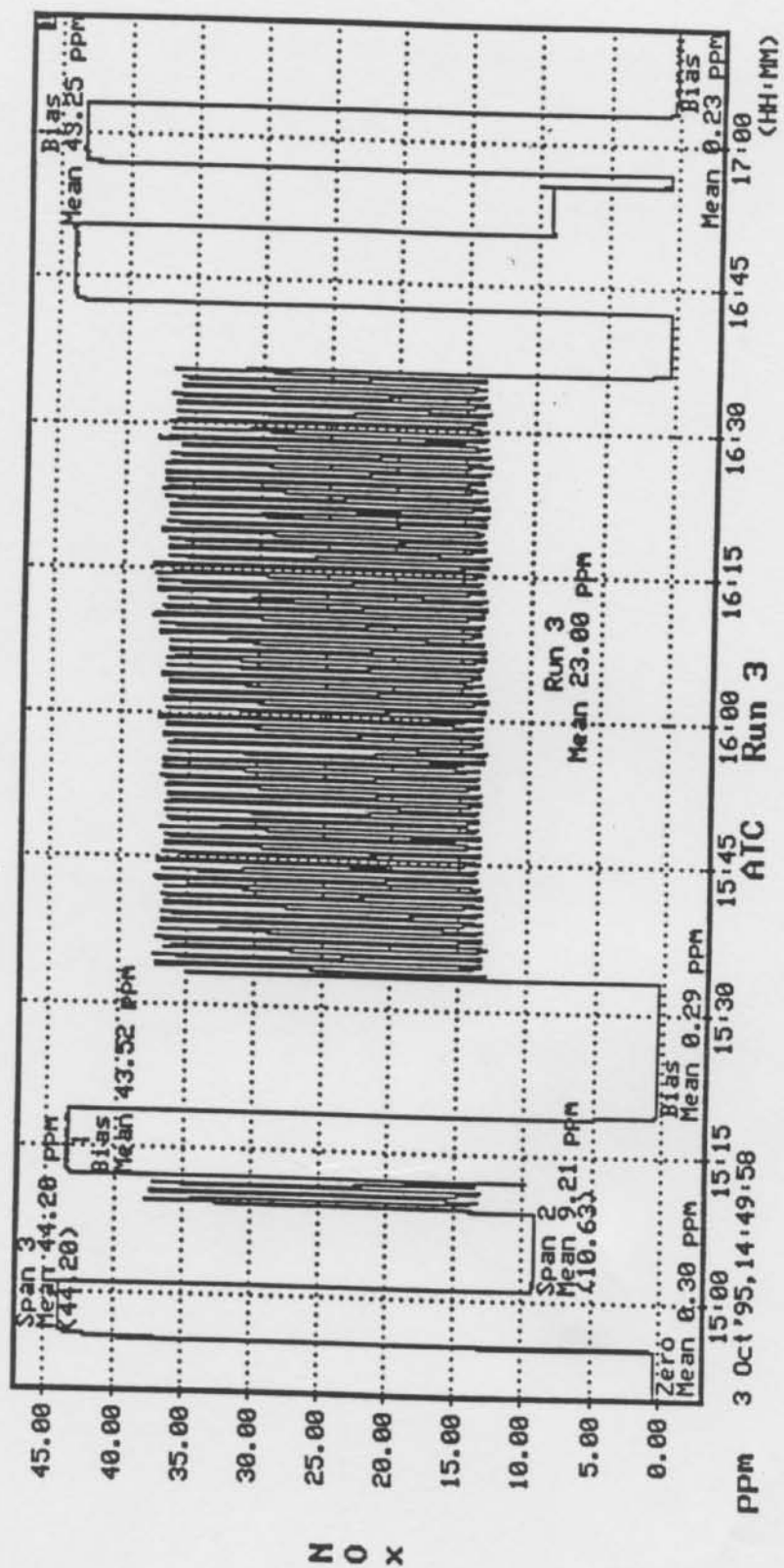
Final Volume:	686.0 g		
Initial Volume:	673.0 g		
Net Volume:	13.0 g		
Total Moisture:			

Description of Impinger catch: 88-1 CLEAR

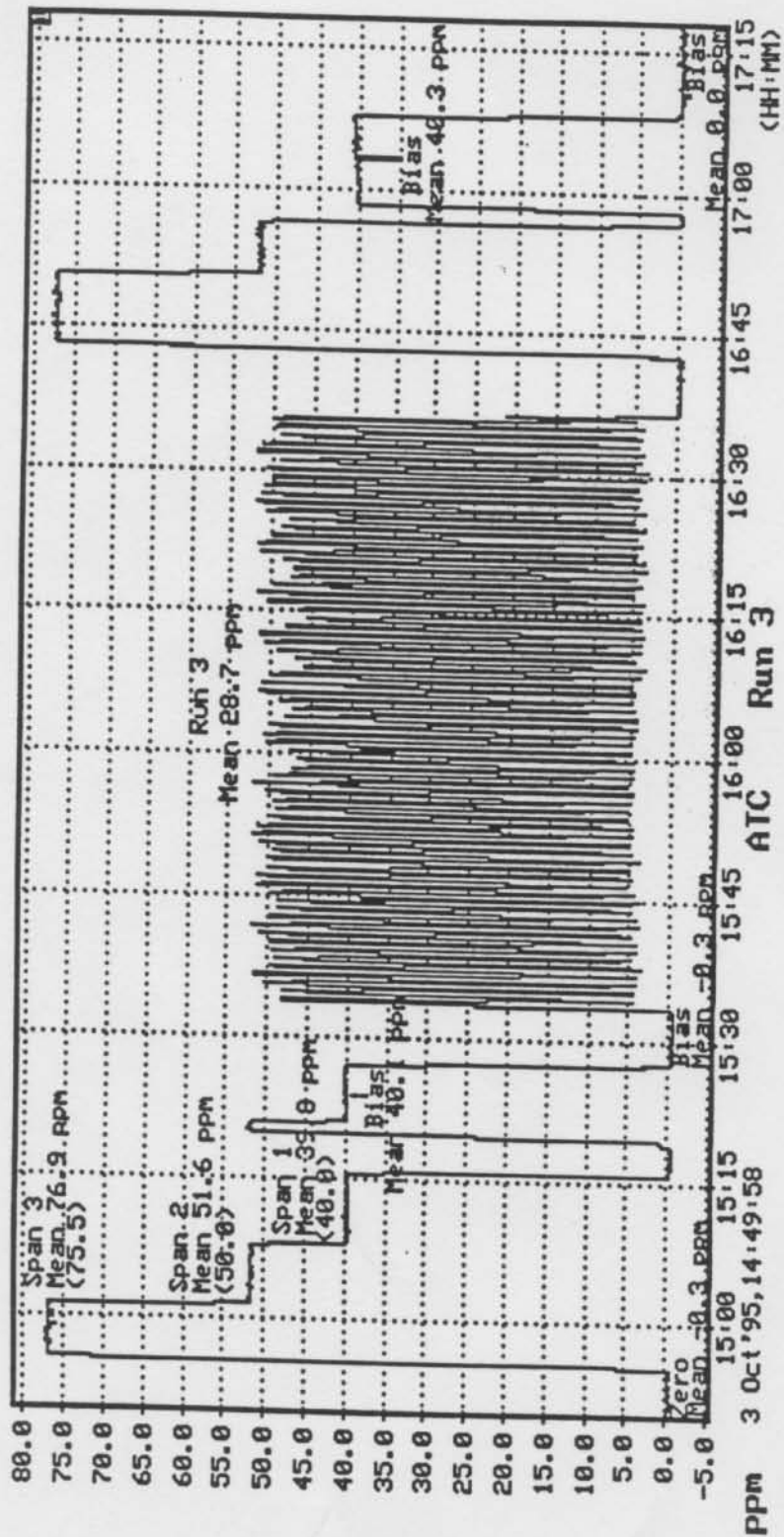


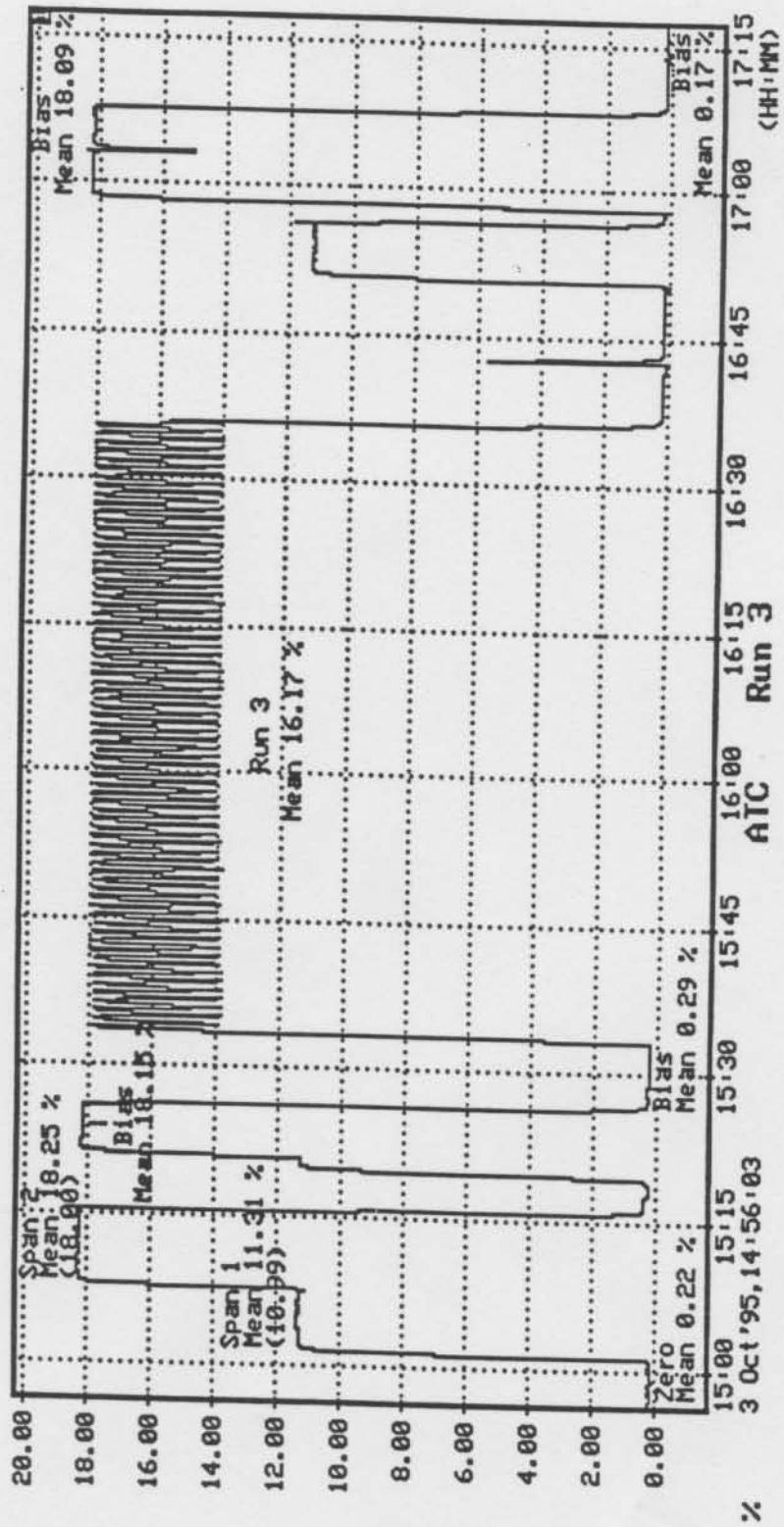
T H C





Carbon Monoxide





PES Inc.
Calculations for :

EPA Method 2,3a,4,6c,7E,10
and 25a

Plant	ATC Consultants - Balboa Pacific
Project #	5102
Operation	Pyrolytic Unit
Run	3
Load	Batch 3
Location	Santa Fe Springs, CA
Date	10/4/95

DATA INPUT

INPUT	Vic =	60.3 cc	Vol. of H2O collected
INPUT	Vm =	43.940 cf	Dry gas meter reading
INPUT	Pb =	29.70 in. Hg	Barometric pressure
INPUT	Pg =	-0.03 in. H2O	Static pressure
INPUT	dP =	0.165	Avg. sq.rt delta P
INPUT	dH =	1.240 in. H2O	Avg. delta H
INPUT	Tm =	574.0 R	Avg. meter temp.
INPUT	Ts =	839.0 R	Avg. stack temp.
INPUT	Y =	1.005	Meter calibration factor
INPUT	t =	72 min.	Duration of sampling time
INPUT	A =	2.3300 sq.ft.	Stack Area
INPUT	Cp =	0.84	Pitot tube coefficient
	Kp =	85.49	Pitot tube constant
	K1 =	17.64 R/in.Hg	constant
	K2 =	0.04707 cu.ft/ml	constant
	K3 =	0.002669 in.Hg-cf/ml	constant

[CO] =	28.60	ppmV(dry)	adj concentration
[NOx] =	23.31	ppmV(dry)	adj concentration
[THC] =	3.08	ppmV(wet)	adj concentration
[SO2] =	0.26	ppmV(dry)	adj concentration

CALCULATIONS

01) Volume of gas sampled at standard conditions, V_{mstd}

$$V_{mstd} = K1 \cdot Y \cdot V_m \cdot (P_b + dH/13.6)/T_m$$

$V_{mstd} =$ 40.43 cu.ft
 1.14 cu.m

02) Volume of water vapor collected at standard conditions.

$$V_{w(std)} = K2 \cdot V_{lc}$$

$V_{w(std)} =$ 2.84 scf

03) Decimal fraction of moisture by volume in stack gas

$$B_{ws} = V_{wstd}/(V_{mstd} + V_{wstd})$$

$B_{ws} =$ 0.066

04) Molecular weight of the stack gas on a wet basis

$$M_s = (1-Q) \cdot ((44 \cdot \%CO_2) + (28 \cdot \%CO) + (32 \cdot \%O_2) + (28 \cdot \%N_2)) + (18 \cdot Q)$$

$M_s =$ 28.31

05) Average stack gas velocity.

$P_s =$ 29.70 in. Hg

$$v_s = K_p \cdot C_p \cdot (dP^{0.5}) \cdot (T_s/P_s \cdot M_d)^{.5}$$

$v_s =$ 11.84 ft/sec

06) Average actual stack gas volumetric flowrate.

$$Q = 60 \cdot v_s \cdot A_s$$

$Q =$ 1654.77 cfm
 46.86 cmm

07) Average stack gas dry volumetric flowrate.

$$Q_{std} = Q \cdot (T_{std}/T_s) \cdot (P_s/P_{std}) \cdot (1-B_{ws})$$

$Q_{std} =$ 965.84 dscfm
 27.35 dscmm
 57950.53 dscfh

08) Emission Calculation - Carbon Monoxide

$$\text{lbs CO/hr} = ([\text{CO}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

$[\text{CO}] =$ 28.60 ppmv (dry) Actual conc.
 $[\text{CO}] =$ 0.12 Lbs/hr

09) Emission Calculation - Nitrogen Oxides

$$\text{lbs NOx/hr} = ([\text{NOx}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

$[\text{NOx}] =$ 23.3 ppmv (dry) Actual Conc.
 $[\text{NOx}] =$ 0.16 Lbs/hr

10) Emission Calculation - Total Hydrocarbons

$$\text{lbs THC/hr} = ([\text{THC}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

$[\text{THC}] =$ 3.3 ppmv (dry) Actual Conc.
 $[\text{THC}] =$ 0.02 Lbs/hr

11) Emission Calculation - Sulfur Dioxide

$$\text{lbs NMHC/hr} = ([\text{NMHC}] \cdot \text{DSCFH} \cdot \text{MW}) / 387 \cdot 10^6$$

$[\text{SO}_2] =$ 0.3 ppmv (dry) Actual Conc.
 $[\text{SO}_2] =$ 0.03 Lbs/hr

APPENDIX B
LABORATORY REPORTS

September 29, 1995

PACIFIC ENVIRONMENTAL SERVICES
13100 Brooks Drive
Baldwin Park, CA 91706

Attn: S. Hugh Brown

JOB NO. 30387

S

WCAS

**WEST COAST
ANALYTICAL
SERVICE, INC.**

ANALYTICAL CHEMISTS

LABORATORY REPORT

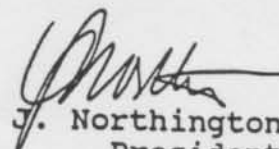
Samples Received: Three (3) Impingers & Three (3) Filters
Date Received: 9-15-95
Project Name: ATC-Balboa Pacific

The samples were analyzed as follows:

<u>Samples Analyzed</u>	<u>Analysis</u>	<u>Page</u>
Three (3) samples	Metals by CARB 436	2 - 3

Page 1 of 3


Michael Shelton
Technical Director


D. J. Northington, Ph.D.
President

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WEST COAST ANALYTICAL SERVICE, INC.

PACIFIC ENVIRONMENTAL SERVICES
Mr. S. Hugh BrownJob # 30387
September 29, 1995

LABORATORY REPORT

Carb Method 436
Quantitative Analysis Report
Inductively Coupled Plasma-Mass Spectrometry

Total Micrograms Per Impinger Train (ug)

	ATC-3	ATC-5	ATC-7	Blank DL
Beryllium	ND<1	ND<1	ND<1	1
Chromium	10	11	12	2
Manganese	4	4	5	1
Nickel	8.3	4.7	5.2	0.4
Copper	18	13	7	1
Zinc	69	48	58	8
Arsenic	2.3	2.9	2.4	0.2
Selenium	ND<7	ND<7	ND<7	7
Molybdenum	842	2500	2470	3
Silver	ND<0.1	ND<0.1	ND<0.1	0.1
Cadmium	ND<2	ND<5	ND<5	2
Antimony	ND<3	ND<3	ND<3	3
Barium	32.6	33	34.2	0.4
Thallium	ND<0.1	ND<0.1	ND<0.1	0.1
Lead	8.7	7	6.2	0.2

Date Analyzed: 9-26-95

WEST COAST ANALYTICAL SERVICE, INC.

PACIFIC ENVIRONMENTAL SERVICES
Mr. S. Hugh BrownJob # 30387
September 29, 1995

LABORATORY REPORT

Client: ATC-3 (Quality Control)
Matrix: Impinger train

Total micrograms Per Impinger Train (ug)

Sample	Duplicate		RPD %	Spike Conc ug	Spk Rslt		Detect. Limit
						% Recovery	
Beryllium	ND<1	ND<1		125	159	127.2	1
Chromium	10	10		125	140	104	2
Nickel	8.3	6.9		125	129	97.1	0.4
Copper	18	17		125	139	97.2	1
Zinc	72	63		125	177	87.6	10
Arsenic	2.3	3.3		125	121	94.6	0.5
Selenium	ND<7	ND<7		1250	1240	99.2	7
Molybdenum	842	854	1.4	125	980		3
Silver	ND<0.1	ND<0.1		125	126	100.8	0.1
Cadmium	ND<2	ND<2		125	124	99.2	2
Antimony	ND<3	ND<3		125	138	110.4	3
Barium	32.6	34.5	5.7	125	158	99.6	0.4
Thallium	ND<0.1	ND<0.1		125	122	97.6	0.1
Lead	8.7	9.1	4.5	125	130	96.9	0.2

Date Analyzed: 9-26-95

Abbreviations Summary

General Reporting Abbreviations:

- B Blank - Indicates that the compound was found in both the sample and the blank. The sample value is reported without blank subtraction. If the sample value is less than 10X the blank value times the sample dilution factor, the compound may be present as a laboratory contaminant.
- D Indicates that the sample was diluted, and consequently the surrogates were too dilute to accurately measure.
- DL Detection Limit - Is the minimum value which we believe can be detected in the sample with a high degree of confidence, taking into account dilution factors and interferences. The reported detection limits are equal to or greater than Method Detection Limits (MDL) to allow for day to day and instrument to instrument variations in sensitivity.
- J Indicates that the value is an estimate.
- ND Not Detected - Indicates that the compound was not found in the sample at or above the detection limit.
- ppm parts per million (billion) in liquids is usually equivalent to mg/l (ug/l), or in solids to mg/kg (ug/kg). In the gas phase it is equivalent to ul/l (ul/m³).
- ppb
- TR Trace - Indicates that the compound was observed at a value less than our normal reported Detection Limit (DL), but we feel its presence may be important to you. These values are subject to large errors and low degrees of confidence.
- | | | | |
|-------------|--------------|---------------|---------|
| kg kilogram | mg milligram | l liter | m meter |
| g gram | ug microgram | ul microliter | |

QC Abbreviations:

- Control Control Limits are determined from historical data for a QC parameter. The test value must be within this acceptable range for the test to be considered in control. Usually this range corresponds to the 99% confidence interval for the historical data.
- % Error Percent Error - This is a measure of accuracy based on the analysis of a Laboratory Control Standard (LCS). An LCS is a reference sample of known value such as an NIST Standard Reference Material (SRM). The % Error is expressed in percent as the difference between the known value and the experimental value, divided by the known value. The LCS may simply be a solution based standard which confirms calibration (ICV or CCV - initial or continuing calibration verification), or it may be a reference sample taken through preparation and analysis.

CHAIN-OF-CUSTODY RECORD

DATE 9-15-56

[illegible]

~~10-10-3-8-5~~ 1112 0387



WEST COAST
ANALYTICAL
SERVICE, INC.

ANALYTICAL CHEMISTS

November 6, 1995

PACIFIC ENVIRONMENTAL SERVICES
13100 Brooks Drive
Suite 100
Baldin Park, CA 91706

Attn: Siya Mokm

Re: WCAS Job Number: 30527

Dear Mr. Mokm,

Please find enclosed a copy of the revised laboratory report for WCAS Job No: 30527. Per your request, molybdenum has been added to the results.

Sincerely,

WEST COAST ANALYTICAL SERVICE, INC.

A handwritten signature in cursive script, appearing to read "Ramona Lee Northington".

Ramona Lee Northington
Laboratory Director

RLN:sm

October 26, 1995

WCAS

**WEST COAST
ANALYTICAL
SERVICE, INC.**

ANALYTICAL CHEMISTS

PACIFIC ENVIRONMENTAL SERVICES
13100 Brooks Drive
Suite 100
Baldwin Park, CA 91706

Attn: Siya Mokm

JOB NO. 30527

S

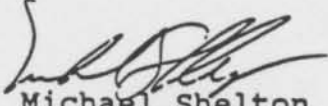
LABORATORY REPORT

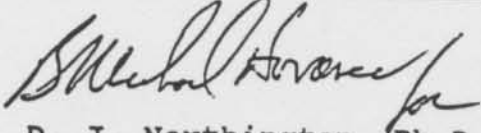
Samples Received: Four (4) Impinger Samples in Seven (7)
Containers & One (1) Filter Received 10-5-95 &
One (1) Filter Received 10-13-95
Purchase Order No: 5102

The samples were analyzed as follows:

<u>Samples Analyzed</u>	<u>Analysis</u>	<u>Page</u>
Four (4) samples	Metals by CARB 436	2 - 4

Page 1 of 4


Michael Shelton
Technical Director


D. J. Northington, Ph.D.
President

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WEST COAST ANALYTICAL SERVICE, INC.

PACIFIC ENVIRONMENTAL SERVICES
Mr. Siya Mokm

Job # 30527
October 26, 1995

LABORATORY REPORT

Metals by CARB 436
Quantitative Analysis Report
Inductively Coupled Plasma-Mass Spectrometry

Total micrograms per Sample Train

	MM1/ATC2	MM2/ATC2	MM4/ATC2	Blank Detect. Limit
	-----	-----	-----	-----
Antimony	ND<2	ND<2	ND<2	2
Arsenic	ND<0.1	ND<0.1	ND<0.1	0.1
Barium	4	3	ND<1	1
Beryllium	ND<1	ND<1	ND<1	1
Cadmium	3	3	ND<0.3	1
Chromium	ND<6	ND<6	ND<6	6
Copper	12	9	ND<1	1
Lead	12.7	7.5	0.2	0.1
Manganese	ND<4	ND<4	ND<4	4
Molybdenum	801	592	ND<2	2
Nickel	ND<9	ND<9	16	9
Selenium	ND<10	ND<10	ND<10	10
Silver	ND<0.1	ND<0.1	ND<0.1	0.1
Thallium	ND<0.2	ND<0.2	ND<0.2	0.2
Zinc	109	65	ND<9	9

Date Analyzed: 10-13-95

WEST COAST ANALYTICAL SERVICE, INC.

PACIFIC ENVIRONMENTAL SERVICES
Mr. Siya Mokm

Job # 30527
October 26, 1995

LABORATORY REPORT

Metals by CARB 436
Quantitative Analysis Report
Inductively Coupled Plasma-Mass Spectrometry

Total micrograms per Sample Train

	MM3/ATC2	Blank DL
	-----	-----
Antimony	ND<3	
Arsenic	0.5	3
		0.3
Barium	14	
Beryllium	ND<3	1
		3
Cadmium	ND<7	
Chromium	7	7
		4
Copper	10	
Lead	ND<4	2
		4
Manganese	3	
Molybdenum	3000	2
Nickel	19	2
		10
Selenium	ND<20	
Silver	ND<0.1	20
		0.1
Thallium	ND<0.1	
Zinc	491	0.1
		10

Date Analyzed: 10-23-95

WEST COAST ANALYTICAL SERVICE, INC.

PACIFIC ENVIRONMENTAL SERVICES
Mr. Siya Mokm

Job # 30527
October 26, 1995

LABORATORY REPORT

Sample: MM2/ATC2 (Quality Control)
Matrix: Impinger

Total micrograms per Sample Train

Sample		Spike Conc ppm	MS		MSD		
				% Recovery		% Recovery	% RPD
Antimony	ND<2	142.9	135	94.5	135	94.5	0
Arsenic	ND<0.1	142.9	126	126	126	126	0
Barium	3	142.9	145	99.4	141	96.6	2.8
Beryllium	ND<1	142.9	152	106.4	168	117.6	10
Cadmium	3	142.9	145	99.4	155	106.4	6.7
Chromium	ND<6	142.9	158	110.6	154	107.8	2.6
Copper	9	142.9	152	100.1	159	105	4.5
Lead	7.5	142.9	163	108.8	162	108.1	0.6
Molybdenum	592	142.9	732	-----	731	-----	0.1
Nickel	ND<9	142.9	157	109.9	157	109.9	0
Selenium	ND<10	1428.6	1340	93.8	1410	98.7	5.1
Silver	ND<0.1	142.9	138	96.6	147	102.9	6.3
Thallium	ND<0.2	142.9	148	103.6	151	105.7	2
Zinc	59	142.9	204	101.5	204	101.5	0

Date Analyzed: 10-13-95

CHAIN OF CUSTODY RECORD

COMPANY THE UNIVERSITY OF ALABAMA
ADDRESS 100 UNIVERSITY BLVD
ANN ARBOR MI 48106
PHONE NO. 313 763 7777 FAX 313 763 7777
MAIL REPORT TO: 100 UNIVERSITY BLVD

PROJECT MANAGER _____
PROJECT NAME _____
PROJECT NO. _____
PURCHASE ORDER NO. _____

WEST COAST ANALYTICAL SERVICE, INC.
9840 Alburis Avenue
Santa Fe Springs, CA 90670
(310) 948-2225 Fax (310) 948-5850

COMMENTS:

If sample is liquid & has sediment or particulate should we:

- _____ test filtrate only?
- _____ mix sample by shaking?
- _____ test particulate only?

If sample is multi-phased, should we:

- _____ test each phase separately?
- _____ test only ONE phase? Which phase?
- _____ mix all phases by shaking, if possible?

Sample I.D. #	Date Sampled	Time Sampled	Preservative	MATRIX				# of containers	Remarks																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																	
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Retiniquished by:

Date/Time 11:46 Received by:

Received by: *L. J. J. J. J.*
Received by: *L. J. J. J. J.*

Date/Time

Relinquished by:

Observed

10/11/20

Date/Time	2017.11.10
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Retinquished by:

1

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Date/Time _____

NOTE: Samples are discarded 30 days after date of final report.

White Copy • WCAS • Yellow • Report • Pink • Chart

WCAS Job No.

1630527



PACIFIC ENVIRONMENTAL SERVICES, INC.

Project No.	51CZ.CCC	Page	1	of	1
Client	ATC Ballon Pacific				
Location					
Prepared By	Date	Checked By	Date	Sheet Title	
RIN	9/21/99			EPA Method 5 Analysis	

SAMPLE FILTER IMPINGERS ACETONE TOTAL

- ATC-2 0.4530
 0.4574
 0.0006 29.1615
 (13) 29.1574
 00.0041 29.1574
 (13) 29.1561
 0.0013

- ATC-4 0.4717
 0.4517
 0.0200 28.6174
 (15) 28.6139
 0.0035 28.6139
 (15) 28.6007
 0.0032

- ATC-6 0.4457
 0.4491
 -0.0034 28.6414
 (12) 28.6396
 0.0018 28.6396
 (12) 28.6377
 0.0019

BLANK

0.4532

29.0844
29.0844
0.0000



PACIFIC ENVIRONMENTAL SERVICES, INC.

Project No.

4100

Page

of

1

1

Client

ATC BALBOA PACIFIC

Location

Prepared By

Date

Checked By

Date

Sheet Title

EPA Method 5 Analysis

<u>SAMPLE</u>	<u>FILTER</u>	<u>IMPINGERS</u>	<u>ACETONE</u>	<u>TOTAL</u>
ATC2/PM1	$\begin{array}{r} 0.4502 \\ 0.4470 \\ \hline 0.0032 \end{array}$	$\begin{array}{r} 28.6141 \\ 28.6129 \\ \hline 0.0012 \end{array}$	$\begin{array}{r} 28.6129 \\ 28.6107 \\ \hline 0.0022 \end{array}$	0.0066
ATC2/PM2	$\begin{array}{r} 0.4435 \\ 0.4429 \\ \hline 0.0006 \end{array}$	$\begin{array}{r} 28.7259 \\ 28.7228 \\ \hline 0.0031 \end{array}$	$\begin{array}{r} 28.7228 \\ 28.7175 \\ \hline 0.0053 \end{array}$	0.0090
ATC2/PM3	$\begin{array}{r} 0.4532 \\ 0.4490 \\ \hline 0.0042 \end{array}$	$\begin{array}{r} 28.6019 \\ 28.6010 \\ \hline 0.0009 \end{array}$	$\begin{array}{r} 28.6010 \\ 28.6005 \\ \hline 0.0005 \end{array}$	0.0056
BLANK	$\begin{array}{r} 0.4514 \\ 0.4514 \\ \hline 0.0000 \end{array}$	$\begin{array}{r} 28.6877 \\ 28.6877 \\ \hline 0.0000 \end{array}$	$\begin{array}{r} 28.6877 \\ 28.6875 \\ \hline 0.0002 \end{array}$	0.0002

APPENDIX C
CALIBRATION DATA



Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 887-2571

Fax: (909) 887-0549

C E R T I F I C A T E O F A N A L Y S I S

PACIFIC ENVIRONMENTAL SER

13100 BROOKS DRIVE

BALDWIN PARK

CA 91706

PROJECT #: 02-36512-001

PO#: 0640-102

ITEM #: 02024520 4AL

DATE: 2/21/95

CYLINDER #: ALM041187

FILL PRESSURE: 2000 PSIG

BLEND TYPE : CERTIFIED MASTER GAS

ANALYTICAL ACCURACY: +-1% NIST

COMPONENT	REQUESTED GAS		ANALYSIS	
	CONC	MOLES	(MOLES)	
CARBON DIOXIDE	11.	%	10.98	%
CARBON MONOXIDE	50.	PPM	50.00	PPM
OXYGEN	11.	%	10.99	%
NITROGEN		BALANCE		BALANCE

2000 PSIG BIN 1 HC/RG 02/24

CRM 1675 ALM001136 - CO2
 NTRM 1678 ALM09624 - CO
 CRM 2658 ALM017565 - O2

ANALYST:

FREMONT, CALIFORNIA SAN BERNARDINO, CALIFORNIA LONGMONT, COLORADO CHICAGO, ILLINOIS BATON ROUGE, LOUISIANA
 WAKEFIELD, MASSACHUSETTS TROY, MICHIGAN DURHAM, NORTH CAROLINA SOUTH PLAINFIELD, NEW JERSEY
 AVON LAKE, OHIO SARNIA, ONTARIO HOUSTON, TEXAS PLUMSTEADVILLE, PENNSYLVANIA BREDA, THE NETHERLANDS



Shipped
From:

2600 CAJON BLVD.
SAN BERNARDINO CA 92411
Phone: 909-887-2571

Fax: 909-887-0549

CERTIFICATE OF ANALYSIS

PACIFIC ENVIRONMENTAL SER

13100 BROOKS DRIVE

BALDWIN PARK

CA 91706

PROJECT #: 02-37653-001
PO#: 0640-102 REPLACEMENT
ITEM #: 02024520 4AL
DATE: 4/10/95

CYLINDER #: AAL1080

FILL PRESSURE: 2000 PSIG

BLEND TYPE : CERTIFIED MASTER GAS

ANALYTICAL ACCURACY: +-1% NIST

COMPONENT

CARBON DIOXIDE
CARBON MONOXIDE
OXYGEN
NITROGEN

REQUESTED GAS CONC MOLES

18. %
75. PPM
20. %
BALANCE

ANALYSIS (MOLES)

18.06 %
75.47 PPM
19.99 %
BALANCE

2000 PSIG BIN 1 04-14-95

ANALYST:

PLUMSTEADVILLE, PENNSYLVANIA / TROY, MICHIGAN / HOUSTON, TEXAS, DURHAM, NORTH CAROLINA
SOUTH PLAINFIELD, NEW JERSEY / FREMONT, CALIFORNIA / WAKEFIELD, MASSACHUSETTS / LONGMONT, COLORADO
BATON ROUGE, LOUISIANA



Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 887-2571 FAX: (909) 887-0549

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
PACIFIC ENVIRONMENTAL SER
STEVE HERNANDEZ
13100 BROOKS DRIVE
BALDWIN PARK CA 91706

Assay Laboratory
Scott Specialty Gases
2600 Cajon Boulevard
San Bernardino, CA 92411

Purchase Order 0640-102
Project # 33323.001

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay and Certification of Gaseous Calibration Standards; Procedure G1; September 1993.

Cylinder Number ALM007529
Cylinder Pressure* 1850PSIG

Certification Date 09-21-94

Exp. Date 09-21-96

ANALYZED CYLINDER

Components
(NITRIC OXIDE)
TOTAL OXIDES OF NITROGEN

Certified Concentration
5.095PPM
5.154PPM

Analytical Uncertainty*
± 1 % NIST Traceable
REFERENCE VALUE ONLY

(Nitrogen)

Balance Gas

*Do not use when cylinder pressure is below 150 psig.

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type/Sample No. SRM2627A
Expiration Date 12-95

Cylinder Number CLM004199

Concentration
4.8PPM NO IN N2

INSTRUMENTATION

Instrument/Model/Serial #
TECO / 10AR / 14853-150

Last Date Calibrated
09-14-94

Analytical Principle
Chemi-Luminescent

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components	First Triad Analysis	Second Triad Analysis	Calibration Curve																																										
NITRIC OXIDE	<table><tr><td>Date: 09-14-94</td><td colspan="3">Response Units: mv</td></tr><tr><td>Z1= 0.00</td><td>R1= 39.3</td><td colspan="2">T1= 41.8</td></tr><tr><td>R2= 39.3</td><td>Z2= 0.00</td><td colspan="2">T2= 41.8</td></tr><tr><td>Z3= 0.00</td><td>T3= 41.7</td><td colspan="2">R3= 39.3</td></tr><tr><td colspan="2">Avg. Conc. of Cust Cyl.</td><td colspan="2">5.101PPM</td></tr></table>	Date: 09-14-94	Response Units: mv			Z1= 0.00	R1= 39.3	T1= 41.8		R2= 39.3	Z2= 0.00	T2= 41.8		Z3= 0.00	T3= 41.7	R3= 39.3		Avg. Conc. of Cust Cyl.		5.101PPM		<table><tr><td>Date: 09-21-94</td><td colspan="3">Response Units: mv</td></tr><tr><td>Z1= 0.00</td><td>R1= 39.3</td><td colspan="2">T1= 41.7</td></tr><tr><td>R2= 39.3</td><td>Z2= 0.00</td><td colspan="2">T2= 41.7</td></tr><tr><td>Z3= 0.00</td><td>T3= 41.6</td><td colspan="2">R3= 39.3</td></tr><tr><td colspan="2">Avg. Conc. of Cust Cyl.</td><td colspan="2">5.089PPM</td></tr></table>	Date: 09-21-94	Response Units: mv			Z1= 0.00	R1= 39.3	T1= 41.7		R2= 39.3	Z2= 0.00	T2= 41.7		Z3= 0.00	T3= 41.6	R3= 39.3		Avg. Conc. of Cust Cyl.		5.089PPM		<table><tr><td>Concentration=</td><td>LINEAR CURVE</td></tr></table>	Concentration=	LINEAR CURVE
Date: 09-14-94	Response Units: mv																																												
Z1= 0.00	R1= 39.3	T1= 41.8																																											
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Z3= 0.00	T3= 41.6	R3= 39.3																																											
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Date:	Response Units: mv																																												
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R2=	Z2=	T2=																																											
Z3=	T3=	R3=																																											
Avg. Conc. of Cust Cyl.																																													
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Avg. Conc. of Cust Cyl.																																													
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	<table><tr><td>Date:</td><td colspan="3">Response Units: mv</td></tr><tr><td>Z1=</td><td>R1=</td><td colspan="2">T1=</td></tr><tr><td>R2=</td><td>Z2=</td><td colspan="2">T2=</td></tr><tr><td>Z3=</td><td>T3=</td><td colspan="2">R3=</td></tr><tr><td colspan="2">Avg. Conc. of Cust Cyl.</td><td colspan="2"></td></tr></table>	Date:	Response Units: mv			Z1=	R1=	T1=		R2=	Z2=	T2=		Z3=	T3=	R3=		Avg. Conc. of Cust Cyl.				<table><tr><td>Date:</td><td colspan="3">Response Units: mv</td></tr><tr><td>Z1=</td><td>R1=</td><td colspan="2">T1=</td></tr><tr><td>R2=</td><td>Z2=</td><td colspan="2">T2=</td></tr><tr><td>Z3=</td><td>T3=</td><td colspan="2">R3=</td></tr><tr><td colspan="2">Avg. Conc. of Cust Cyl.</td><td colspan="2"></td></tr></table>	Date:	Response Units: mv			Z1=	R1=	T1=		R2=	Z2=	T2=		Z3=	T3=	R3=		Avg. Conc. of Cust Cyl.				<table><tr><td>Concentration=</td><td></td></tr></table>	Concentration=	
Date:	Response Units: mv																																												
Z1=	R1=	T1=																																											
R2=	Z2=	T2=																																											
Z3=	T3=	R3=																																											
Avg. Conc. of Cust Cyl.																																													
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Z1=	R1=	T1=																																											
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Z3=	T3=	R3=																																											
Avg. Conc. of Cust Cyl.																																													
Concentration=																																													

Special Notes:

Analyst: _____



Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 887-2571 FAX: (909) 887-0540

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS RECERTIFICATION

Customer
PACIFIC ENVIRONMENTAL SER
STEVE HERNANDEZ
13100 BROOKS DRIVE
BALDWIN PARK CA91706

Assay Laboratory
Scott Specialty Gases
2600 Cajon Boulevard
San Bernardino, CA 92411

Purchase Order F028-000
Scott Project # 29408.001

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol 1 Procedure #G1, Section Number 3.0.4

Cylinder Number ALM010841
Cylinder Pressure 1800PSIG

Certification Date 01-25-94

Previous Certification Dates 10-26-93

Acid Rain Exp.
General Exp. 01-25-96

ANALYZED CYLINDER

Components
NITRIC OXIDE

Certified Concentration
10.43PPM

Analytical Uncertainty*
±1% NIST Traceable

Balance Gas: Nitrogen
NOX

10.63PPM

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type
GMS
Expiration Date
12-13-96

Cylinder Number
ALM033926

Concentration
9.950PPM

INSTRUMENTATION

Instrument/Model/Serial #
TECO / 10AR-38644-258

Last Date Calibrated
12-02-93

Analytical Principle
Chemi-Luminescent

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components

NITRIC OXIDE

Previous Certification

Date: 10-26-93 Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl. 10.26PPM

Third Triad Analysis

Date: 01-25-94 Response Units: mv
Z1= 0.08 R1= 92.48 T1= 96.83
R2= 92.52 Z2= 0.12 T2= 96.96
Z3= 0.140.08 T3= 96.98 R3= 92.49
Avg. Conc. of Cust Cyl. 10.43PPM

Calibration Curve LINEAR

Concentration=

Date: Response Units:
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Date: Response Units:
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Concentration=

Date: Response Units:
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Date: Response Units:
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Concentration=

SPECIAL NOTES: IF THIS PRODUCT IS USED FOR ACID RAIN COMPLIANCE, THE ACID RAIN DATE NOTED ABOVE APPLIES PER 40 CFT PART 73, APPENDIX A. OTHERWISE THE GENERAL EXPIRATION DATE APPLIES.

Analyst



Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 887-2571 FAX: (909) 887-0549

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
PACIFIC ENVIRONMENTAL SER
13100 BROOKS DRIVE
BALDWIN PARK, CA 91706

Assay Laboratory
Scott Specialty Gases
2600 Cajon Boulevard
San Bernardino, CA 92411

Purchase Order 0640-102
Project # 36545.002

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay and Certification of Gaseous Calibration Standards, Procedure G1; September 1993.

Cylinder Number ALM052505
Cylinder Pressure+ 2000 PSIG

Certification Date 03/14/95

Exp. Date 03/14/97

ANALYZED CYLINDER

Components
(NITRIC OXIDE)
TOTAL OXIDES IN NITROGEN

Certified Concentration
25.71 PPM
25.93 PPM

Analytical Uncertainty*
±1% NIST TRACEABLE
REFERENCE VALUE ONLY

(Nitrogen)

Balance Gas

+ Do not use when cylinder pressure is below 150 psig.

* Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type/SRM Sample No. CRM 1683
Expiration Date 06/30/95

Cylinder Number
ALM015394

Concentration
49.6 PPM NO IN N2

INSTRUMENTATION

Instrument/Model/Serial #
TECO / 10AR / 14853-150

Last Date Calibrated
03/04/95

Analytical Principle
Chemi-Luminescent

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components

First Triad Analysis

Date: 03/07/95 Response Units: mv
Z1= 0.00 R1= 46.82 T1= 24.17
R2= 46.80 Z2= 0.01 T2= 24.20
Z3= 0.01 T3= 24.21 R3= 46.78
Avg. Conc. of Cust Cyl 25.71 PPM

Second Triad Analysis

Date: 03/14/95 Response Units: mv
Z1= 0.00 R1= 46.79 T1= 24.20
R2= 46.81 Z2= 0.00 T2= 24.18
Z3= 0.01 T3= 24.18 R3= 46.81
Avg. Conc. of Cust Cyl 25.71 PPM

Calibration Curve

Concentration= Ax + B
A = 2.592
B = 0.07521

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl

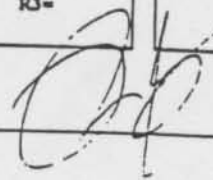
Concentration=

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl

Concentration=

Special Notes:

Analyst: 



Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 887-2571 FAX (909) 887-0549

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
PACIFIC ENVIRONMENTAL SER.
STEVE HERNANDEZ
13100 BROOKS DRIVE
BALDWIN PARK, CA 91706

Assay Laboratory
Scott Specialty Gases
2600 Cajon Boulevard
San Bernardino, CA 92411

Purchase Order 0640-102
Project # 29933.001

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol 1 Procedure #G1, Section Number 3.0.4

Cylinder Number ALM014364
Cylinder Pressure 1900 psig

Certification Date 02-15-94

Exp. Date 08-15-94

ANALYZED CYLINDER

Components
SULFUR DIOXIDE

Certified Concentration
46.28 PPM

Analytical Uncertainty*
± 1 % NIST Traceable

Balance Gas: Nitrogen

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type
GMIS
Expiration Date 06-94

Cylinder Number
AAL9133

Concentration
238.8 ppm

INSTRUMENTATION

Instrument/Model/Serial #
Horiba / OPE-135D / 56463601

Last Date Calibrated
01-31-94

Analytical Principle
NDIR

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components

First Triad Analysis

Date: 02-08-94 Response Units: mv
Z1= 0.00 R1= 97.0 T1= 19.9
R2= 97.0 Z2= 0.00 T2= 19.9
Z3= 0.00 T3= 19.9 R3= 97.0
Avg. Conc. of Cust Cyl. 46.28 ppm

Second Triad Analysis

Date: 02-15-94 Response Units: mv
Z1= 0.00 R1= 97.0 T1= 19.9
R2= 97.0 Z2= 0.00 T2= 19.9
Z3= 0.00 T3= 19.9 R3= 97.0
Avg. Conc. of Cust Cyl. 46.28 ppm

Calibration Curve

Concentration= Ax + B
A = 0.4925
B = 0.03282

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Concentration=

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Concentration=

SPECIAL NOTES: IF THIS PRODUCT IS USED FOR ACID RAIN COMPLIANCE, THE ACID RAIN EXPIRATION DATE NOTED ABOVE APPLIES PER 40 CFT PART 75, APPENDIX H. OTHERWISE THE GENERAL EXPIRATION DATE APPLIES.

ANALYST: Th Wilb



Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 887-2571 FAX: (909) 887-0549

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
PACIFIC ENVIRONMENTAL SER.
STEVE HERNANDEZ
13100 BROOKS DRIVE
BALDWIN PARK, CA 91706

Assay Laboratory
Scott Specialty Gases
2600 Cajon Boulevard
San Bernardino, CA 92411

Purchase Order 0640-102
Project # 29933.002

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol 1 Procedure #G1, Section Number 3.0.4

Cylinder Number ALM035663
Cylinder Pressure 1900 psig

Certification Date 02-15-94

Exp. Date 02-15-96

ANALYZED CYLINDER

Components
SULFUR DIOXIDE

Certified Concentration
86.01 PPM

Analytical Uncertainty*
± 1 % NIST Traceable

Balance Gas: Nitrogen

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type
GMIS

Expiration Date
06-94

Cylinder Number
AAL9133

Concentration
238.8 ppm

INSTRUMENTATION

Instrument/Model/Serial #
Horiba / OPE-135D / 56463601

Last Date Calibrated
01-31-94

Analytical Principle
NDIR

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components	First Triad Analysis	Second Triad Analysis	Calibration Curve
Sulfur Dioxide	Date: 02-08-94 Response Units: mv Z1= 0.00 R1= 97.0 T1= 36.5 R2= 97.0 Z2= 0.00 T2= 36.5 Z3= 0.00 T3= 36.5 R3= 97.0 Avg. Conc. of Cust Cyl 86.01 ppm	Date: 02-15-94 Response Units: mv Z1= 0.00 R1= 97.0 T1= 36.5 R2= 97.0 Z2= 0.00 T2= 36.5 Z3= 0.00 T3= 36.5 R3= 97.0 Avg. Conc. of Cust Cyl 86.01 ppm	Concentration= Ax^2+Bx+C A=0.001735 B=-2.295 C=-0.07555
	Date: Response Units: mv Z1= R1= T1= R2= Z2= T2= Z3= T3= R3= Avg. Conc. of Cust Cyl	Date: Response Units: mv Z1= R1= T1= R2= Z2= T2= Z3= T3= R3= Avg. Conc. of Cust Cyl	Concentration=
	Date: Response Units: mv Z1= R1= T1= R2= Z2= T2= Z3= T3= R3= Avg. Conc. of Cust Cyl	Date: Response Units: mv Z1= R1= T1= R2= Z2= T2= Z3= T3= R3= Avg. Conc. of Cust Cyl	Concentration=

SPECIAL NOTES: IF THIS PRODUCT IS USED FOR ACID RAIN COMPLIANCE, THE ACID RAIN EXPIRATION DATE NOTED ABOVE APPLIES PER 40 CFR PART 75, APPENDIX H. OTHERWISE THE GENERAL EXPIRATION DATE APPLIES.

ANALYST

JK Wil



Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 887-2571 FAX: (909) 887-0549

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS RECERTIFICATION

Customer
PACIFIC ENVIRONMENTAL SER.
13100 BROOKS DRIVE
HALLOWIN PARK, CA 91706
C/O STEVE HERNANDEZ

Assay Laboratory
Scott Specialty Gases
2600 Cajon Boulevard
San Bernardino, CA 92411

Purchase Order 4896-000
Project # 31442.001

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay and Certification of Gaseous Calibration Standards. Procedure G1; September 1993.

Cylinder Number AAL018067
Cylinder Pressure+ 200 PSIG

Certification Date 05-17-94
Previous Certification Date 10-20-93

Exp. Date 05-17-97

ANALYZED CYLINDER

Components
(PROPANE)

Certified Concentration
20.01 PPM

Analytical Uncertainty*
± 1 % NIST Traceable

(Air)

Balance Gas

*Do not use when cylinder pressure is below 150 psig.

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type/Sample No. Expiration Date
SRM1667B 04-98

Cylinder Number
CLM005374

Concentration
47.30 ppm C3H8/Air

INSTRUMENTATION

Instrument/Model/Serial #
C3H8: OPE-435

Last Date Calibrated
03-25-94

Analytical Principle
F.I.D.

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components	Previous Certification	Third Triad Analysis	Calibration Curve																																														
Propane	<table><tr><td>Date: 10-20-93</td><td colspan="3">Response Units: mvv</td></tr><tr><td>Z1=</td><td>R1=</td><td colspan="2">T1=</td></tr><tr><td>R2=</td><td>Z2=</td><td colspan="2">T2=</td></tr><tr><td>Z3=</td><td>T3=</td><td colspan="2">R3=</td></tr><tr><td colspan="2">Avg. Conc. of Cust Cyl.</td><td colspan="2">20.09 ppm</td></tr></table>	Date: 10-20-93	Response Units: mvv			Z1=	R1=	T1=		R2=	Z2=	T2=		Z3=	T3=	R3=		Avg. Conc. of Cust Cyl.		20.09 ppm		<table><tr><td>Date: 05-17-94</td><td colspan="3">Response Units: mvv</td></tr><tr><td>Z1= 0.00</td><td>R1= 47.2</td><td colspan="2">T1= 20.0</td></tr><tr><td>R2= 47.2</td><td>Z2= 0.00</td><td colspan="2">T2= 20.0</td></tr><tr><td>Z3= 0.00</td><td>T3= 20.0</td><td colspan="2">R3= 47.2</td></tr><tr><td colspan="2">Avg. Conc. of Cust Cyl.</td><td colspan="2">20.01 ppm</td></tr></table>	Date: 05-17-94	Response Units: mvv			Z1= 0.00	R1= 47.2	T1= 20.0		R2= 47.2	Z2= 0.00	T2= 20.0		Z3= 0.00	T3= 20.0	R3= 47.2		Avg. Conc. of Cust Cyl.		20.01 ppm		<table><tr><td>Concentration=</td><td>Ax + B</td></tr><tr><td>A=1.002</td><td></td></tr><tr><td>B=-0.03716</td><td></td></tr></table>	Concentration=	Ax + B	A=1.002		B=-0.03716	
Date: 10-20-93	Response Units: mvv																																																
Z1=	R1=	T1=																																															
R2=	Z2=	T2=																																															
Z3=	T3=	R3=																																															
Avg. Conc. of Cust Cyl.		20.09 ppm																																															
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Date:	Response Units: mvv																																																
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Z3=	T3=	R3=																																															
Avg. Conc. of Cust Cyl.																																																	
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Date:	Response Units: mvv																																																
Z1=	R1=	T1=																																															
R2=	Z2=	T2=																																															
Z3=	T3=	R3=																																															
Avg. Conc. of Cust Cyl.																																																	
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Z1=	R1=	T1=																																															
R2=	Z2=	T2=																																															
Z3=	T3=	R3=																																															
Avg. Conc. of Cust Cyl.																																																	
Concentration=																																																	

Special Notes:

Analyst:

76 Wil



Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 887-2571 FAX: (909) 887-0549

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
PACIFIC ENVIRONMENTAL SER
13100 BROOKS DRIVE
BALDWIN PARK, CA 91706

Assay Laboratory
Scott Specialty Gases
2600 Cajon Boulevard
San Bernardino, CA 92411

Purchase Order 0640-102
Project # 31576.001

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay and Certification of Gaseous Calibration Standards; Procedure G1; September 1993.

Cylinder Number AAL-14083
Cylinder Pressure+ 2000 PSIG

Certification Date 6/2/94

Exp. Date 4/4/98

ANALYZED CYLINDER

Components
(PROPANE)

Certified Concentration
29.03 PPM

Analytical Uncertainty*
± 1 % NIST Traceable

(AIR)

Balance Gas

+Do not use when cylinder pressure is below 150 psig.

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type/Sample No. SRM1666B
Expiration Date 4/4/98

Cylinder Number
CLM007196

Concentration
95.50 PPM C3H8 IN AIR

INSTRUMENTATION

Instrument/Model/Serial #
OPE435

Last Date Calibrated
6/3/94

Analytical Principle
FID

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components

First Triad Analysis

Second Triad Analysis

Calibration Curve

PROPANE

Date: 6/3/94 Response Units: mv
Z1= 00.0 R1= 95.3 T1= 29.0
R2= 95.3 Z2= 00.0 T2= 29.0
Z3= 00.0 T3= 29.0 R3= 95.3
Avg. Conc. of Cust Cyl 29.03

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl

Concentration= Ax + B
A = 1.002165
B = -0.037166

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl

Concentration=

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl

Concentration=

Special Notes:

Analyst:



Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 887-2571 FAX: (909) 887-0549

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
PACIFIC ENVIRONMENTAL SER.
13100 BROOKS DRIVE
BALDWIN PARK, CA 91706

Assay Laboratory
Scott Specialty Gases
2600 Cajon Boulevard
San Bernardino, CA 92411

Purchase Order 4896-000
Project # 31443.001

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay and Certification of Gaseous Calibration Standards, Procedure G1; September 1993.

Cylinder Number AAL 2522
Cylinder Pressure+ 2000 PSIG

Certification Date 5/23/94

Exp. Date 5/23/97

ANALYZED CYLINDER

Components
(PROPANE)

Certified Concentration
48.00 PPM

Analytical Uncertainty*
± 1 % NIST Traceable

(AIR)

Balance Gas

+Do not use when cylinder pressure is below 150 psig.

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type/Sample No. Expiration Date
SRM 3/4/98

Cylinder Number
CLM005374

Concentration
47.30 PPM C3H8 IN AIR

INSTRUMENTATION

Instrument/Model/Serial #
OPE435/FID/5603411215

Last Date Calibrated
3/25/94

Analytical Principle
FID

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components

First Triad Analysis

Second Triad Analysis

Calibration Curve

PROPANE

Date: 5/23/94 Response Units: mv
Z1= 0.00 R1= 95.3 T1= 48.0
R2= 95.3 Z2= 0.00 T2= 47.9
Z3= 0.00 T3= 47.9 R3= 95.3
Avg. Conc. of Cust Cyl. 48.00 PPM

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Concentration= $Ax + B$
A = 1.002
B = -0.03716

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

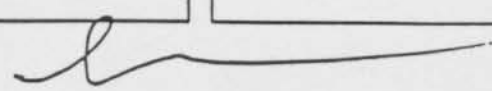
Concentration=

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Date: Response Units: mv
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Concentration=

Special Notes:

Analyst: 



Scott Specialty Gases, Inc.

Shipped
From:

2600 CAJON BLVD.
SAN BERNARDINO CA 92411
Phone: 909-887-2571

Fax: 909-887-0549

CERTIFICATE OF ANALYSIS

PACIFIC ENVIRONMENTAL SER
STEVE HERNANDEZ
13100 BROOKS DRIVE

BALDWIN PARK

CA 91706

PROJECT #: 02-28207-004
PO#: PO# 0640-102
ITEM #: 0202RCOC AL
DATE: 10/20/93

CYLINDER #: ALM06161
FILL PRESSURE: 2000PSIG

COMPONENT

PROPANE
PROPANE
AIR

ANALYSIS (MOLES)

OLD# 80.58 PPM
NEW# 80.38 PPM
BALANCE

2000PSIG 30N#2 10-22
TRACEABLE TO SRM 1668B
CYL# CL#007196

ANALYST: *CS*

PLUMSTEADVILLE, PENNSYLVANIA TROY, MICHIGAN HOUSTON, TEXAS DURHAM, NORTH CAROLINA
SOUTH PLAINFIELD, NEW JERSEY FREMONT, CALIFORNIA WAKEFIELD, MASSACHUSETTS LONGMONT, COLORADO
BATON ROUGE, LOUISIANA

DRY GAS METER AND ORIFICE CALIBRATION

Dry Gas Meter No.: 677152

Meter Box No.: 4A

Reference Dry Gas Meter No.: 25507

Barometric Pressure: 29.56

Calibration Date: 5/15/95

Calibration Performed By: *[Signature]*

Orifice Manometer Setting	Initial Reference DGM Reading V = ft ³	Final Reference DGM Reading V = ft ³	Reference Gas Volume V _r = ft ³	Initial DGM Reading V = ft ³	Final DGM Reading V = ft ³	Test DGM Volume V _d = ft ³	Temperature				Run Time minutes	Flow Rate Q = cfm	Meter Gamma	Delta H @
							Reference DGM	DGM Inlet	DGM Outlet	DGM Average				
H = "H ₂ O							tr = F	t = F	t = F	td				
0.5	417.842	427.866	10.024	508.593	518.615	10.022	71	77	72	75	24.9	0.40	1.006	1.745
1.0	428.236	438.253	10.017	518.984	529.027	10.043	70	83	76	79	17.9	0.55	1.012	1.785
2.0	438.827	448.881	10.054	529.596	539.694	10.098	70	88	78	83	13.0	0.76	1.015	1.855
4.0	449.612	459.777	10.165	540.430	550.651	10.221	70	91	79	85	9.3	1.08	1.013	1.851

Average 1.011 1.809

DRY GAS METER AND ORIFICE CALIBRATION

Dry Gas Meter No.: 6847415

Meter Box No.: 2A

Reference Dry Gas Meter No.: 25507

Barometric Pressure: 29.45

Calibration Date: 5/12/95

Calibration Performed By: 

Orifice Manometer Setting	Initial Reference DGM Reading	Final Reference DGM Reading	Reference Gas Volume	Initial DGM Reading	Final DGM Reading	Test DGM Volume	Temperature				Run Time	Flow Rate	Meter Gamma	Delta H @
							Reference DGM	DGM Inlet	DGM Outlet	DGM Average				
H = "H ₂ O	V = ft ³	V = ft ³	V _r = ft ³	V = ft ³	V = ft ³	V _d = ft ³	t _r = F	t = F	t = F	t _d	minutes	Q = cfm		
0.5	287.442	297.528	10.088	665.563	676.750	10.187	74	80	75	78	25.9	0.38	0.995	1.883
1.0	298.279	308.342	10.063	676.415	686.712	10.297	74	88	83	86	18.7	0.52	0.996	1.943
2.0	309.885	319.965	10.080	688.260	698.416	10.156	74	88	83	86	13.3	0.74	1.009	1.959
4.0	321.039	331.463	10.424	699.510	709.982	10.472	74	93	84	89	9.8	1.03	1.012	1.978

Average 1.003 1.941

DRY GAS METER AND ORIFICE CALIBRATION

Dry Gas Meter No.: 1042485

Meter Box No.: 1A

Reference Dry Gas Meter No.: 25507

Barometric Pressure: 29.45

Calibration Date: 5/12/95

Calibration Performed By: *Richard J. [Signature]*

Orifice Manometer Setting	Initial Reference DGM Reading	Final Reference DGM Reading	Reference Gas Volume	Initial DGM Reading	Final DGM Reading	Test DGM Volume	Temperature				Run Time minutes	Flow Rate Q = cfm	Meter Gamma	Delta H @
							Reference DGM	DGM Inlet	DGM Outlet	DGM Average				
H = "H2O	V = ft ³	V = ft ³	Vr = ft ³	V = ft ³	V = ft ³	Vd = ft ³	tr = F	t = F	t = F	td	minutes	Q = cfm		
0.5	376.847	385.983	10.136	186.880	196.893	10.013	75	82	76	79	26.3	0.39	1.019	1.781
1.0	386.451	396.531	10.080	197.360	207.368	10.008	75	87	80	84	18.1	0.54	1.021	1.828
2.0	397.015	407.094	10.079	207.853	217.875	10.022	75	89	81	85	13.2	0.74	1.018	1.939
4.0	407.473	417.604	10.131	218.254	228.281	10.027	75	93	83	88	9.3	1.06	1.026	1.895

Average 1.021 1.861

REPORT OF CALIBRATION
LIQUID-IN-GLASS-THERMOMETER

CALIBRATED BY EVER READY THERMOMETER CO.

MARKED: ERTCO 611-3FC S/N-2269
RANGE: -20 TO +110 DEGREES C IN 1 DEGREE GRADUATIONS.

THERMOMETER READING	CORRECTION (ITS-90)**
0.0 C	0.0 C
37.0	-0.1
56.0	0.0

** ALL TEMPERATURES IN THIS REPORT ARE BASED ON THE INTERNATIONAL TEMPERATURE SCALE OF 1990 (ITS-90) PUBLISHED IN THE METROLOGIA 27, NO. 1, 3/10/90.

THIS THERMOMETER WAS CALIBRATED AGAINST A STANDARD CALIBRATED AT THE NATIONAL INSTITUTE OF STANDARDS AND TECHNOLOGY (NIST) FORMERLY THE NATIONAL BUREAU OF STANDARDS (NBS).

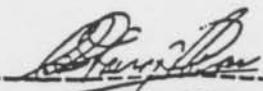
FOR A DISCUSSION OF ACCURACIES ATTAINABLE WITH SUCH THERMOMETERS SEE NBS MONOGRAPH 150.

IF NO SIGN IS GIVEN ON THE CORRECTION, THE TRUE TEMPERATURE IS HIGHER THAN THE INDICATED TEMPERATURE; IF THE SIGN GIVEN IS NEGATIVE, THE TRUE TEMPERATURE IS LOWER THAN THE INDICATED TEMPERATURE. TO USE THE CORRECTIONS PROPERLY, REFERENCE SHOULD BE MADE TO THE NOTES GIVEN BELOW.

THE THERMOMETER WAS TESTED IN A LARGE, CLOSED-TOP, ELECTRICALLY HEATED, LIQUID BATH, BEING "IMMERSED" 76MM. THE TEMPERATURE OF THE ROOM WAS ABOUT 25 DEGREES C (77 DEGREES F). IF THE THERMOMETER IS USED UNDER CONDITIONS WHICH WOULD CAUSE THE AVERAGE TEMPERATURE OF THE EMERGENT LIQUID COLUMN TO DIFFER MARKEDLY FROM THAT PREVAILING IN THE TEST, APPRECIABLE DIFFERENCES IN THE INDICATIONS OF THE THERMOMETER WOULD RESULT.

THE TABULATED CORRECTIONS APPLY PROVIDED THE ICE POINT READING IS 0.0 DEGREES C. IF THE ICE-POINT READING IS FOUND TO BE HIGHER (OR LOWER) THAN STATED, ALL OTHER READINGS WILL BE HIGHER (OR LOWER) TO THE SAME EXTENT.

TEST NUMBER: 140381
DATE: 06/21/90
STANDARD SERIAL NO. 128239
NIST IDENTIFICATION NO. 80024



EVER READY THERMOMETER CO.

METER BOX TEMPRATURE READOUT CALIBRATION

CALIBRATED BY: Aria Mike

DATE: 5/25/95

	<u>Inlet (°F)</u>	<u>Outlet (°F)</u>	<u>Thermometer (°F)</u>
BOX 1A	34.0 74.0 202.0	35.0 75.0 203.0	33.8 (1 °C) 75.2 (24 °C) 203.0 (95 °C)
BOX 2A	34.0 74.0 214.0	33.0 76.0 215.0	33.8 (1 °C) 75.2 (24 °C) 212.0 (100 °C)
BOX 3A	32.0 70.0 213.0	30.0 71.0 212.0	32.0 (0 °C) 73.4 (23 °C) 212.0 (100 °C)
BOX 4A	32.0 71.0 211.0	32.0 71.0 210.0	32.0 (0 °C) 75.2 (24 °C) 212.0 (100 °C)
BOX 5A	35.0 75.0 214.0	33.0 74.0 212.0	32.0 (0 °C) 75.2 (24 °C) 212.0 (100 °C)

NOTE:

Thermometer Standard Serial Number: 128239

Thermometer NIST I.D. Number: 88024

THERMOCOUPLE TEMPERATURE CALIBRATION

CALIBRATED BY: *Rachel R*

DATE: 5/26/95

TC #	ROOM		FREEZING		BOILING	
	REF. (C)	DIG. (C)	REF. (C)	DIG. (C)	REF. (C)	DIG. (C)
22	23	23	1	1	100	100
11	19	19	1	1	100	100
5	23	23	0.5	0-1	95.5	100
100	23	23	1	1	100	100
10	23	23	1	1	100	99
101	23	23	2	2	100	100
17	23	23	0.5	1	100	100
6	23	23	0.2	0	100	100
9	23	23	1	1	100	100
16	23	23	1	1	100	100
102	23	23	1	1	100	100
S-3A	24	23	2.5	1	100	99
S-4A	24	23-24	3	3	100	99
S-2A	24	23-24	0.3	1	100	99
S-19A	24	24	1	1	99.5	98
S-16A	24	24	0.5	1	99	97
S-18A	24	24	1.5	1	100	99
S-15A	24	24	1	1	100	99
S-17A	24	24	1.2	2	99.5	97
S-14A	24	24	2	2	100	99
2	24	24	1	1	99.5	100
103	24	24	1	1	100	101
104	24	24	2	2	99	99
D8	24	23-24	1	2	99	99
*A	24	22	2	1	100	100
*B	24	23	2	1	100	100

* New Probes: Need to be numbered.



PRECISION
INSTRUMENT
REPAIR

PRECISION INSTRUMENT REPAIR CO

13414 WOODRUFF AVE., BELLFLOWER CA 90706

310/925-6672

Certification Report Of Precision Balances and Scales

This is to certify that the balance calibrated is in compliance to US Government MIL-STD #45662A and N.I.S.T. Handbook 44, Table 2 tolerances for devices I, II and III.

REPORT NUMBER: 4038
PURCHASE ORDER NUMBER:
COMPANY: PACIFIC ENVIRONMENTAL SERVICES
ADDRESS: 13100 BROOKS, SUITE 100
BALDWIN PARK, CA. 91706

DATE OF TEST: 11-23-94
TEMPERATURE: 65°F
R.H. 50%
NIST TRACEABLE STANDARD USED: CLASS 1 SET

SERIAL NUMBER OF STANDARD: L233



BALANCE MFG. MODEL SERIAL NUMBER

TORBAL EA-1 ANALYTICAL BALANCE, S/N 156636

CALIBRATION AS FOUND: 100 mg = 103.3 mg

CALIBRATED TO: 100 mg = 100.0 mg

LINEARITY: In Spec
MAXIMUM LOAD: In Spec 160 GRAMS
REPETEABILITY: In Spec

Date of Calibration 11-23-94 Technician Tom Benson License 1-0903

DICK MUNNS COMPANY
Liquid and Gas - Flowmeter Calibration Service
10571 Calle Lee - 133 • Los Alamitos, California 90720
Telephone (310) 596-1559 • Telefax (714) 827-0823

CERTIFICATE OF CALIBRATION

Client Name:	P.E.S., INC.	Calibration Date:	12-02-1994
Reference Number:	25507	Calibration Due:	12-02-1995
Instrument Manufacturer:	ROCKWELL	Calibration Fluid:	AIR 14.7 PSIA 70F
Instrument Description:	P.D.METER	Test Unit(s):	A-3 DUE 5-2-95
Model Number:	190 CFH	NIST Traceability Per:	M-0122
Serial Number:	25507	Ambient Conditions:	29.96"HGA 70F RH.38%
Mfg.Rated Accuracy:	+/- .5%	CERT NUMBER:	PES25507
Accuracy Given:	WITHIN MFG TOLERANCE		

	IND.SCFM	ACT.SCFM
1	0.100	0.100
2	0.200	0.200
3	0.399	0.400
4	0.814	0.813
5	1.000	0.999
6	1.508	1.504
7	2.091	2.087
8	2.305	2.312
9	2.559	2.553
10	2.920	2.919
11	3.334	3.325

Comments:

All instruments used in the performance of the above calibration have direct traceability to the National Institute of Standards and Technology (NIST). Calibration has been performed in accordance with MIL-STD-45662A.

Calibration Performed By:

RALPH AWAD

Approved By:

Michael Munns

MICHAEL MUNNS

Pitot Tube Calibration Data Sheet

Calibrated by: [Signature]

Date: 5-30-95

Pitot Tube I.D. S-2A

Effective Length: 37"

Pitot Tube Assembly Level ? ☒ Yes ☐ No

Pitot Tube Openings Damaged ? ☐ Yes ☒ No

If Yes, Explain _____

$\alpha_1 =$ 0° ($<10^\circ$)

$\alpha_2 =$ 0° ($<10^\circ$)

$\beta_1 =$ 0° ($<10^\circ$)

$\beta_2 =$ 0° ($<10^\circ$)

$\gamma =$ 0-5° $\theta =$ 0° $A =$ 0.945

$Z = A \sin \gamma =$ 0 - 0.0824 cm (in.) 0.32 cm ($<1/8$ in.)

$W = A \sin \theta =$ 0 cm (in.) 0.08 cm ($<1/8$ in.)

$P_A =$ 0.472 cm (in.)

$P_B =$ 0.472 cm (in.)

$D_t =$ 0.381 cm (in.)

Comments: _____

Calibration Required ? ☐ Yes ☒ No

ENI

Lilia CCC

5-30-95

9-3R

55

☒ Yes☐ No☐ Yes☒ No

5

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1.6

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1.11

C

c. 561

C. 561

C, 377

☐ Yes☒ No

Pitot Tube Calibration Data Sheet

Calibrated by: David C. T.

Date: 5-30-95

Pitot Tube I.D. S-4A

Effective Length: 37"

Pitot Tube Assembly Level ? ☒ Yes ☐ No

Pitot Tube Openings Damaged ? ☐ Yes ☒ No

If Yes, Explain _____

$\alpha_1 =$ 0 $^{\circ}(<10^{\circ})$

$\alpha_2 =$ 0 $^{\circ}(<10^{\circ})$

$\beta_1 =$ 0-2 $^{\circ}(<10^{\circ})$

$\beta_2 =$ 0 $^{\circ}(<10^{\circ})$

$\gamma =$ 0-2 $^{\circ}$

$\theta =$ 0 $^{\circ}$

$A =$.952 $^{\circ}$

$Z = A \sin \gamma =$ 0-0.332 cm (in.) 0.32 cm ($<1/8$ in.)

$W = A \sin \theta =$ 0 cm (in.) 0.08 cm ($<1/16$ in.)

$P_A =$ 0.459 cm (in.)

$P_B =$ 0.459 cm (in.)

$D_t =$ 0.377 cm (in.)

Comments: _____

Calibration Required ? ☐ Yes ☒ No



SOURCE SAMPLING NOZZLE CALIBRATION

CALIBRATED/UPDATED BY: *Paula Hoff*

DATE: 9-21-95

NOZZLE	READING (INCHES)			AVERAGE	SHAPE	COMMENTS
ID #	1	2	3	DIAMETER		
X1	0.311	0.311	0.312	0.311	CURVED	
X2	0.372	0.371	0.373	0.372	CURVED	
X5	0.239	0.241	0.240	0.240	CURVED	
X6	0.269	0.272	0.271	0.271	CURVED	
X9	0.333	0.334	0.334	0.334	CURVED	
X10	0.353	0.354	0.354	0.354	CURVED	
X11	0.355	0.356	0.356	0.356	CURVED	
X12	0.323	0.323	0.324	0.323	CURVED	
X13	0.298	0.298	0.299	0.298	CURVED	
X15	0.281	0.283	0.287	0.284	CURVED	NO GOOD
X16	0.245	0.248	0.248	0.247	CURVED	
X21	0.261	0.258	0.262	0.260	CURVED	
X22	0.276	0.277	0.279	0.277	CURVED	
X23	0.219	0.217	0.217	0.217	CURVED	
X24	0.169	0.166	0.168	0.168	CURVED	
X25	0.240	0.242	0.240	0.240	CURVED	
X26	0.190	0.193	0.194	0.192	CURVED	
X27	0.256	0.256	0.256	0.256	CURVED	
X28	0.180	0.180	0.180	0.180	CURVED	
N1	0.143	0.142	0.142	0.142	B.H.	
N3	0.142	0.141	0.141	0.141	B.H.	
N6	0.494	0.493	0.495	0.494	B.H.	
N9	0.430	0.431	0.430	0.431	B.H.	
M1	0.749	0.751	0.752	0.751	B.H.	
M2	0.494	0.496	0.491	0.494	B.H.	NO GOOD
M3	0.446	0.443	0.444	0.444	B.H.	
M4	0.504	0.504	0.504	0.504	B.H.	
M5	0.472	0.471	0.473	0.472	B.H.	
M6	0.808	0.802	0.805	0.805	B.H.	NO GOOD
M7	0.431	0.437	0.432	0.433	B.H.	NC GOOD
M8	0.275	0.277	0.275	0.276	B.H.	
05P	0.239	0.241	0.240	0.240	CURVED	
40P	0.226	0.225	0.225	0.225	ELBOW	
28PB	0.439	0.438	0.436	0.438	B.H.	
30PB	0.798	0.803	0.805	0.802	B.H.	NO GOOD
38PB	0.796	0.806	0.805	0.802	B.H.	NO GOOD
44PB	0.309	0.307	0.309	0.308	B.H.	
45PB	0.375	0.375	0.372	0.374	B.H.	
100	0.385	0.385	0.384	0.385	ELBOW	
120	0.381	0.382	0.383	0.382	ELBOW	